

WHAT'S NEW IN MARINE RADIOTELEPHONE

14278

Popular Electronics

WORLD'S LARGEST-SELLING ELECTRONICS MAGAZINE

JULY 1975/75¢

HOW TO PROGRAM READ-ONLY MEMORIES

Have Fun With
Electronic Dice

Listen In to
Apollo/Soyuz
Transmissions

Precision Matching
of Resistors

Audio Frequency
Meter Project

LAB TEST REPORTS

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JVC CD-1669
Stereo Cassette Deck

Pioneer SE-700
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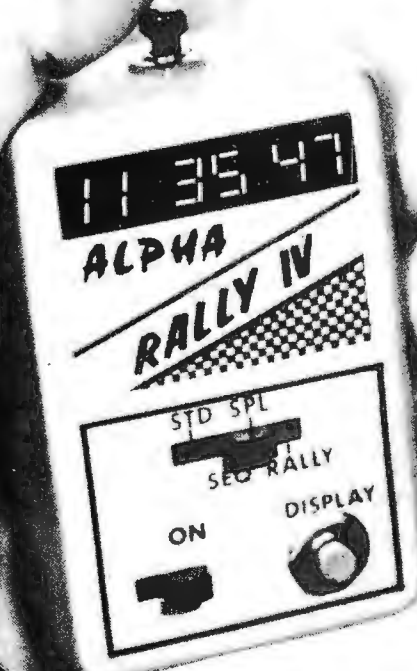
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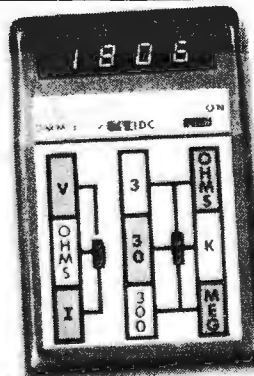
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Editorial

THE ATIS CONNECTION

CB'ers of the future may someday find Damocles's Sword hanging over them in the event they abuse the Service's rulings (transmitting foul language, exceeding the five-minute communication limit, not using station callsigns, "skip" communications, etc).

If the FCC's Docket No. 20351 is ever put into effect, all new CB gear will be fitted with an automatic transmitter identification system (ATIS) that will spew out callsigns in coded form. The ATIS identifier would only be mandatory for new transmitters placed in service one year after the final rules are adopted. CB manufacturers, as well as manufacturers of other transmitters in the Safety and Special Radio Service, would then be compelled to include an ATIS in each new transmitter. The encoding of the callsign into the ATIS would have to be performed by a first- or second-class commercial radiotelephone licensee or the manufacturer. (Note: ATIS installation and design require that the transmitter will *not* function unless this is done.)

The proposed system is alphanumeric. It would be binary coded in ASCII (American Standard Code for Information Interchange), with the station's callsign transmitted automatically at the beginning and the end of each transmission and, if transmission exceeds 30 seconds duration, once each thirty seconds. The ATIS information would be applied to the carrier by audio-frequency shift keying (AFSK) 85 Hz above and below a 1200-Hz center frequency, with "0" being 1115 Hz and "1" being 1285 Hz. Transmission of the 22-character code, which also includes the gear's serial number (how's that for a theft deterrent?), is suggested at a rate of 100 bauds (a baud is a pulse per second). Accordingly, each code transmission would consume about 1/4 to 1/5 of a second. You'll hear it, of course. However, the ATIS will not eliminate the operator's need to identify transmissions vocally as presently outlined in the FCC's Part 95.95 Rules and Regulations.

The proposal is certainly interesting. It would have the advantage of exposing those CB'ers who flagrantly violate the operating rules in one way or another. Equally important, it would doubtlessly motivate these people to operate according to the rules (which promise to be loosened in the near future). Although the fractional-second "brrrrp" audio code that would sound whenever one presses or releases the mike's "talk" button might be a slight irritant, it would serve a most useful purpose. It would also alert the receiving party that transmission had ended. Naturally, ATIS would add a few dollars to cost, but one can easily chalk that up to a one-shot insurance premium cost.

There might well be other objections, considerations and suggestions from various parties. For example, should a subaudible system be adopted; will the proposed system be compatible with future designs for nonvoice control functions such as selective calling, repeater control, and so on? Time will tell.

Art Salsberg

New 21^(diag.) Heathkit digital-design Color TV

Popular Electronics editors called the digital-design GR-2000 "the color TV of the future." Now you can enjoy the same technology and features in the new GR-2050 with the convenient, popular 21-inch picture tube.

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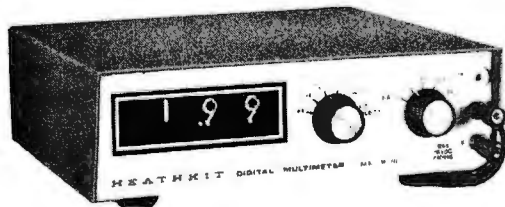
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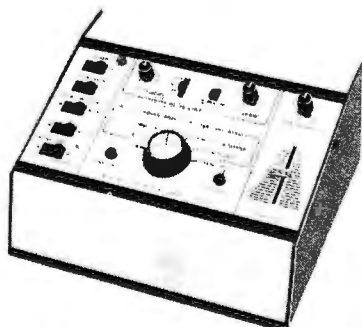


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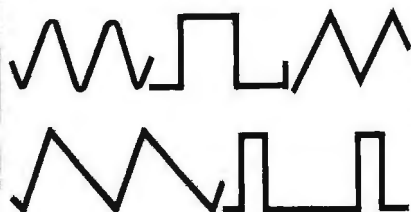
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Letters

MORE ON OBTAINING PARTS

I found the February 1975 Editorial ("It's a Tough World Out There"), dealing with finding parts for projects, both interesting and true. I currently have several projects underway, but at a standstill because I can't find the parts I need. My new policy is never to start any project, no matter how simple it is, until I know exactly where to locate every item needed.

I realize that quite a few projects call for the latest IC's that aren't available at the time of publication. I cannot fault this because, after all, POPULAR ELECTRONICS wouldn't be the fine source of information if it is if you didn't keep up with new developments.

GEORGE H. THOMPSON, JR.
Goleta, Calif.

Amen! to your February Editorial. Getting all the parts needed for a project might be difficult for people in the States, but it can't begin to compare with the frustrations we overseas subscribers must endure.

Wouldn't it make your projects more feasible and attractive to get companies to market complete kits of parts for your projects?

JACK BENNETT
Berlin, Germany

Whenever we publish construction plans for a project using a brand new device, we first make sure the device is available—either directly from the manufacturer or through an authorized distributor. For most major construction projects, we do try to get a company to supply a complete kit of parts or a kit of the parts that are difficult to obtain except in large orders.

FEEDBACK ON AM BCB DX'ING

Another reason for DX'ing the medium-wave band ("How to Listen to Out-of-State AM Broadcasts," April 1975) is good listening. My favorite station is WWL out of New Orleans. Doubtless, many readers will find favorite stations or programs out of state as I did.

LEONARD H. PONDER
Chandler, N.C.

I thoroughly enjoyed "How to Listen to Out-of-State AM broadcasts." However, I have an important correction for you. Cleveland Cavalier games are no longer carried on WERE. Station WWWE (1100 kHz, 50 kW) has carried these games for the past two seasons. WWWE covers 38 states on a normal night, and we have recently received reception reports from the West Coast and Sweden. DX'ers who want to listen to WWWE should tune us in after the sun sets in the West.

JIM ARCARO
WWWE Engineer
Cleveland, Ohio

MEMORY TRANSLATOR

I was very enthusiastic when I first saw "Build a Portable A/D Memory Translator" (April 1975). But after reading the text, I have some apprehensions. According to the text, an uncompensated telephone line cannot be expected to convey frequencies much outside a 300- to 3000-Hz passband. The proposed recentering of the carrier at 2000 Hz would seemingly introduce intolerable distortion for deviations much beyond ± 1000 Hz unless the changes also produce a suitable reduction in deviation.

Furthermore, the unmodified version with a 7000-Hz ± 2000 Hz output would not appear to be suitable for low-cost recorders, most of which would be hard pressed to accommodate the carrier, let alone the upper sideband. I was wondering whether the required linearity could be achieved if the carrier were centered at 3000 Hz (± 2000 Hz), switchable to 1650 Hz (± 1350 Hz) for telephone applications, and how it would affect the "chart recordings by mail" application.

J.P. LANE
Roanoke, Va.

The change to the 2000-Hz center frequency also reduces the FM deviation to ± 800 Hz so that limitations in telephone-line performance will not be due to bandwidth. The 7000-Hz ± 2000 Hz FM output may be out of the 3-dB bandwidth of a low-cost recorder, but this is not critical for operation of the Translator. The Translator will operate well with virtually any tape recorder since it has a built-in 7000-Hz filter for improved sensitivity in this band and, more importantly, the FM detector has good AM rejection—meaning that low-amplitude signals will still control the phase-locked loop. We determined that the 10,000-Hz response can be down as much as 30 dB in a poor recording apparatus and still the Translator will detect properly.

The chart recording by mail arrangement depends mainly on the initial 15-second ground reference as explained in the text. Any comments concerning bandwidth changes or special calibration should be forwarded with the cassette.

—Author

WESTINGHOUSE MAKES COLOR CRT'S TOO

"The New Color TV Picture Tubes" (March 1975) explained the advancements in color CRT's very well. However, when the author listed the major manufacturers of tubes, he left out Westinghouse Electric Corp. Westinghouse was making color picture tubes in the 1950's. In fact, it introduced the first all-glass rectangular color tube, the 22EP22, in 1956.

Most of Westinghouse's market is for private labels. The company has also developed some types of color tubes for the more discriminating European market and has marketed these tubes for a number of years under the (W) label.

ROBERT RUSSELL
Wellsburg, N.Y.

SOME COMMENTS ON FAA CAREER

Readers whose interest was sparked by "How to Become an FAA Electronics Technician" (April 1975) might like to know of a college program that can help them land a position. Mercer County College offers the A.A.S. degree in Aviation Electronics Technology.

PETER J. HOLSBERG
Associate Professor of
Electrical Engineering
Mercer County Community College
Trenton, N.J.

One thing not mentioned in "How to Become an FAA Electronics Technician" is the fact that ET's must do shift work. At almost all FAA facilities, there are evening, midnight, and weekend shifts that must be manned. Normally, the ET works a shift until he is promoted to a staff position.

GERALD D. PELTON
FAA Electronics Technician

H.H. SCOTT

Audio Pioneer

Herman Hosmer Scott, founder and former president of H.H. Scott, Inc., of Maynard, Massachusetts, died recently in Newton, Mass., at the age of 66.

He established his firm in 1947 and retired in 1972. The name H.H. Scott was among the handful of brands familiar to hi-fi equipment buffs during the early days of the industry.

Mr. Scott held a number of patents, including those for the dynamic noise suppressor and RC oscillator.

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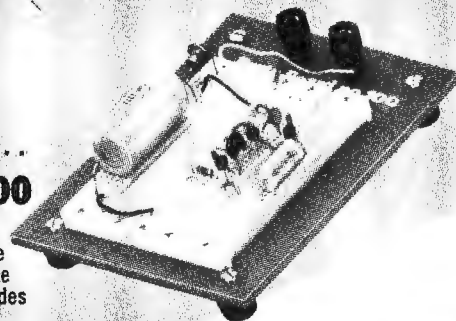
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CIRCLE NO. 14 ON READER SERVICE CARD

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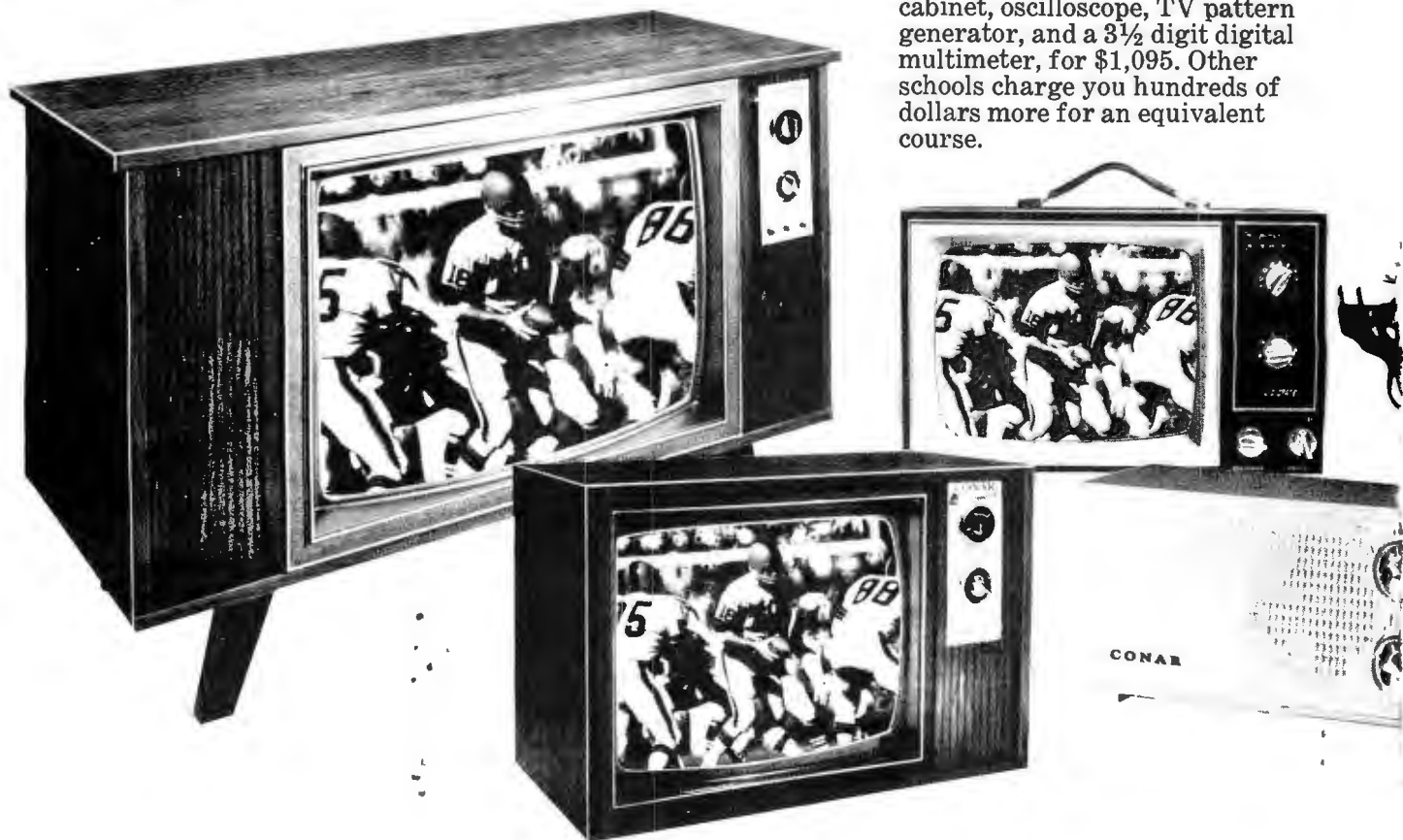
NRI saves you tuition because our costs are lower. We pay no salesmen, and we engineer our own kits and training equipment. We don't buy "hobby kits" from others. Nor do we penalize you with big interest charges for time payments. We pass the savings on to you.

Compare training

NRI is one of the few home study schools that maintains its own full-time staff of technical writers, editors, illustrators, development engineers and publications experts. The people who design the kits also design the lessons... so that theory and practice go hand in hand. The lessons aren't "retro-fitted" to an outside-source "hobby kit." At each stage of building, you experiment with the *power on*; you don't wait till the set's completed to learn troubleshooting. The NRI set is designed exclusively for training. It is also a superb 100% solid-state receiver for your personal use.

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Most schools offer one course in color TV servicing, period. Only NRI offers you five different courses to match your needs and budget. The comprehensive 65-lesson course, complete with 7 kits, costs as little as \$370. Or you can choose the \$465 course that includes a 12" diagonal black & white portable TV for hands-on experience. Then there's the 19" diagonal solid-state color TV course for \$795; the advanced color TV course for trained technicians with an 18" diagonal color TV for \$645; and finally, the magnificent 25" diagonal solid-state color TV course, complete with console cabinet, oscilloscope, TV pattern generator, and a 3½ digit digital multimeter, for \$1,095. Other schools charge you hundreds of dollars more for an equivalent course.



in TV/Audio home choose NRI.

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Before you settle on any home training course, compare the over-all program. See if you are getting kits engineered for experimentation and training . . . or merely "hobby kits". Count the experiments . . . compare the components. Don't just count kits. (Some schools even call a slide rule a kit.)

Home study isn't a sideline with NRI. We've been its innovating leader for 60 years. Ask any of the hundreds of thousands of NRI graduates. They'll tell you . . . you can pay more but you can't buy better training.

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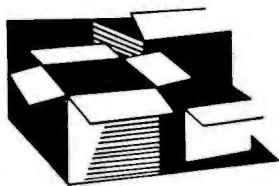
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New Products

Additional information on new products covered in this section is available from the manufacturers. Either circle the item's code number on the Reader Service Card inside the back cover or write to the manufacturer at the address given.

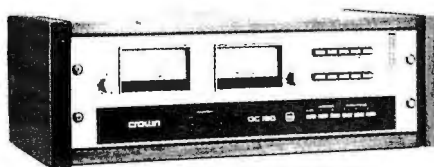
EICO DIGITAL LOGIC PROBE

The model DLP-6 Digital Logic Memory Probe can be used with DTL and TTL systems, and provides detection capabilities for pulse durations as short as 50 nanoseconds. The indicator system consists of three LED's. The bottom LED lights green for logic 1, the center LED lights red for logic 0, and the top LED lights yellow to indicate a positive- or negative-going transition. Each LED remains in the "on" stage for 200 nanoseconds regardless of pulse duration. A memory switch causes the LED to remain on permanently after a positive or negative pulse occurs. Available in either kit (\$19.95) or factory-assembled (\$29.95) form.

CIRCLE NO. 69 ON READER SERVICE CARD

CROWN STEREO OUTPUT CONTROL CENTER

Crown's Model OC-150 provides flexible control of an audio system. Output monitoring of three separate amplifiers is



provided by two meters, operating in either the average- or peak-reading modes with five full-scale ranges. Three speaker systems can be switched singly or in parallel by front-panel controls. Two headphone jacks have discrete levels of attenuation, for headphones with various degrees of sensitivity. The Crown OC-150 weighs 10 lb (4.5 kg) and measures 17" W x 8 1/2" D x 5 1/4" H (43.2 x 21.6 x 13 cm). \$299.00.

CIRCLE NO. 70 ON READER SERVICE CARD

TEMPEST LAB SERIES 1 SPEAKER SYSTEM

The Tempest Lab Series 1 loudspeaker system by the Tempest Div. of ESS, Inc. combines the high-frequency Heil air-motion transformer with a dynamic 12-inch woofer in a two-way bookshelf configuration. The long-excursion woofer is back-loaded through a low-frequency phased vent path,

resulting in bass response down to 30 Hz, according to ESS. Above the crossover frequency of 1500 Hz, the Heil "power ring" tweeter is active. A dual control panel allows for flexibility in response shadings. Power handling capacity is 60 W rms of continuous program material, 160 W on music peaks. A minimum amplifier output of 10 W rms is recommended. Available with a walnut vinyl finish, and foam grille options of brown, blue and rust. It measures 27" H x 15" W x 13-7/8" D (68.6 x 38.1 x 35.2 cm).

PIONEER AM/FM STEREO TUNER

Pioneer announces its most sensitive AM/FM stereo tuner, the Model TX-9500. Among the FM circuit features are three dual-gate MOSFET's in the front end, four dual-ceramic filters, an eight-stage limiter, a linear detector, phase-locked-loop multiplex demodulator, and a two-step muting



circuit. A built-in 440-Hz test tone, calibrated to correspond to 50% FM modulation, enables recordists to preset recording levels before taping program material. Two meters facilitate tuning. Rear panel connections are provided for multipath scope outputs, fixed and variable audio outputs, and a 4-channel MPX output jack for future discrete FM broadcasts. A two-position de-emphasis switch allows proper demodulation of regular and Dolby-encoded broadcasts. TX-9500 specs include a frequency response of 20-15,000 Hz +0.2 dB, -1.5 dB; stereo separation better than 35 dB between 50 and 10,000 Hz; and an FM sensitivity of 1.5 µV (IHF). Harmonic distortion is rated at less than 0.2% (stereo), stereo S/N at 75 dB, selectivity at 85 dB, and capture ratio at 1.9 dB. The tuner measures 16 1/2" W x 14 3/8" D x 5 7/8" H (42 x 36.5 x 14.9 cm). \$399.95.

CIRCLE NO. 71 ON READER SERVICE CARD

ADS MOBILE HIGH FIDELITY SYSTEM

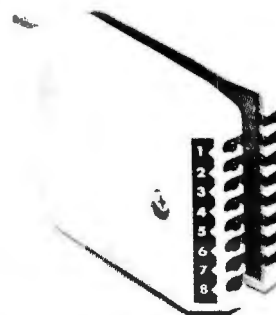
ADS introduces its Model 2001 high-power bi-amplified speaker system for use where space is limited and only 12 V dc is available—vans, campers, and boats. The two acoustic-suspension speaker systems contain specially designed 4-inch (10-cm) long-excursion woofers and 1-inch (2.5-cm) soft-dome tweeters. A total of 160 W rms is provided by four independent amplifiers, which are powered by a high-frequency dc/dc inverter. The system draws a maximum of 26 A from a 12-V storage battery. Frequency range of the 2001 is said to be 50-25,000 Hz (DIN). Each speaker enclosure weighs 4 lb (1.8 kg) and measures 6 7/8" H x 4 1/4" W x 4" D (17.5 x 10.8 x

10.2 cm). Power amplifiers measure 9 9/16" W x 6 1/2" D x 3 5/8" W (23.8 x 16.5 x 9.2 cm). The power supply (attachable to the amplifier module) is 6 1/4" W x 3 5/8" H x 3 1/2" D (15.9 x 9.2 x 8.9 cm). \$450.

CIRCLE NO. 72 ON READER SERVICE CARD

CONTINENTAL SPECIALTIES LOGIC MONITOR

Continental Specialties' Logic Monitor simultaneously displays static and dynamic logic states of DTL, TTL, HTL, and

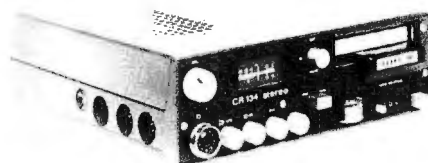


CMOS DIP IC's. Whenever the voltage at a pin exceeds 2 V, the numbered LED corresponding to that pin lights, indicating a logic one. The Logic Monitor clips onto the DIP, and requires no external power supply, calibration or adjustment. Input impedance is 100,000 ohms, and it draws a maximum of 150 mA at 15 V according to the manufacturer. The unit weighs 3 oz (85 g) and measures 4" L x 2" W x 1 1/2" D (10.2 x 5.1 x 3.8 cm). \$84.95.

CIRCLE NO. 73 ON READER SERVICE CARD

UHER PORTABLE CASSETTE DECK

Uher's Model CR134 portable stereo cassette deck features a special head design incorporating four tracks in-line, and a photo-sensitive electronic control for the



tape-drive mechanism. The deck has automatic tape reversal, built-in condenser microphone, a speaker, a stereo amplifier with a 1-W/channel output, and defeatable ALC. It can be powered from line current or rechargeable batteries. Frequency response is rated at 25 to 15,000 Hz ± 2 dB, S/N at 56 dB, and wow and flutter (rms) under 0.12%. Stereo and mono operation are possible. The CR134 measures 7" W x 7" D x 2" H (17.8 x 17.8 x 5.1 cm). \$378.

CIRCLE NO. 74 ON READER SERVICE CARD

PICKERING CD-4 QUADRAHEDRAL CARTRIDGE

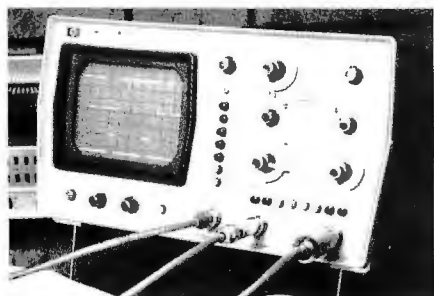
The new Pickering XUV/4500Q cartridge can play stereo, SQ, QS, and CD-4 discs while tracking at one gram or less. It is said to provide good frequency response and separation to beyond 50,000 Hz. The XUV/4500Q features the patented

Quadrhedral™ stylus assembly, with the Quadrhedron™ stylus tip, which is a new shape in diamond styli. In four-channel discrete playback, its frequency response is 10 to 50,000 Hz (± 1.5 dB in the base bands, ± 2 dB in the carrier bands), with a channel separation of 35 dB nominal at 1000 Hz, and 25 dB nominal at 30,000 Hz. The cartridge provides a nominal output of 3.4 mV at 5.5 cm/s. \$139.95.

CIRCLE NO. 75 ON READER SERVICE CARD

H-P 15-MHZ DUAL-TRACE OSCILLOSCOPE

A new 15-MHz dual-channel oscilloscope, the Model 1222A from Hewlett-Packard, has a built-in delay line to make visible the leading edges of traces. This feature is especially valuable in digital and pulse work. The Model 1222A also gives the user the option of viewing channels A and B in either the A+B or A-B modes. The scope is said to have 3% vertical accuracy, cali-



brated 8 x 10 cm display, internal graticule to eliminate parallax, dc coupling, triggered sweep and pushbutton beam-finder. Vertical calibration is adjustable from 2 mV/cm to 10 V/cm. Built-in TV sync separation makes possible automatic triggering on frame or line. The calibrated sweep is said to be accurate to within 4%. The Model 1222A also has AUTOMATIC or NORMAL triggering. The scope weighs 16¼ lb (7.3 kg), and requires 35 watts at 100, 120, 220, or 240 volts. \$895.

CIRCLE NO. 76 ON READER SERVICE CARD

HEATH LAB-GRADE POWER SUPPLY

The Model IP/SP272 is one of Heath's new 2700 Series of lab-grade power supplies with analog or digital readout. The power supply produces 0 to 15 V at 5 A, has a large 3½-digit readout, constant-current and constant-voltage operation, remote voltage and current programming, automatic compensation for lead voltage drops, and complete output protection, according to Heath. The digital readout has two-decade autoranging to provide good resolution for low voltage and current settings. Load regulation is rated at 0.05% + 1 mV for voltage, 0.1% + 3.5 mA for current. Built-in standards allow calibration to within +1.0% for voltage and within 1.5% for current. Closer tolerance is possible if lab standards are used. The IP/SP 2721 is available in kit (\$219.95) or assembled (\$340.00) form.

CIRCLE NO. 5 ON READER SERVICE CARD

SYLVANIA COLOR TV TEST JIG

GTE Sylvania's Model CK3000 test jig is said to be compatible with 7000 solid-state, tube, and hybrid color television chassis. It can be used with chassis generating anode voltages up to 30,000 V, and can handle delta 70- and 90-degree tube, hybrid, transistor, and SCR sweep circuitry with a range of impedances. A built-in alternate supply permits testing of focus voltages as low as 4500 V. A set of programmers for the jig's patented yoke circuit provides correct matching to six different receiver deflection outputs. The CK3000 also contains a 90-degree slotted-mask, in-line 13-inch (33-cm) CRT. Optional accessories are

adapter kits for seven popular name brands and discrete adapters for 41 more. The test jig weighs less than 25 lb (11.4 kg).

CIRCLE NO. 78 ON READER SERVICE CARD

PEARCE-SIMPSON MARINE RADIO TELEPHONE

The new Bimini 25 vhf FM marine radio-telephone features full legal (25 watts) power output, a backlighted channel selector knob with provisions for 12 transmit and 14 receive channels, a snap-on mounting cradle and quick-connect power plug. The solid-state transceiver also has a two-position transmitter output switch (25 watts high, 1 watt low), and a noise-canceling ceramic microphone. The re-

20 hi-fi watts in 1.2 cubic inches

What a powerhouse! SK3154 packs a 20-watt RMS audio amplifier in one small module. With virtually flat response from 15 Hz to 70 kHz. In the SK3154 package you'll find all the information you need. Just follow the instructions for adding 12 easy-to-get

passive components, power supply and hardware — and you've got one channel of a fine stereo or quad amplifier. The fun — and a super finished product — are yours. (Ten and 15-watt SK modules also available.) Start now! See your RCA electronics distributor.



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Electronic organ, temperature alarm, tachometer, light-operated switch — 68 useful solid-state projects in one book. Complete instructions plus some theory. \$2.95 optional price. At your RCA electronics distributor.

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CIRCLE NO. 38 ON READER SERVICE CARD



RCA

The CROWN VFX-2

electronic crossover

Commercial sound contractors across America have been asking for an electronic crossover for use on sophisticated sound installations. There's no more waiting. And the Crown VFX-2 embodies all you expect in high quality and performance capabilities from the people at Crown.

Only the Crown VFX-2 electronic crossover will give every installation **maximum** versatility. Such **flexibility** for so little cost. And never before has an electronic crossover been offered that can be easily and readily adjusted with front panel controls.

Tunable from 20- to 20,000 Hz, this solid state component is compatible with 600 ohms loads and up, and features both balanced and unbalanced inputs and outputs.

Overall noise and distortion are extremely low. IM distortion is less than 0.01% at rated output, and noise is more than 97dB below rated output with open inputs.

Providing either crossover or bandpass functions, the VFX-2 utilizes two continuously variable filters per channel, and filter roll-off is at a fixed 18 dB/octave.

Applications include stereo bi-amping, mono tri-amping, and combining the bandpass filter with the normal two-way crossover on a mono signal. And all connections are quarter-inch phone jacks for positive electrical contact.

The VFX-2 is designed for standard 19" rack mounting and measures in at 3½" high by 5¾" deep and includes a clear plastic cover for protecting control settings.



Write for complete specifications.


crown

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CIRCLE NO. 15 ON READER SERVICE CARD

ceiver section claims a sensitivity of 0.7 μ V, a spurious signal and adjacent channel rejection of 50 dB. The Bimini 25 requires a 13.6-V dc source, and draws 5 A on transmit (high), 1 A on low, and 0.15 A during receive. The transceiver weighs 3.5 lb (1.6 kg), and measures 11" W \times 6½" D \times 3" H (27.9 \times 16.5 \times 7.6 cm).

CIRCLE NO. 79 ON READER SERVICE CARD

AKG STEREO HEADPHONES

Philips Audio Products' Model K-140 lightweight headphones have earcups that are universally jointed, allowing flexible



positioning. Bass response is said to be unaffected by the shape of the listener's ears, or by air leaks between the ears and cushions. Microphone-derived transducers are used and are said to deliver very transparent sound images. \$34.50.

CIRCLE NO. 80 ON READER SERVICE CARD

GRILLE FOAM ADD-ON KITS

A series of speaker grille replacement kits, featuring sculptured acoustic foam, available from the Dew Foam Company, are said to be acoustically transparent, and easy to install. They are available in brown and black, and can be painted with any color acrylic or lacquer paint. The grille is cut to size, and applied using pressure-sensitive material which is supplied. Kits are available for three sizes of speaker enclosures: **SMALL** (up to 10¼" \times 16¾" or 26 \times 42.5 cm); **MEDIUM** (up to 13¾" \times 23¾" or 34.9 \times 60.6 cm); and **LARGE** (up to 16¾" \times 28¼" or 42.9 \times 71.8 cm), and are priced at \$6.95, \$9.95, and \$14.95, respectively. Address: Dew Foam Co., 14768 Raymer St., Van Nuys, CA 91405.

REAR-MOUNTED AUDIBLE INSTRUMENT ALARM

Floyd Bell Associates' Model AL-100-RM is an audible alarm designed for rear-panel installation. The unit produces a continuous tone at about 2600 Hz, with a sound output to 90 dB. In operation, the alarm draws 4 to 16 mA from a 5- to 30-V dc source. Tin-plated screw-type terminals are used. The AL-100-RM is said to have sealed electronics, and can be used in marine and commercial applications at temperatures from -20° to +65°C (-4°F to 149°F). Address: Floyd Bell Associates, Inc., 555 Marion Road, Columbus, OH 43207.

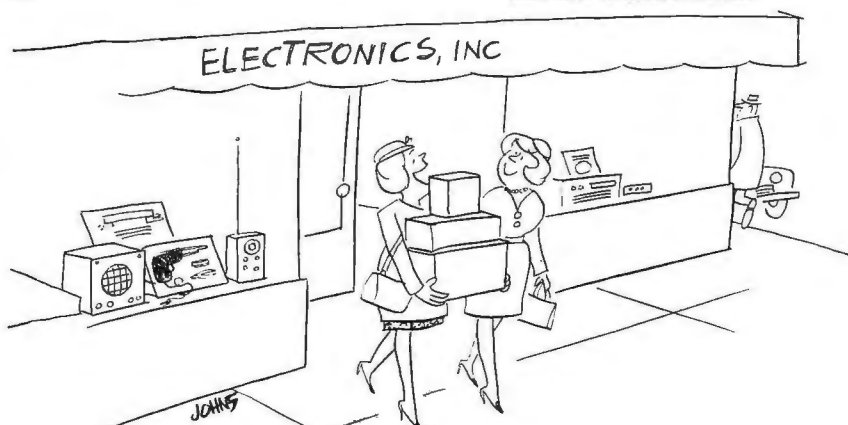
BOZAK AUDIO SIGNAL PROCESSOR

The Bozak Model 919 Audio Signal Processing Center permits the user to blend three different two-channel input signals with separate level, bass, mid-range, and treble controls for each input. Input channels include phono, microphone, and switch-selected choice of tape, tuner, or

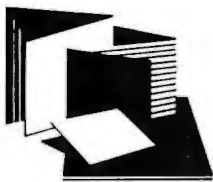


auxiliary inputs. A "panning" circuit allows the user to "locate" the microphone anywhere between the right and left channels, and the stereo blend control varies the "width" of the output from mono (in which the sound comes from one spot) to extra-wide (in which the sound source appears to have a wider frontal area). A "cue selector" makes it possible to monitor each of the inputs separately. Claimed distortion is less than 0.1% from 20 to 20,000 Hz with a full 10-volt output into a 200-ohm load. The unit weighs 21 lb (9.5 kg) and measures 17¾" W \times 10¾" D \times 7" H (45.1 \times 27 \times 17.8 cm). An optional walnut enclosure is available. \$797.

CIRCLE NO. 81 ON READER SERVICE CARD



"I'll say one thing for Charles.
He's no problem on birthdays and Christmas."



New Literature

NSC PRODUCT GUIDE

National Semiconductor has published a 15-page guide to some 300 functional products that make up its line of bipolar TTL/MSI devices. The guide is divided into eight sections: multiplexers and demultiplexers, counters, display products, memory products, shift registers, latches and storage registers, decoders and comparators, and miscellaneous TTL products. Address: Marketing Services Dept., National Semiconductor Corp., 2900 Semiconductor Dr., Santa Clara, CA 95051.

IDI INDICATOR LIGHTS

A comprehensive 24-page selection guide to pilot and indicator lights is available from Industrial Devices Inc. It reviews the specifications of a variety of custom, stock, and off-the-shelf lights in three different light sources: neon, incandescent, and

solid-state, and compares the advantages and disadvantages of each. Address: Industrial Devices Inc., Edgewater, N.J. 07020.

DATA CONVERSION APPLICATIONS NOTE

A six-page applications note from Datel Systems, called "Know Your Conversion Codes," is a handy summary of the various digital codes used in data conversion modules. Various codes such as straight binary, complementary binary, BCD, complementary BCD, offset and complementary offset binary, sign-magnitude BCD, and two's complement are discussed in detail. Also covers code relationship to internal circuitry in the conversion module. Address: Datel Systems, Inc., 1020 Turnpike St., Canton, MA 02021.

AMATEUR RADIO EQUIPMENT CATALOG

The new catalog from MFJ Enterprises describes many new products, including CW and SSB audio filters, electronic keyers, frequency standards, audio amplifier modules, QRP rigs, pc boards, and electronic components. Address: MFJ Enterprises, Box 494, Mississippi State, MS 39762.

CRYSTAL OSCILLATOR GUIDELINES

An applications bulletin from Vectron Labs, entitled "How to Specify Crystal Os-

cillators," covers clock oscillators, TCXOs, and oven-controlled oscillators; includes 16 diagrams and illustrations. A comparison of these oscillator types is given, as well as a discussion of timing applications. Address: Vectron Laboratories, Inc., 121 Water Street, Norwalk, CT 06854.

RECEIVING TUBE PRICE LIST

A new 12-page Export Price List covering more than 2,000 receiving tube types is available from the International Components Corp. This list contains many American, Japanese, and European consumer and industrial receiving tubes, including many classic and antique types. Address: International Components Corp., 105 Maxess Rd., Melville, NY 11746.

IEEE STANDARDS CATALOG

The new 32-page IEEE Standards 1975 Catalog lists more than 350 standards publications by subject as well as numerical sequence. Standards developed by the IEEE cover test methods, installation practices, units, definitions, symbols, and applications methods. Among the standards listed are those which deal with antenna design, communications, power generation and distribution, microwaves, rotating machinery, and electromagnetic compatibility. Address: IEEE Standards Dept., 345 E. 47th St., New York, NY 10017.

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Most of you know the evaluation of automotive electrical systems . . . an evaluation characterized only occasionally by efficiency and performance. I know that, and that's why I use the Delta Mark Ten B CDI on all my cars, new and old. And believe me, you don't have to have a new car to appreciate the best electronic ignition available today. Study these features and you'll know what I mean.

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Mark Ten B, kit	\$49.95 ppd	Deltakit®	\$34.95 ppd

CIRCLE NO. 17 ON READER SERVICE CARD



Stereo Scene

CHOOSING YOUR FM ANTENNA

By Ralph Hodges

FROM its beginning, FM has supplied entertainment and information to a great number of people. Of course, many cannot afford the ultimate in an FM tuner; but being dependent on the airwaves, they often have a strong desire to own such a paragon to obtain exciting performance in terms of low distortion, high signal-to-noise ratio, and good stereo separation. But a "super tuner" does not, as an automatic consequence, necessarily provide the ultimate in signal-pulling power, number of listenable stations, and freedom from external interference.

There's a large distinction to be made between a tuner's function as a *receiver*—that is, as a potent grabber of airborne electromagnetic radiation—and as a *signal processor*, which is the role it plays once it has that

clean, strong signal in its grasp. Many "super" tuners, while designed to excel in both areas, surpass the performance of their lesser brethren mostly in the signal-processing functions (low distortion, noise, etc.). As *receivers*, their superiority may not be so pronounced. So in practice, what this means is that someone with reception problems could possibly find a readier cure by adding a very good FM antenna to an adequate tuner. I realize that is an easy statement to make, because the problem is where and how to find that very good antenna. The various designs that are available can be confusing, to say the least.

I don't think antenna designers are by nature secretive men, but they tend not to launch into full-dress discussions of their trade with the greatest

enthusiasm. You might think they were wary of unscrupulous imitators, except that all of their work is usually right out in the open—literally on rooftop display—to inspect and copy if you're so inclined. No, the real cause of their reticence seems to lie in the craft itself, which is more than commonly resistant to textbook solutions.

The consumer should not despair, however. Armed with a little savvy about antenna terms and specifications, and a knowledge of what he needs for his location, he can get the desirable, "very good" FM antenna.

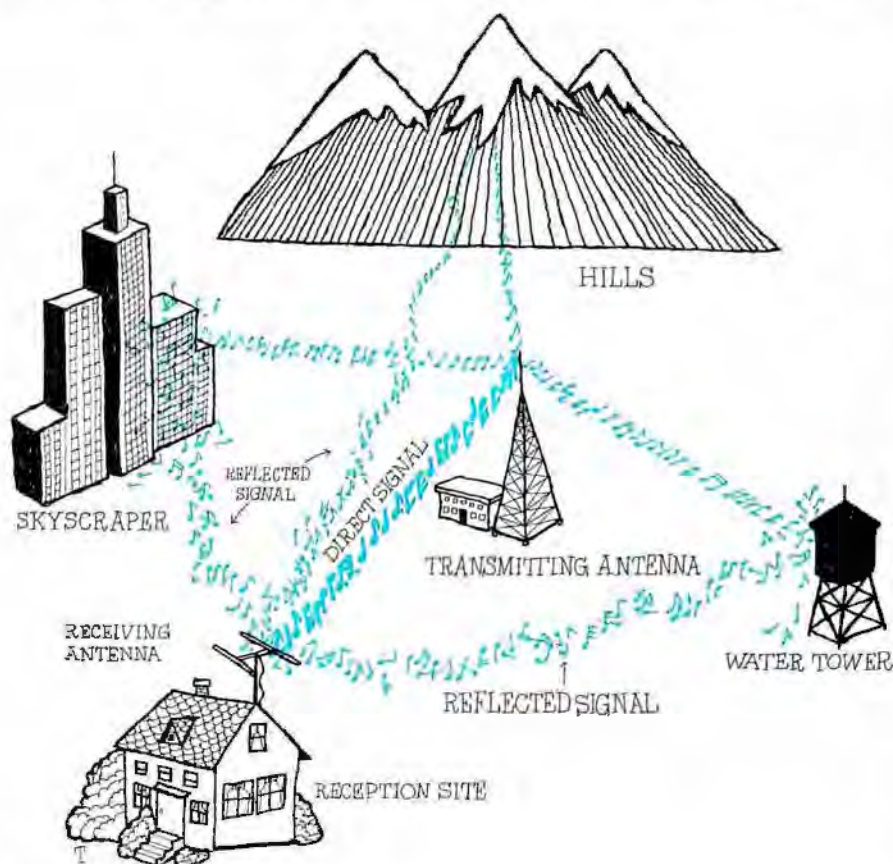
Gain. A primary function of an antenna is, of course, to provide the receiver with the strongest possible signal. So an antenna should have high sensitivity or high gain. Gain over what? Gain over a dipole, the simplest type of efficient antenna, with two metallic rods cut to the proper length to receive FM frequencies as shown in Fig. 1. The antenna's directional response is roughly like a figure-eight, with best results at 90° and 270°. Those signals coming in on-end are not received too well.

The dipole is the reference antenna that is used in comparing more complex designs. It is the cheapest to make, and one of its forms (the "folded" dipole) is often included in the "package" with a tuner as a T-shaped piece of TV-type lead-in.

For years, antenna design concentrated on gain as a way of overcoming the noisy front ends of typical r-f receivers. Now some experts believe that the best possible results have been achieved, given present-day techniques and materials, and the emphasis is shifting to *directionality*.

Directionality. With tuners as quiet and sensitive as they are today, extremely high antenna gain is no longer such a necessity, except in some rural areas. In fact, it can be a liability if it is available to *all* signals impinging on the antenna.

Remember that the sky is crowded, with (potentially) hashed-up versions of the very signal you want to receive. I refer here to the phenomenon called multipath reception—the simultaneous reception of one signal from multiple sources. Only one of the sources is the transmitting antenna. The others are reflectors of the signal, such as hills, water towers, tall buildings, and anything else that rears itself high enough above the terrain and



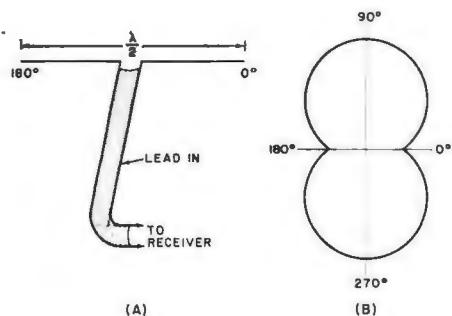


Fig. 1. Simplest antenna is the half-wave dipole (A). Its polar diagram is shown at (B).

contains a significant amount of conductive material. Like billiard cushions, they bounce the signal away from its straight-line path. Then one of these reflected signals can hit your antenna as well as the signal straight from the transmission site. But what's wrong with that?

What's wrong is that the reflected signal arrives at your antenna later than the direct one, since the reflection requires it to travel a longer route. Then the two signals experience phase interference and the result is some ugly distortion of the original broadcast waveform.

Multipath causes ghosts in TV reception and rasping distortion in FM. The latter is particularly noticeable at high audio frequencies and during loud musical passages. It is curable, much of the time, if the receiving antenna is highly directional since no late reflections of significant strength will arrive from precisely that same direction.

Antennas And Tuners. A high-gain antenna will help any tuner rise above its basic sensitivity specification and provide noise-free reception of stations that may have been out of range before. A highly directional antenna will have the same effect on other tuner specifications—capture ratio, AM suppression, and selectivity, to name a few. Selectivity is simply a tuner's ability to reject broadcast frequencies close to the one to which it is tuned. If you can aim your directional antenna away from the offending stations and right at the one you want to receive, you save the tuner the trouble of trying to sort things out internally. (If the interfering stations lie in the same direction as the desired one, the antenna usually can't do much, however.)

Good capture ratio and AM suppression are assets to any tuner in eliminating multipath effects. Capture

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ratio specifies the tuner's ability to reject weaker signals at essentially the same frequency as the desired one (note that multipath has the same average frequency as the direct signal, and is also usually weaker), while AM suppression has to do with fluctuations in the desired signal's strength before it reaches the tuner's input (such fluctuations are due to multipath and a host of other interference factors). Respectively, the two specifications refer to a tuner's effectiveness in ignoring spurious FM and also AM effects on the incoming signal. The better tuners are astonishingly good at this, but an appropriate antenna can be even better. A highly directional antenna helps the tuner's capture ratio by making reflections much weaker than the direct signal. A tuner's AM suppression is profited by both high gain and high directionality.

Which Antenna? There are four basic types of antennas available to the FM enthusiast: outdoor beams (both "yagi" and "log-periodic" types) which are exclusively for FM, outdoor TV antennas, indoor FM "rabbit ears" and simple indoor dipoles. Which is right for you? That depends on where you live, what you listen to, and what kind of a tuner you have.

The typical rooftop FM antenna is a variant of the yagi or log-periodic principle. Sometimes it's a hybrid of the two. A pure yagi has only one active crossbar ("element") connected to the tuner. The other elements are "parasitic," either directing the signal to the active element or reflecting it back. (The reflection here won't cause multipath.) The log-periodic design connects several elements to the tuner input, and these elements "couple" in mysterious ways to provide gain over a more-or-less wide range of frequencies. Whatever the principle, the elements progressively increase in length so that, observed from above, the antenna assumes an arrowhead shape that should be pointed at the desired station's antenna (Fig. 2).

Both of these antennas can be very high in directionality and gain. Both also have their shortcomings: impedance variation (responsible for losses in the antenna-tuner coupling), limited bandwidth, and susceptibility to interference. I wish I could advise as to which of these weaknesses is most tolerable, but the fact is that it depends on local (sometimes very local) reception conditions. The best antenna for you can't be readily pinpointed by even the most expert of experts. An adequate antenna is the one your next-door neighbor likes.

Other Solutions. A TV antenna can serve very well for FM unless it has an FM trap (optional on most large outdoor antennas). The FM band is located in approximately the center of the vhf TV band. Often there is interference between the two, so the trap is used to wipe out the interloping FM from the TV.

Assuming there is no trap, using the same antenna for both TV and FM introduces lots of other potential problems. Sometimes it will work fairly well when the antenna is connected directly to both. More often, a so-called "signal splitter" is required. Even then, there may be trouble. The TV screen is usually the first to suffer, with snow starting to appear.

Can you find happiness with an indoor antenna such as the familiar rabbit ears? Many authorities resist the idea, but it seems to be possible—particularly in urban areas where multipath rejection is more important than gain. They are mildly directional and insensitive to signals arriving from the sides. Their great advantage over a twin-lead dipole is that they are rigid (therefore easily rotated and aimed) and their telescoping elements are tunable to various wavelengths. But rabbit ears don't offer exciting performance in any case.

The final alternative is to build your own antenna, and sometimes excellent results can be obtained. But that is a subject we can't pursue here.

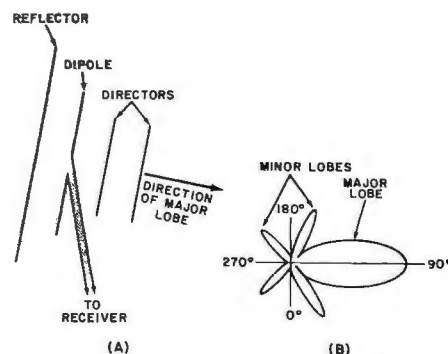


Fig. 2. Typical four-element beam (A) has directional polar plot (B).

Accessories. After you've chosen an antenna—presumably an outdoor one if you can manage it—your subsequent decisions will involve the proper lead-in cable and whether or not you need a rotator.

There are two basic types of lead-in: coaxial (or unbalanced) and twinlead (balanced). Coax is immune to positioning and weather, and some types have low losses. Its characteristic impedance (for RG-59) is 75 ohms. If a balanced antenna or tuner input is to be used with coax, it is necessary to use a "balun" (balanced-to-unbalanced line converter).

Balanced line can be used, but if it is not of the shielded variety, some problems may arise. If unshielded twinlead is bent sharply, run close to a metal object or gets wet, its nominal 300-ohm impedance can take off into the blue. This type of line also deteriorates badly after some exposure to the elements. The problems involved in using unshielded twinlead are often such that it is hardly worth bothering with. Shielded twinlead, if you can find it, is weather-sealed, shares the noise-immunity characteristic of coax, and has lower losses.

A rotator—an electric motor mounted on the antenna mast to point the antenna toward the direction of interest—plays no part in the inherent performance of an antenna. It is, however, necessary if you want to aim a good directional antenna at stations lying at different compass points. ♦

UPCOMING AUDIO SHOWS

October 10-12
October 31-November 3

BALTIMORE HI-FI SHOW
AUDIO ENGINEERING SOCIETY
(52nd Convention)

Location to be determined
Waldorf-Astoria Hotel, NYC

November 6-10
February 12-16, 1976
March 12-14, 1976

PHILADELPHIA HI-FI SHOW
DETROIT HI-FI SHOW
SAN DIEGO HI-FI SHOW

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news HIGHLIGHTS

GE Leaving Phono Business

General Electric has announced it is getting out of the portable phonograph business. The company is closing its last audio manufacturing facility in Decatur, Ill., where it produces phonos, changers and Show 'N Tell phono viewers, among other products. However, inventory will allow GE to market products at least through 1975.

Economic Ups and Downs

The EIA's Consumer Electronics Group reports that 1974 consumer electronic sales were the third highest in the industry's history. However, they were down 11.8% from 1973, the record year. In two other areas, substantial gains are expected in 1975. Litton Industries predicts that industry sales of home microwave ovens will exceed 900,000 units, representing a retail market of \$360 million. That would be a 25% increase over 1974 sales. The Air Conditioning and Refrigeration Institute projects that sales of electronic air cleaners, which remove a large portion of dirt, pollen, and smoke from indoor air, will pass 200,000 units in 1975. Annual sales were 10,000 units in 1960, 100,000 in 1970, and about 194,000 in 1974.

IC's In The Body

Researchers are now readying biomedical sensors using IC's for actual insertion in the body. This will allow a doctor to monitor biological activities of his patients during their normal routines. Data from the sensors can be transmitted to a nearby receiver, which is linked to a diagnostic unit in the doctor's office by a telephone connection. It is possible that, in the future, medical check-ups will involve nothing more than dialing your physician and moving within range of your telemeters. Any bioelectric phenomenon, such as EKG, EEG, muscular activity and nerve transmissions could be monitored in this way.

Checkless Bill Paying

"Pay-by-Phone" service, a computer-based method of checkless bill-paying, allows a subscriber with any type of Touch-Tone telephone to initiate a transaction by punching out code numbers identifying his bank account, personal security code, payee, and amount, either to an automated or live teller. Subscribers with conventional rotary dial phones can use the service by giving the same information to a customer service representative. A verified bank statement is provided as proof of payment. The system eliminates check writing, addressing envelopes, applying postage, and manually posting payments. It can also be extended to permit payments to be made from savings accounts as well as conventional checking accounts. Telephone Computer Service of Seattle is the developer. The first fully operative Pay-by-Phone system is operated by a bank in Minneapolis. If and when your bank is prepared to offer the service, they will undoubtedly let you know.

Electronic License Plates

An electronic license plate is being developed that may some day play an important role in automobile operation. The license plate is a microwave transceiver which would automatically communicate with official vehicles. It could respond with an identifying code number when electronically interrogated, and serve as a transponder for use in a cooperative-avoidance radar. The plate includes an r-f detector, a frequency doubler, a modulator, and an antenna. It would be about 12 inches long, 6 inches high, and half-an-inch thick. Covering the circuitry would be a plastic radome displaying the license number of the vehicle. Other uses might include an automatic speeding indicator, toll-billing device, and reception of safety messages about road and weather conditions.

Recording "Firsts"

RCA Records has released Massenet's "Thais" as the first opera to be recorded in full-surround discrete four-channel sound. It stars Anna Moffo, in the title role, Jose Carreras, Gabriel Bacquier, and Justino Diaz, with Julius Rudel conducting the New Philharmonia Orchestra and the Ambrosian Opera Chorus of London.

Anagram, a Springfield, Va. computer firm, is set to tackle the highly competitive music industry with its 13-rank Wurlitzer Theatre organ and a computer named "Genii." According to the company, development of the computer permits exploration of utilization of computers in the music field. The "Musictran" translation of written music to computer language is processed by the "Marvel" computer program developed by Anagram. Its first album, "Two Loves Have I: Jean and Genii," is produced mainly for organ and computer buffs and to demonstrate the capabilities of both the organ and the computer.

Bicentennial Amateur Callsigns

The FCC has authorized amateurs to use special callsigns during the bicentennial celebration year, 1976. Use of the call letters will be optional, and no notification to the Commission will be required. Callsign prefixes or prefixes plus digit can be changed in accordance with the following:

WA—AA	KH6—AH6
WB—AB	KJ6—AJ7
W—AC	KL7—AL7
K—AD	KM6—AH7
WD—AE	KP4—AJ4
WR—AF	KP6—AIΦ
WN—AK	KS4—AH4
KB6—AG2	KS6—AH3
KC4—AL4	KV4—AJ3
KG6—AG6	KW6—AG7

These special callsigns can be used from 0500 GMT January 1, 1976 until January 1, 1977. Suffixes remain unchanged.

MITS Altair Computer Report A Computer Language You Can Understand

ALTAIR BASIC is an inexpensive, general-purpose computer language with the power for advanced data processing. It is easy to learn and to use.

ALTAIR BASIC is part of the overall MITS computer concept. That is, **computers must be made understandable and affordable.**

ALTAIR BASIC comes in three versions. The first of these is a 4K BASIC designed to run in an Altair with as little as 4,000 words of memory. This powerful BASIC language has **6 functions** (RND, SQR, SIN, ABS, INT, and SGN) in addition to **15 statements** (IF . . . THEN, GOSUB, RETURN, FOR, NEXT, READ, INPUT, END, DATA, LET, DIM, REM, RESTORE, PRINT, STOP and **4 commands** (LIST, RUN, CLEAR, SCRATCH).

The second ALTAIR BASIC option is the 8K BASIC designed to run in an Altair with as little as 8,000 words of memory. This BASIC language is the same as the 4K BASIC only with **8 addi-**

tional functions (COS, LOG, EXP, TAN, ATN, INP, FRE, POS) and **4 additional statements** (ON. . . GOTO, ON . . . GOSUB, OUT, DEF) and **1 additional command** (CONT). This BASIC has a multitude of advanced STRING functions and it can be used to control low speed devices—features not normally found in many BASIC languages.

The third ALTAIR BASIC is the EXTENDED BASIC version designed to run on an Altair with as little as 12,000 words of memory. It is the same as the 8K BASIC with the addition of PRINT USING, DISK I/O, and double precision (13 digit accuracy) add, subtract, multiply and divide.

ALTAIR BASIC is only the beginning. MITS is currently engaged in an extensive software development program. Our Disk Operating System is scheduled for delivery in August. Other software now available includes an Assembler, System Monitor, and Text Editor.

ALTAIR USERS GROUP

The Altair Users Group is both a means of communication among Altair Users and a method of building a comprehensive library of Altair Programs. All Altair purchasers are entitled to a free, one year membership in this group.

Members of the Altair Users Group are encouraged to submit programs by entering Altair "Software Contests." Winners of these contests are awarded **prizes of up to \$1,000** credit toward the purchase of an Altair Computer or Altair options.

Contest winners are announced in the Altair newspaper, **Computer Notes**, which is published monthly and mailed free to all members of the Altair Users Group. **Computer Notes** contains complete update information on Altair hardware and software developments, programming tips, general computer articles and other useful information.

Associate Memberships are available to non-Altair customers for only \$30.00 a year. Membership fees are refunded to Associate Members who buy an Altair Computer within 8 months after they become a member.

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For an Altair Computer kit, send in your used computer plus a check for \$561.00 (\$439.00 for an Altair plus \$264.00 for memory plus \$8.00 for postage and handling minus \$150.00). For an assembled Altair with 4K of memory, send in your used computer plus a check for \$817.00.

PRICES

Altair Computer kit with complete assembly instructions	\$439.00
Assembled and tested Altair Computer	\$621.00
1,024 word memory board	\$176.00 kit and \$209.00 assembled
4,096 word memory board	\$264.00 kit and \$338.00 assembled
Full Parallel Interface board	\$92.00 kit and \$114.00 assembled
Serial Interface board (RS232)	\$119.00 kit and \$138.00 assembled
Serial Interface board (TTL or teletype)	\$124.00 kit and \$146.00 assembled
4K BASIC Language (when purchased with Altair, 4,096 word memory and Interface board)	\$60.00
8K BASIC Language (when purchased with Altair, 2 4,096 word memory boards and Interface board)	\$75.00
EXTENDED BASIC (when purchased with Altair, 3 4,096 word memory boards and Interface board)	\$150.00

NOTE: Altair Computers and software come with complete documentation and operating instructions. BASIC language is available on either paper tape or cassette tape (specify). Warranty: 90 days on parts for kits and 90 days on parts and labor for assembled units. Prices, specifications and delivery subject to change.

ALTAIR TIME PAYMENT PLAN (kits only)

The Altair time payment plan allows you to be the owner of an Altair Computer with 256 words of memory for **just \$68.75 a month**. Each month (for 8 months) you send in your payment and we send you part of an Altair kit until you have the complete system. The advantages to this plan are: **NO interest** or financing charge, **GUARANTEED** price based on today's price, and free, immediate **membership to the Altair Users Group**.

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Month Four	\$68.75	Case with hardware
Month Five	\$68.75	1K Static Memory Board with 256 words of memory
Month Six	\$68.75	CPU Board with all components except processor chip
Month Seven	\$68.75	Control Board with all components
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HOW TO PROGRAM READ-ONLY MEMORIES

*An experimenter's guide to programmable ROM's—
what they are and practical applications for them.*

BY ROBERT D. PASCOE

PROGRAMMABLE read-only memories are unique among the digital integrated circuits readily available to experimenters. What makes it unique is that it is user programmable. You decide what you want the PROM to do and program it to do just that. The only "tools" you need are a pair of regulated power supplies, some switches, and a resistor. The programming procedure itself is outlined later on in this article.

The PROM is one member of the standard ROM family of memories. Once it is programmed, its memory is nonvolatile, which means that, if power is removed from and then reapplied to the PROM, the stored information remains intact. By contrast, a RAM (random-access memory) has a volatile memory; if power is interrupted, when it is again applied, whatever information was stored in the memory will be erased.

The ROM (and PROM) can be made from bipolar transistors, in which case it is called a bipolar ROM. It can also be made from metal oxide semiconductor devices, which makes it a MOS-ROM. Whichever type it is, the ROM is a digital device that "remembers" information on the standard binary format of 1's and 0's. The logic levels remembered by the bipolar

ROM are the same as those used in TTL circuits, whereas the levels remembered by the MOS-ROM are determined by the supply voltage required by the device itself.

Organization. An important characteristic of the ROM is its organization. The ROM remembers quantities of binary "bits" that are organized into "words." Each word has a certain number of bits. For example, one type

of ROM can remember 256 bits of information organized into 32 words of eight bits apiece ($32 \text{ words} \times 8 \text{ bits} = 256 \text{ bits}$).

Some of the more commonly available ROM's can remember 256, 1024, 2048, or 4096 bits in a single IC chip. With the various types of ROM's, the manufacturer determines how the total number of bits is organized in the chip.

The organization of the bits deter-

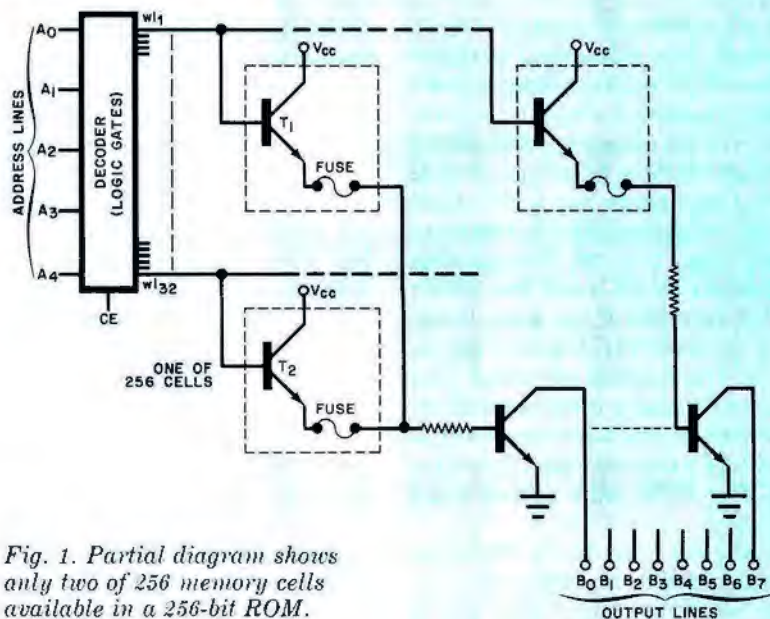


Fig. 1. Partial diagram shows only two of 256 memory cells available in a 256-bit ROM.

SOME APPLICATIONS FOR PROM's

THERE are countless applications for the ROM. Some of the more traditional ones use the ROM as lookup-table (trigonometry, logarithms, etc.) memories in calculators; as micro-instruction systems in computers; and character generators for displaying alphanumeric characters on a CRT screen. The following are examples of what you can do with an 8223 PROM:

Character Generator. A seven-segment display device can be used to create the numerals 0 through 9, a number of upper- and lower-case letters of the alphabet, and some mathematical punctuation—all with a single 8223 PROM chip. Because the display has only seven segments, it cannot form all 52 upper- and lower-case or even all 26 upper- or lower-case letters.

In Fig. A is shown the logic diagram for an alphanumeric/punctuation generator. Beside it is the "truth table" we used for generating the 32 possible characters. Note that the entire memory storage capability is "used up" in this truth table. (This truth table

assumes a buffering transistor between the outputs of the 8223 and segments of the display. The display can be either an RCA 2100 incandescent or common-anode LED display. For common-cathode LED displays, all B_0 through B_7 logic levels must be reversed.)

All eight output lines from the 8223 PROM are used, with one output assigned to each segment of the display and a final one for

Figure Displayed	Address (A_4-A_0)	Outputs (B_7-B_0)	Segments on
0	00000	00111111	abcdef
1	00001	00000110	bc
2	00010	01011011	abdeg
3	00011	01001111	abcdg
4	00100	01100110	bcfg
5	00101	01101101	acdfg
6	00110	01111101	acdefg
7	00111	00000111	abc
8	01000	01111111	abcdefg
9	01001	01101111	abcdfg
.	01010	10000000	decimal point
-	01011	01000000	g
=	01100	01001000	dg
A	01101	01110111	abcefg
b	01110	01111100	cdefg
C	01111	00111001	adef
c	10000	01011000	deg
d	10001	01011110	bcdeg
E	10010	01111001	adefg
F	10011	01110001	aefg
G*	10100	00111101	acdef
H	10101	01110110	bcefg
h	10110	01110100	cefg
i*	10111	00010000	e
J	11000	00011110	bcde
L	11001	00111000	def
n*	11010	01010100	ceg
o	11011	01011100	cdeg
P	11100	01110011	abefg
r*	11101	01010000	eg
U	11110	00111110	bcdef
u	11111	00011100	cde

*These letters are only approximations, included only to use up the PROM's program capability.

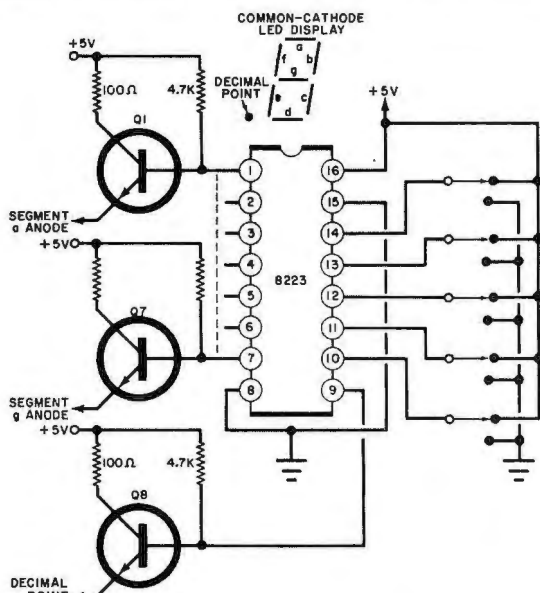


Fig. A. Once PROM is programmed according to truth table at right, it can generate numbers, letters, etc., on 7-segment display device.

mines the number of address (input) and output lines that will be available in a given ROM. Address input pins are the means by which a specific word in the memory is accessed or selected. If a particular ROM is organized with 32 words of eight bits per word, each word can be addressed with five input address lines ($2^5 = 32$). The address 00000 would be for word one, 00001 for word two, 00010 for word three, and so on until 11111 would be for word 32. The number of output pins for a small memory is determined by the number of bits used per word in the memory's organization. In our example, the ROM would have eight output pins.

The address lines for a ROM are usually denoted by the legends A_0 , A_1 , A_2 , etc., while the output lines would

be denoted by B_0 , B_1 , B_2 , etc. For a five-address-line input and eight-line output ROM, the address pins would be labelled A_0 , A_1 , A_2 , A_3 , and A_4 , and the output pins would be labelled B_0 , B_1 , B_2 , B_3 , B_4 , B_5 , B_6 , and B_7 .

Illustrated in Fig. 1 is a basic 256-bit (32-word by eight-bit) bipolar ROM. The address lines are fed to logic gates that decode the 32 possible combinations of 1's and 0's that appear on the five address lines. These 32-word lines are denoted by the legends w_1 through w_{32} . For the particular ROM shown, there are eight output transistors whose collectors are labelled B_0 through B_7 . The memory "cells" are denoted by the legends T_1 and T_2 . There are 256 of these basic memory cells for a 256-bit ROM.

The output lines from the ROM

would be either high (logic 1) or low (logic 0), depending on whether or not a conduction path exists between the memory cell and the output transistor in each line. As an example, if a 0 is to be stored at B_0 in word 32, the T_2 resistance link (fuse symbol) must be present. If, on the other hand, a 1 is to be stored at B_0 of word 32, the fuse must be electrically removed (blown) from the circuit.

Most ROM's have a pin labelled CE, for "chip enable," that permits the output to be isolated from the rest of the circuitry inside the IC. So, if a 1 is placed at CE (while the address is being changed), the outputs will be at the logic-1 level. The placement of this specific binary information into the ROM is called "programming." The means of programming is determined

the decimal point. To use up the entire storage capability of the PROM, the entire 00000 through 11111 series was used on the address lines (A₀ through A₄). We will discuss later how to perform the actual "programming" procedure for the PROM.

An extension of the single-character generator is the word generator. Here, we have several PROM's and an equal number of displays, each programmed with identical information. Depending on the number of PROM's and displays desired, this system can be used to generate words, strings of numbers, identification and license numbers, etc. You simply set the address lines of each PROM to generate the character you want.

Model RR Track Patterns. The PROM can also help an HO model railroader remember track patterns for his train layout. As an example, suppose an HO train layout has eight track switches and 10 possible track configurations. A PROM can be used to remember the positions of the various switches for the 10 possible track patterns, as shown in Fig. B. The outputs of the PROM would be connected to the track switches through electronic switches (driver transistors). This ensures that the output voltage levels of the PROM are converted to the proper voltages and currents needed to move or position the track switches.

The PROM must be programmed with the appropriate binary codes. The words w₁ through w₁₀ can then be the various track patterns that the train can have. The one-shot multivibrator's output is coupled to the CE input of the PROM so that the switches do

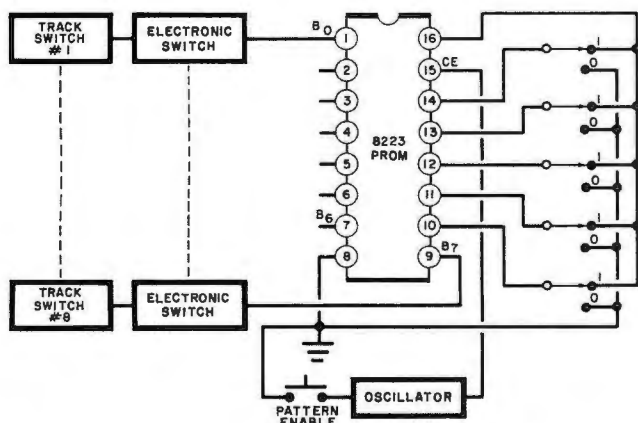


Fig. B. In model-railroad system, PROM would be programmed to control all possible combinations of switches on track.

by the type of ROM. The two major types of ROM's are the custom-programmed and the field-programmable ROM.

With custom-programmed ROM's, the manufacturer places the binary information (links or no links) into the memory as specified by the user. Custom programming of ROM's can be very expensive when only small quantities are ordered. To reduce the high cost of small quantities of ROM's, manufacturers offer the field-programmable ROM or PROM.

The PROM is an ordinary ROM that has all of its on-chip fuses intact. A 256-bit PROM would have 256 of these fuses, one for each bit of memory. The user can program information into the PROM simply by blowing selected on-chip fuses. The fuses are blown

open by passing a specific amount of current through them for a specified period of time. (The Signetics 8223 is an example of a 256-bit PROM. It is readily available from a number of surplus-parts suppliers for about \$4.50. This PROM is organized into 32 words of eight bits per word.)

Erasable PROM's. ROM's are usually thought of as having permanent binary information programmed into their memories. Once information is programmed into an ordinary ROM, it cannot be altered. Recently, however, a new type of PROM—the erasable PROM—has become available. This type of PROM permits information stored semi-permanently to be erased and new information to be reprogrammed in.

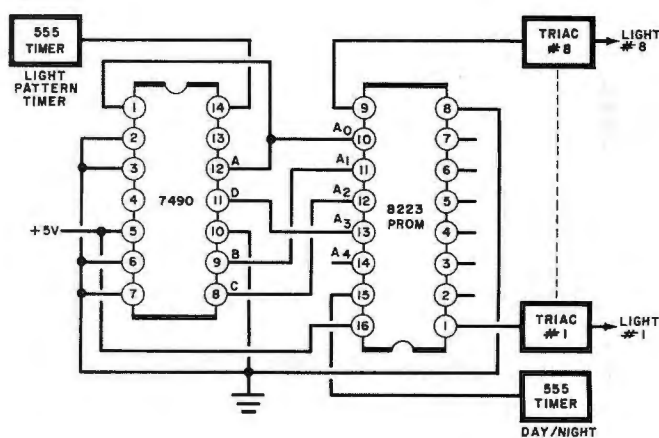


Fig. C. Clocked by timer circuit, 7490 counter delivers a 4-bit input to PROM, which controls triacs to turn lights on and off.

not have voltage across their coils continuously. With the PROM remembering the various track positions for the eight switches, you need only select the pattern you wish and push a button to initiate the selection of that pattern.

Intruder Deterrent. When you go away from home for a day or longer, you probably use mechanical timers to turn on and off house lights to make it appear that someone is home. A PROM can be used for this purpose and is much more effective in deterring intruders than are mechanical timers.

Shown in Fig. C is a system, built around a PROM, for turning on and off house lights in a certain sequence. Suppose that there are eight lights located throughout the house. The lights can be controlled by individual triacs, with the triacs controlled by the outputs from the PROM.

Assume that 10 light patterns are to be used in the evening hours. Word one can be a basement and a living room lights-on command, word two can be a living room and a kitchen lights-on command, and so on.

The various patterns of lights (words) can be selected by changing the address inputs, which are connected to a 7490 decade counter. A 555 timer can be used to change the outputs, of which there are a possible 10, of the 7490. This, in turn, changes the lighting sequence for the house. With this arrangement, various lights in the house can be changed every so often to give the appearance that someone is home and moving from room to room.

One type of erasable PROM, the 2048-bit MM5203, is made by National Semiconductor Corp. It can be erased by concentrated shortwave ultraviolet light. (It is available, surplus, for about \$24.) The MM5203 is housed in a 16-pin dual in-line package (DIP) with a quartz top that is transparent to shortwave UV light. The 2048 bits are organized as either 256 words of eight bits per word or 512 words of four bits per word.

The advantage of the erasable PROM, as opposed to the nonerasable PROM, is that it can be used over and over again for different programs. The unwanted information is simply erased by directing UV light through the IC's quartz "window" and reprogramming as desired.

Another type of erasable PROM

PREPARING A PROGRAMMING AND ADDRESSING TRUTH TABLE FOR PROM'S

Because the PROM is a logic element, programming and addressing it must conform to the rules of logic. To do this, a truth table must be drawn up for the programming procedure. This same truth table is also used for addressing the ROM after programming has taken place so that stored information can be retrieved.

There are two approaches you can use when working up your truth table. The first is an arbitrary table, used mainly for demonstration purposes. Since you would key in the address codes by manually setting switches, you can use any address system that suits your fancy. The truth table accompanying the diagram in Fig. A is an example of the arbitrary approach.

For more practical applications, address code selection would be under the control of the digital system in which the PROM is to be used. In this case, the programming truth table for both input and output codes must conform to those required by the system. A typical example is a BCD-to-7-segment decoder.

Let us assume a 7490 decade counter's encoded output is to be used to drive a seven-segment LED display. All decoding can be accomplished with a PROM. The PROM will then feed inverter/buffer transistors, which in turn will power the display's segments. The truth table, with the 7490's DCBA output lines feeding the 8223's A_7, A_6, A_5, A_4 , address lines respectively, would be:

$A_4, A_3, A_2, A_1, A_0, B_7, B_6, B_5, B_4, B_3, B_2, B_1, B_0$

NO.	D	C	B	A	g	f	e	d	c	b	a
0	X	0	0	0	X	0	1	1	1	1	1
1	X	0	0	0	1	X	0	0	0	0	1
2	X	0	0	1	0	X	1	0	1	1	0
3	X	0	0	1	1	X	1	0	0	1	1
4	X	0	1	0	0	X	1	1	0	0	1
5	X	0	1	0	1	X	1	1	0	1	0
6	X	0	1	1	0	X	1	1	1	1	0
7	X	0	1	1	1	X	0	0	0	0	1
8	X	1	0	0	0	X	1	1	1	1	1
9	X	1	0	0	1	X	1	1	0	1	1

The DCBA in the heading represents the outputs from the 7490, while the gfedcba represents the display segments controlled. The X's are don't-care states, since there is no input to the A_4 input nor output termination for the B_7 output lines of the 8223 PROM.

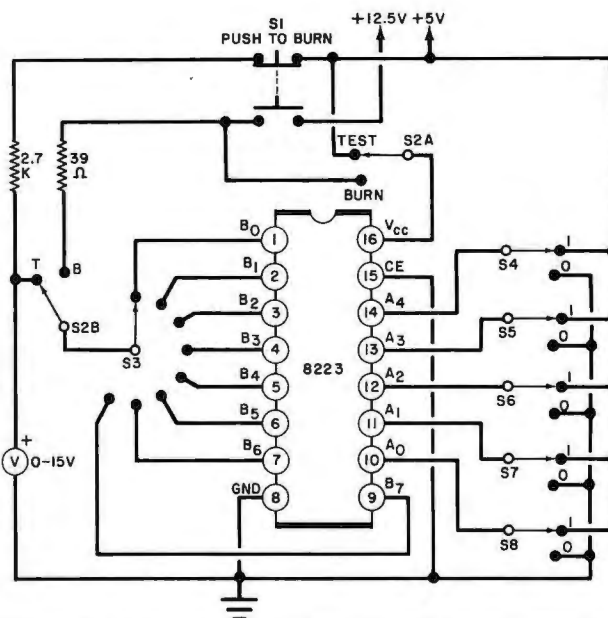


Fig. 2. In this programming setup, both power supplies must be regulated. Once PROM is programmed, its memory can be checked as described in the text.

—this one not so readily available to experimenters—is the Nitron Company's NC7010 EAROM. This device can be erased electrically in one second. It can be erased and reprogrammed up to a million times. The NC7010 is organized as 512 words of two bits per word.

How to Program a PROM. The 8223 PROM used in the applications described is shipped with all of its outputs at a logic-0 level. This means that all of its on-chip fuses are intact. If a logic 1 is to be written into the PROM's memory, the fuses must be blown. The procedure for blowing selected fuses is called programming. It can be performed with the circuit shown in Fig. 2. The +5- and +12.5-volt power supplies must be regulated. Switch S1 is a two-circuit push-button switch, with one set of contacts normally open and the second set normally closed. Switch S2 is a dpdt slide or toggle switch, while switch S3 must be a non-shorting rotary switch with eight or more positions.

After wiring together the Fig. 2 circuit, program the PROM as follows:

1. Set S2 to the BURN position. (Note: Never operate S1 when S2 is set to BURN.)

2. Feed the proper logic-1 (+5-V) and logic-0 (0-V or ground) code for word one onto address lines A_4 through A_7 via S4 through S8.

3. Set S3 to the first PROM output line position in which a fuse is to be blown according to your programming truth table.

4. Depress S1 for about a half second and release. This action, in blowing the fuse, develops considerable localized on-chip heat; so, **do not depress S1 for longer than a full second.**

5. Allow several seconds of cooling down time for the chip.

6. Set S3 to the next output line in which a fuse is to be blown.

7. Repeat steps 4 and 5 for each output line in which a fuse is to be blown.

8. Set S4 through S8 for the logic required for word two.

9. Repeat steps 3 through 7.

10. Continue to address the PROM for each succeeding word, repeating steps 3 through 7 as you proceed from word to word, until you have completed programming the PROM.

The schematic diagram shown in Fig. 2 depicts a program and test circuit. As you finish steps 3 through 7 for each word, set S2 to TEST (do not change the address code yet) and, observing the meter, check the PROM's outputs by cycling through S3's positions. Logic 0 will be indicated by the pointer swinging to near the scale's zero index, while logic 1 will be indicated by about a +5-volt reading. Once you have verified that the program has "taken" for a given word, set up the circuit for programming into the PROM's memory the next word that you want.

After making sure that the PROM is properly programmed, affix some identifying code on its case and truth table and file away the latter in a safe place where it will not get lost. ♦

HOME EMERGENCY LIGHT for "BLACKOUTS"

- Automatic "on" when ac power fails
- Full-wave battery-charging circuit
- Doubles as lantern flashlight
- Compact, neat design



BY WILLIAM OLDACRE

WHEN a power blackout occurs, one is likely to get caught in the dark without ready access to a flashlight or candle. Here is a hand emergency light to solve the problem, minimizing possible injury and fear due to darkness.

This emergency light goes on automatically whenever ac power is interrupted for one second or more, providing several hours of light before a recharge is needed. (The 1-second delay is built in to prevent flickering.) In addition, the system includes a battery charger which maintains full charge on ordinary nickel-cadmium batteries. It can also double as a portable flashlight and is designed into a neat, small package.

This home safety device is simple to build, requiring easy-to-get parts and modification of an inexpensive lantern-type flashlight.

How It Works. The schematic of the emergency light is shown in Fig. 1.

Transformer *T1*, *RECT1* (a full-wave bridge rectifier), and filter capacitor *C1* form a low-voltage dc power supply. When line voltage is applied to the circuit, *LED1* glows. Current through *LED1* is limited by *R1*. The power supply provides charging current for battery *B1*, two NiCd cells. Diode *D1* prevents the battery from discharging back through the LED. Charging current is limited by either *R3* or *R4*. When switch *S1* is in the SLOW position, *R3* allows 33 mA to flow into the battery. When *S1* is placed in the FAST position, *R4* provides 100 mA, which charges *B1* more quickly.

The dc voltage also energizes relay *K1*. Since the relay coil is energized under normal (line voltage-on) conditions, it might tend to get very warm. To keep the coil cool, resistor *R2* is placed in series with it, lowering the amount of continuous current flow. The path between the battery and the light bulb (*I1*) is controlled by the relay contacts. Under line-on conditions, no

current can flow through the bulb.

When the line power drops out, however, the relay coil is de-energized, and the contacts complete the circuit between the battery and the light bulb. The bulb automatically lights up, providing emergency illumination. To prevent the emergency light from flashing on and off whenever the line voltage drops for a fraction of a second (for example, when your refrigerator compressor kicks in), we take advantage of the fact that it takes about one second for the voltage across *C1* to decay to the point where the relay drops out. The exponential properties of the RC circuit smooth out any instantaneous variation in line voltage.

The flashlight is a self-contained unit which connects to the power supply through a three-conductor power plug-jack combination. When independent flashlight operation is desired, switch *S2* takes over the relay's switching operations by pro-

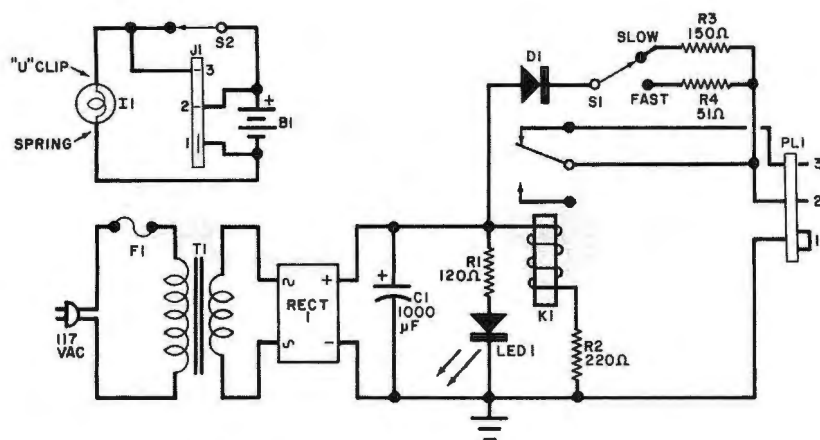


Fig. 1. Schematic of the emergency light. Power failure causes K1 to drop out, supplying power to I1.

PARTS LIST

B1—Two General Electric GC-3 1.25-volt, 1.2 A-hour nickel-cadmium batteries
 C1—1000-µF, 16-volt upright electrolytic capacitor (Radio Shack 273-958 or equivalent)
 D1—1-A, 50-PIV silicon rectifier (Cinch-Jones P303AB or equivalent)
 F1—¼-A fuse (Buss AGC ¼ or equivalent)
 J1—Three-conductor power jack (Cinch-Jones S303AB or equivalent)
 K1—6-volt SPDT relay (Radio Shack 275-004 or equivalent)
 LED1—Light emitting diode (Sprague ED-123 or equivalent)
 PL1—Three-conductor power plug (Cinch-Jones P303AB or equivalent)
 R1—120-ohm, 1-watt resistor
 R2—220-ohm, ½-watt resistor
 R3—150-ohm, ½-watt resistor
 R4—51-ohm, 2-watt resistor
 RECT1—2-amp, 50-PIV bridge rectifier (Radio Shack 276-1151 or equivalent)
 S1—SPDT miniature toggle switch

S2—SPST pushbutton switch (furnished with lantern)
 T1—6.3-volt, 300-mA filament transformer (Radio Shack 273-1384 or equivalent)
 Misc.—Chassis box (4" x 2½" x 6" (Radio Shack 27-252 or equiv.), lantern (Sears 4841, Ray-O-Vac L295 or equiv.), fuse clips (Buss 5682-41 or equiv.), metal battery holder (Radio Shack 270-1439 or equiv.), piece of 1" wood 4" sq., ¾" x ½" aluminum angle stock, ¼"-inch metal spacers, printed circuit or perforated board, line cord, rubber grommets, battery holder, wood screws, machine hardware, brass shim stock, adhesive-backed decorative vinyl, dry-transfer lettering, hookup wire, solder, etc.
 Note—A pre-drilled, etched epoxy printed circuit board is available for \$3.75 postpaid from William Oldacre, Box 12951, University Station, Gainesville, FL 32601.

viding an alternate path for current flow from the battery to light bulb I1.

Construction. The emergency light is composed of two units: a portable flashlight and the base/recharger which it plugs into.

Components forming the recharger circuit should be mounted on a printed circuit or perforated board. Etching and drilling and component placement guides for pc board fabrication are shown in Fig. 2. Mount the components on the board, paying close attention to the polarities of C1, D1, the leads to LED1, and RECT. (Align the rectifier so that the dot on the top of the case faces north. The pin facing north is the +dc output. South is negative, east and west are the ac inputs from the secondary.) Fuse F1 can be mounted either on the back panel using a panel-mount holder, or on the circuit board using standard fuse clips. The clips require 4-40 mounting hardware. The two 4-inch

(10-cm) leads should be connected from LED1 to the appropriate pads on the circuit board. Three 4-inch (10-cm) leads should be run from the board for S1, and three 10-inch (25.4-cm) leads for PL1. Drill holes in the utility box for pc board standoffs, rubber feet, LED1, S1, and the line cord. Insert the line cord through its hole using a grommet or strain relief and connect its leads to the transformer primary. Then mount the circuit board in the utility box using ¾-inch (0.64-cm) metal spacers.

The prototype uses Cinch-Jones three-conductor power connectors, but substitutions are OK. Drill two mounting holes in the wood block and a hole for PL1's leads through the cover of the utility box. Install a grommet in the hole for the leads.

Plug PL1 is mounted on a 3½" x 3½" x ¾" (8.9 x 8.9 x 1.9 cm) block of wood, which is covered with walnut grained adhesive-backed vinyl. Drill holes on the bottom side for mounting hardware (make sure these don't go all the way through), PL1, and the top two metal guide rails (completely through the block). These rails should be fashioned from ¾" x ⅛" (1.9 x 0.32 cm) aluminum angle stock. Round the corners of the aluminum, and drill two holes for securing hardware. Position

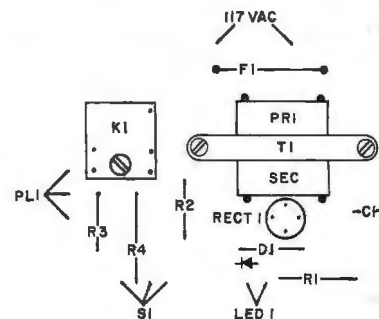
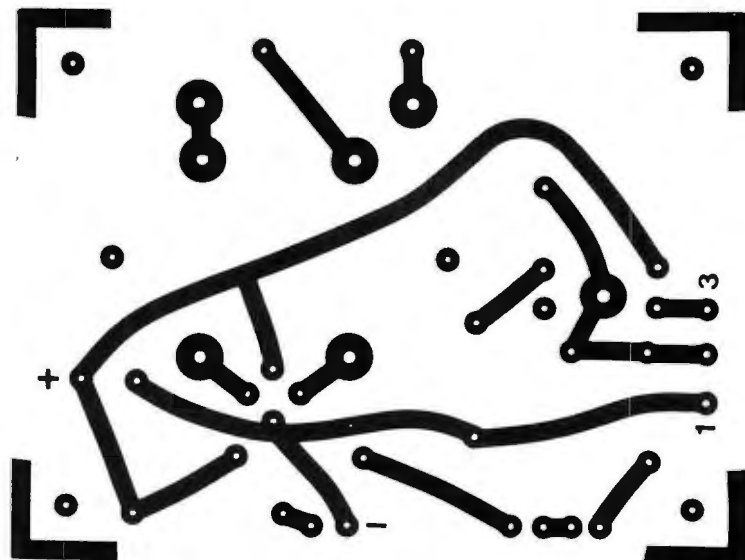


Fig. 2. Etching and drilling guide for pc board is below; component placement at right.



the rails so that they accept the flashlight you choose to use (the one in the photo is a Sears model), and then drill holes into the top of the wood block to match those in the guide rails. Give the rails a brushed appearance by rubbing them lengthwise with fine steel wool under running water. Then attach the rails to the block with $\frac{1}{2}$ " (1.25 cm) roundhead wood screws.

Secure plug PL1 to the wood block and attach the appropriate leads from the circuit board. Mount the block on the top of the utility box's cover, lining up the holes you previously drilled. Secure the block to the cover with roundhead wood screws.

Final assembly of the base/recharger may now be accomplished. First, label the front panel as shown in the photo using dry-transfer letters. Then apply several light coats of clear acrylic spray. This will prevent the letters from being worn off. After the spray has dried, secure S1 in its mounting hole. If your LED1 has no mounting collar, use a $\frac{1}{4}$ -inch (0.64-cm) O.D. rubber grommet to

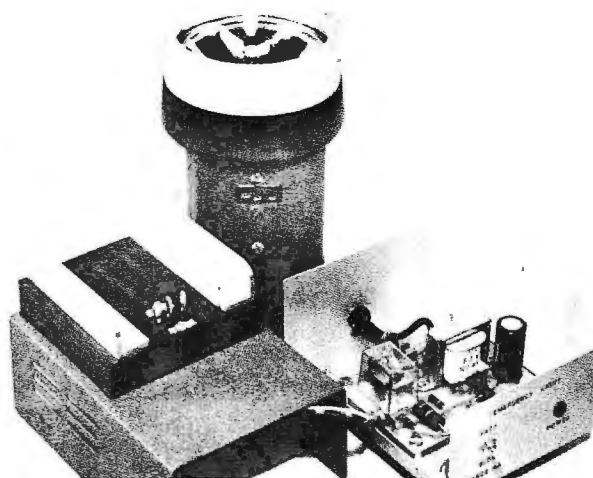
SELECTING AN INCANDESCENT BULB.

The battery power source used in the emergency light holds a power capacity of 1.2 ampere-hours at 2.5 volts (when fully charged). This means that it can keep a 1.2-A current flowing for one hour. Alternatively, it can sustain a 0.6-A current for two hours, 0.3-A for four hours, and so forth. Obviously, the smaller the current drain from the power source, the longer the flow can continue. You will have to decide for yourself how long you will need the light to function before the NiCd cells are completely discharged.

If you live in an area plagued with frequent (but brief) power blackouts, this discharge time is not too important. Alternatively, if your neighborhood gets rare (but prolonged) power losses, duration of the power source should be extended.

These factors will dictate your choice of lantern light bulb. The type PR-2 light bulb, which draws 0.5 A at 2.4 volts, will discharge the battery source in about 2 hours and a quarter. If you choose a PR-4 bulb instead, the NiCd cells will last about 45% longer, since it draws only 0.27 A at 2.3 volts. Although the PR-4 will produce less light than the PR-2, many builders will prefer it because it is easier on the supply. If even longer duration (and a lower light level) are desired, you can choose a less demanding bulb type or add current-limiting resistors in series with the bulb.

Fig. 3. Base with recharger is shown without cover. Flashlight plugs into socket on wooden block.



keep the LED secure. Slip the cover onto the utility box and secure it with the hardware provided for this purpose. This completes the assembly of the base/recharger.

It is necessary to modify the hand lantern that you choose. Disassemble the lantern, and find the "molding line" running down the middle of the housing. This can be used to accurately center the power jack J1. Cut a hole in the bottom of the housing that conforms to the power jack you will install. Use a very sharp safety knife to cut the plastic. Drill holes for the mounting screws for the jack and for a metal battery holder. Rather than soldering inside the lantern housing, prewire the components outside the housing as shown in Fig. 4. Replace the light bulb with a lower voltage unit (see accompanying box).

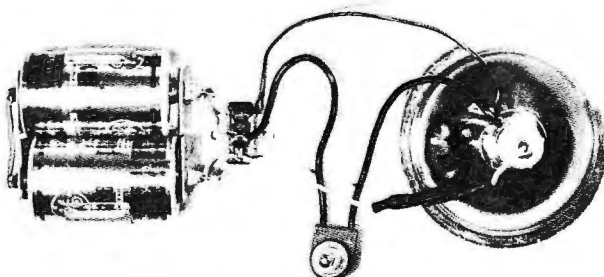
Do not solder the light bulb lead to the brass rivet on the back of the bulb's nylon retainer nut. Instead, remove the compression spring and solder the lead to one loop of spring. Then replace the spring and feed the wire through the hole in the rivet. To make bulb replacement more convenient, install a small in-line connector in the lead between the spring and terminal of jack J1. A U-shaped clip which fits around the barrel of the lamp socket is furnished with the lantern. Solder two leads to the clip, one of which is connected to terminal

3 of J1. Connect the other to S2 as shown in the schematic. Note that S2 is the lamp's original ON/OFF switch. Fasten the U-shaped clip to the lamp socket base. Complete the wiring of J1 and S2, and then install two 1.25-volt NiCd batteries in the metal holder. Reassemble the lantern.

Testing. Make one final check of all wiring before applying power to the unit. Then, setting the lantern aside, plug the line cord into a wall socket. A distinct click should be heard as the relay is energized, and LED1 should glow. If all is well, plug the lantern into the base/recharger. If J1 lights up, switch it off with S2. (If this doesn't turn J1 off, disconnect the line cord and recheck all wiring.) Allow the batteries to charge for about ten minutes with S1 in the FAST position. Then simulate a power failure by disconnecting the line cord. The lantern should light up after a one-second delay. If the lantern checks out OK, plug the line cord back into the wall socket, and allow the batteries to charge for at least 16 hours.

Operation. The lantern should be placed where fail-safe illumination is most needed. After the initial charge (with S1 in the FAST position), use the SLOW charge rate, as this will offer extended battery life and slightly lower consumption. ♦

Fig. 4. Modifying flashlight is best done by working outside the flashlight housing.



DURING the summer months, when power demands peak, brownouts are an all too common occurrence. As power companies cut back on the amount of voltage delivered to the ac outlets in your home, the picture on your TV receiver is likely to shrink and lose color, your lights might dim slightly, and some of your appliances may have difficulty operating on the unaccustomed low voltage. Some electrically operated appliances can even be irreparably damaged if they are operated on too low a voltage.

Most people just grit their teeth and try to bear with the inconveniences of the brownout situation. This is one way to approach the problem, but a more practical approach would be to use a device that will restore the line voltage level to normal. This is exactly what the Power Guard is designed to do. It is completely automatic. As the

line voltage begins to fall below a predetermined level, the Power Guard compensates for the reduction by boosting the voltage available at its output. Then, when the power company restores normal service, the Power Guard switches itself out of the line, to remain ready to go into action again when the next brownout occurs.

About the Circuit. A voltage-sensing circuit that operates a relay, causing it to switch a transformer in and out of the ac line is the heart of the Power Guard (see Fig. 1). The sensing circuit is made up of the voltage divider formed by *R1* and *R2*, neon lamp *I1*, and silicon controlled rectifier *SCR1*.

When switch *S1* is set to ON, line voltage is applied across the *R1/R2* divider network. Assuming that this potential is greater than 105 volts ac, *I1* will fire. This, in turn, indicates that the power available at the wall outlet is at a "normal" level. By adjusting *R2*, the line potential at which *I1* is triggered can be varied.

When *I1* comes on, it applies current to the gate of *SCR1*, triggering the silicon controlled rectifier into conduction and energizing relay *K1*. When this happens, the relay's lower set of contacts places output receptacle *SO1* directly across the ac line.

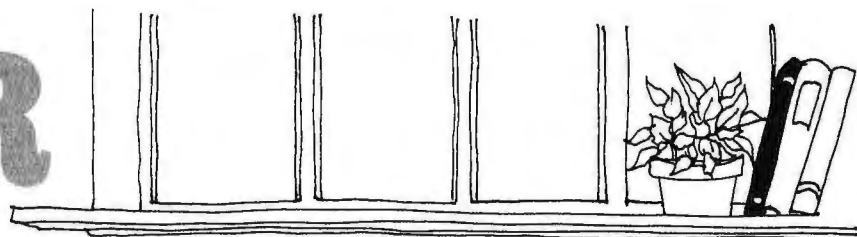
Capacitor *C1* across the solenoid of *K1* eliminates the possibility of relay chatter that would normally be caused by the rectified voltage coming through *SCR1*.

When a brownout occurs and the line voltages drops below the value predetermined by the setting of *R2*, *I1* extinguishes and removes gate current from *SCR1*. This causes the SCR to cut off on the next zero crossing of the line voltage and deenergizes *K1*. This, in turn, switches the secondary of *T1* into the circuit, which is designed to add the primary and secondary voltages. This "boosted" voltage is then delivered to *SO1*. The magnitude of the voltage boost depends on the secondary voltage of *T1* at the reduced line voltage. The point at which the boost comes into play depends on the setting of *R2*. (Note also that, when the boost circuit is operating, *I2* comes on to provide a visual indication that line voltage is down.)

Tracking, the opening and closing of the relay's contacts caused by minor changes in line voltage, is eliminated by *I1*. The reason for this is that the neon lamp's firing voltage is higher than that required to maintain it in the ionized state. So, while the lamp requires about 110 volts to fire, it will not extinguish until the line voltage drops to 105 volts.

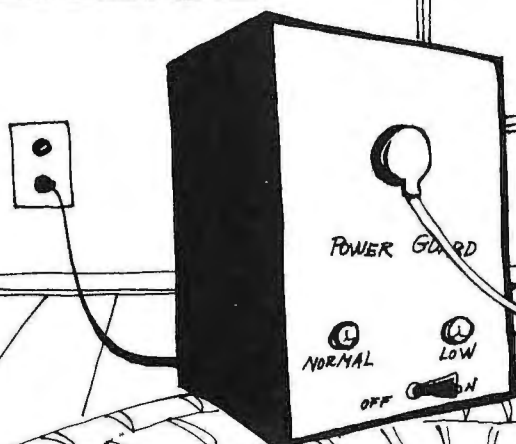
CONSTRUCTION

THE POWER GUARD



**Boosts voltage
and eliminates TV
picture shrinkage
during summer
brownouts**

BY JULES H. GILDER



Modar's Triton vhf unit sits in optional 12-V dc battery charger.



WHAT'S NEW IN **MARINE** **RADIOTELEPHONE**

FCC rules changes, license requirements, and equipment overview.

BY LEN BUCKWALTER

PLEASURE-BOAT owners are sailing through the greatest change-over ever to affect marine radio. Since 1972, when the FCC ordered a five-year exodus from the old band on 2-3 MHz, more than half of the quarter-million radio-equipped boats have switched to the new system. They're now on vhf FM, a band that lies from 156 to 162 MHz and promises to alleviate the communications glut that choked the old channels. With the final deadline less than two years away, vhf FM is having a growing impact on every aspect of the marine radiotelephone—from the tip of the antenna (it's now shorter) to the ground plate (it's missing). Anyone planning to buy a boat or operate a radio should know something about the new band's benefits—and limits.

One big boon is that interference on vhf mostly disappears. Because the old band's medium frequencies skipped through the ionosphere, voices from

well beyond the horizon could clobber local communications. Even the Coast Guard complained that a distress call could be lost in the gibberish of voices on the frequency. That kind of "QRM" is just about licked on vhf because transmission range is barely more than line-of-sight; two stations almost have to "see" each other to exchange signals. Another vhf advantage is less susceptibility to ignition interference from the boat's own engine. It's partly due to the higher frequency, where spark plug and generator noises don't have much effect. Also, the modulation mode in the new service is FM, not AM, where a receiver does a better job of slicing away amplitude-modulated ignition noise (which creates most of the problem). You won't have to labor through a tedious, tricky suppression procedure to quiet the boat's electrical system.

You won't have to pay a hefty installation fee, either, because most vhf FM

models come in a "do-it-yourself" package. On the older band, a technician with a commercial radiotelephone ticket had to come aboard, tune the radio into the antenna and log the start-up. In many cases he'd also have the boat hauled out of the water to be fitted with a ground plate—a copper sheet fastened to the hull to act as an electrical counterpoise for the antenna. That's all done away with in vhf because the higher operating frequency allows self-contained antennas that need no external ground. These factors enable the manufacturer to pretune each set at the factory into a 52-ohm load, and eliminate a second tune-up when the radio is installed aboard ship. In a typical vhf FM installation, you merely mount the antenna at the highest point, run 52-ohm coaxial cable from set to antenna, and hook a dc power cable to the hot and ground side of the boat's 12-volt electrical system.

The current crop of marine radios also boasts a wholesale change-over to solid-state circuitry. Here the advantages multiply. Equipment cabinets are so small and unitized they'll fit under the dash of a runabout or even aboard a rowboat if you provide external battery power. The minuscule current drain of the receiver lets you monitor the emergency and calling channel for hours without running the risk of a dead boat battery.

Disadvantages. Are there any disadvantages to the new breed of marine radios? A lingering objection by old timers has been that no-one was on the new band to hear their calls—especially a shout to the U.S. Coast Guard in time of distress. There was some merit to that complaint until about 1974, when conditions vastly improved. By that time, the Coast Guard filled gaps in its radio coverage of most boating areas after erecting lofty new antennas atop buildings, towers and mountains. Now, if you call for help in some regions, you might communicate through one of the Guard's skypiercing towers up to 100 miles away.

The scarcity of other boats to talk to has also undergone dramatic change. As the deadline looms closer, the number of boats getting on vhf FM is growing in a geometric spiral. It's estimated that more than 130,000 of the marine radio fleet—more than half the total—is now licensed for the new service. There'll be stubborn holdouts



Raytheon 1205 SSB transceiver is for blue-water sailors.

on 2 MHz right up to the deadline at the end of 1976; but, they'll talk to fewer and fewer stations. After the cut-off date, the old-style AM marine radio will be worth no more than ballast.

One limitation of vhf FM for some might be its just-to-the-horizon range. Under normal conditions of antenna height, boat-to-boat communications reach out 20 or 30 miles, or about double that distance when talking to a shore station with a high antenna. Although these moderate distances should serve the needs of almost any boat under 30 feet, they're not intended for the blue-water sailor. When cruising offshore or ocean-racing beyond sight of land, the bigger boat should be equipped with SSB, or single-sideband, which can span hundreds of miles over water. Since SSB is an electronically sophisticated system, it is more costly than the customary vhf FM transceiver. For the same amount of transmitter wattage, an SSB station puts out a signal about six times more powerful and two SSB stations, thanks to a reduction in bandwidth, can operate where one AM station existed before. If your brand of long-distance sailing demands SSB, the FCC insists that you *first* install a regular vhf FM set. With SSB gear starting at about \$700, the electronics represent more than \$1000.00—a significant part of a boat's total cost.

The price of a typical vhf FM set is more than what the old timers paid for lower-frequency radios on 2-3 MHz back at the beginning of the decade. Inflation aside, the higher tag is due to more stages in both receiver and transmitter of the vhf rig. The set also

has more elaborate filtering for good selectivity. A current \$400 vhf FM transceiver, though, is a far cry from the \$1000 versions introduced to the market about six years ago. Today's prices are also significantly offset by the do-it-yourself nature of the vhf FM installation. Another plus: the sets are so compact and light, it's practical to pack them up and return them through the mail for factory service if no local technician with the required FCC ticket and right facilities is available.

About Rules. No matter what you need in the way of two-way radio, be sure you know the FCC deadlines to avoid chucking good equipment overboard or buying someone's white elephant. Here's how the rule changes might affect you:

1. *An old-type marine radio that operates on 2-3 MHz.* If you now own a boat with such a set installed, it's legal to use it until the deadline, January 1, 1977. Although the Coast Guard will monitor the distress frequency (2182 kHz) until the bitter end, the radio then becomes obsolete and illegal to operate.

2. *In the market for a boat?* Be wary if the prospective boat already has an old-type marine radio installed. If you become the new owner, and want to license the old rig, the FCC will deny your application. So don't let an old radio sweeten the seller's deal—you must install vhf FM if you file a license. The same restriction, incidentally, applies if you buy a secondhand radio. You won't be able to license an AM radio for installation aboard your boat. Any new boat you buy can take only the new-type, or vhf, radio.

3. *You lost your old-type radio in a storm.* This is a minor exception; you can replace it with an old-type radio. It will probably have to be a second-hand model, though, because manufacturers long ago stopped making the old-style AM sets. In any case, all old-style radiotelephones should utter a final gasp at the outset of 1977, so you'll be mighty lonely on the 2-3 MHz band.

Let's take a closer look at a typical vhf FM radio for a small cabin cruiser, runabout, or sailboat. Its price tag runs about \$350-\$450 for a model of 12-channel *capability*. The set, however, is factory-fitted with crystals for only three to five channels. Additional channels can be added at a later time or, in some cases, the manufacturer

sells a plug-in channel module for a do-it-yourself frequency addition. Since the module is sealed and pre-tuned, no technician's license is required. When you purchase additional crystals for a conventional set, a licensed technician is required to make the tuning adjustments. With crystals priced at about \$15 per channel, you can see that the number of factory-installed channels has a significant impact on a radio's price tag and should be considered when making your selection.

How Many Channels? At least two marine channels are mandatory for every boat-owner. One is channel 16, the distress, safety, and calling frequency monitored continuously by the Coast Guard and by many other boats. That channel is also the "calling" frequency to raise other boats. Once communications are established, the stations must move to another channel to avoid jamming channel 16.

The second mandatory channel is 6, the ship-to-ship safety channel. With every craft fitted with this channel, you're always assured of communications with someone within hailing distance. Two other extremely popular channels are 26 and 28, both reserved for the marine operator (or "Public Correspondence"). By raising the marine operator, you can place a land-line call to any telephone or even another boat hundreds of miles



At top is Realistic's TRM-12 12-channel rig. Pearce-Simpson Catalina, above, has batteries.

beyond your communicating range. Once you have safety and telephone-company channels, other crystals may be added to cover frequencies assigned to local marinas, yacht clubs, and other local organizations. A weekend boatman should be able to satisfy his communications needs with approximately six to nine channels. Only far-ranging vessels require, say, 20 channels (out of a possible 38) in a set that costs upwards of \$1000.

Almost any vhf set will have one crystal in the receiver section for picking up continuous marine weather from a network of National Weather Service stations strung along every major waterway of the U.S. In most cases, the frequency is 162.55 MHz, but check your local area for possible exceptions on 162.40 MHz. A good source of local frequency information is a nearby marine dealer. If you want to follow the FCC's basic suggestions on channels, see the accompanying table.

Besides the total number of channels, transmitter power also influences the price of a marine radio. Many sets offer a maximum of 25 watts, the legal limit, but there are lower-cost units of 10 watts, or even

less. Power won't make much difference in range unless something is operating at less than highest efficiency in your transmitting system, or the distant station has a poor receiver of low sensitivity. Any set you buy has a transmitter power switch with two positions; the first delivers full r-f power, while the other position reduces r-f output to one watt. This minimizes interference to other radios while you're talking to a nearby boat.

The range of marine communications depends heavily on the antenna. With vhf's straight-line propagation, a higher antenna position on the boat improves the signal's ability to look farther over the horizon. Most popular design is the fiberglass whip with its excellent immunity to the weather. The fittings are plated with chrome or other stainless metal. As mentioned earlier, these antennas need neither tuning nor ground plates. A quarter wave on 2.5 MHz, for example, is almost 100 feet long, which means a vertical whip on the old band is electrically lengthened by tuning at the transmitter. At 156 MHz, on the other hand, a quarter wavelength is only 1.5 feet so antenna elements can be physically resonant to the signal without

external tuning. In actual practice, however, vhf marine antennas are somewhat longer than 1.5 feet to improve signal strength by compressing the radiation pattern to lower angles (where the distant boats lie). Typical marine antennas run about 4 to 9 feet long and come with 52-ohm coaxial cable that can be cut to any length. A solderless connector is often supplied so you can route the cable between antenna and transmitter and easily trim it to size.

Licenses. Licensing a marine radio is easier than ever. No professional help is required to obtain, fill out, and file the forms. You'll need two applications—one for an operator's license, the other to license the station—and both are secured from the FCC's nearest field office. (Look under "U.S. Government" in the phone book if you don't know where it is.) By phone or mail, ask for FCC form 502 for the station license and FCC Form 753-A for the radiotelephone operator's permit. These papers include helpful instructions, but here's what you can generally expect:

Restricted Radiotelephone Permit. This is the operator's license, good for life, at a one-time fee of \$8. There are no technical questions to answer and the form is mostly a declaration that you're not an alien.

Station License. This one is issued for a five-year period and costs \$20 initially, and each time the license is renewed. Since it takes three to six weeks to receive a shipboard license, a local FCC office can issue you an interim 6-month permit on the spot for a \$5 fee. You can get on the air right away and you'll receive the identical call letters when the regular station license arrives.

According to Lou Arnone, an official in the marine division of the FCC's Washington office, the greatest problem with licensing today is when the radio-owner fails to notify the Commission of a change of address: Far from a minor matter; it ultimately causes FCC computers to do battle with undelivered renewal forms, send registered letters and, finally, begin a legal proceeding that could revoke a ship's license. It costs nothing, he points out with a bit of irony, to have the address changed. And sailing without a marine radio could prove much more inconvenient when you're slowly drifting out of gas toward someplace like Tahiti.

Channel Designators	Type of Communications	Recreational Vessel Channel Capability					
		4	6	8	12	16	24
16 (Mandatory)	Distress, Safety & Calling (Intership & ship-to-shore)	*(Number of recommended channels each group)					
		1	1	1	1	1	1
06 (Mandatory)	Intership Safety (Intership)	1	1	1	1	1	1
65, 66, 12, 73, 14, 74, 20	Port Operations (Intership & ship-to-shore)		1	1	2	3	7
13	Navigational (Intership & ship-to-shore)				1	1	1
15 & 162.550 MHz	Environmental (Ship receive only)			1	1	2	2
17	State Control (Ship-to-shore)				1	1	1
07, 09, 10, 11, 18, 19, 79, 80	Commercial (Intership & ship-to-shore)						
67, 77, 88, 08	Commercial (Intership)						
68	Non-Commercial (Intership & ship-to-shore)	1	1	1	1	1	1
09, 69, 71, 78	Non-Commercial (Ship-to-shore)		1	1	1	1	3
70, 72	Non-Commercial (Intership)				1	2	2
24, 25, 84, 85, 26, 27, 86, 87, 28	Public Correspondence (Ship-to-shore)	1	1	2	2	3	5



BUILD A

SEMICONDUCTOR LASER COMMUNICATIONS SYSTEM

State-of-the art communicator

uses pulse modulation to achieve a

possible range greater than 3000 feet.

BY FORREST M. MIMS

COMMUNICATING on a light beam is fairly common with light-emitting diodes ("Experimenting With Light-Beam Communications," POPULAR ELECTRONICS, April 1975, p. 40), but for longer distances and greater efficiency, a laser light source is recommended. With the system described here, it is possible to get a range of more than one kilometer (3300 ft). Since it uses a PIN photodiode in the receiver, the system can be operated in daylight or darkness without an expensive infrared filter.

Though most light-beam communicators use amplitude or intensity modulation, this system employs pulse-frequency or pulse-rate modulation (PFM or PRM). This type of modulation is almost immune to transient atmospheric effects and noise from interfering light sources. Also, the output signal from the PFM receiver is constant in amplitude over the entire communicating range, while that from an AM system becomes progressively weaker as range is increased.

Transmitter. As shown in Fig. 1, a modular amplifier (AMP1) boosts the voice signals from a dynamic microphone. In a pulse-frequency modulator (Q1 and Q2), Q2 is a UJT connected in a relaxation-oscillator mode. With no input from AMP1, Q1 is saturated (with very low emitter-to-collector resistance) and Q2 oscillates at a frequency determined by the time constant of C2 and R6. When an input is present on the base of Q1, the frequency of Q2 is varied in direct proportion to the amplitude of the modula-

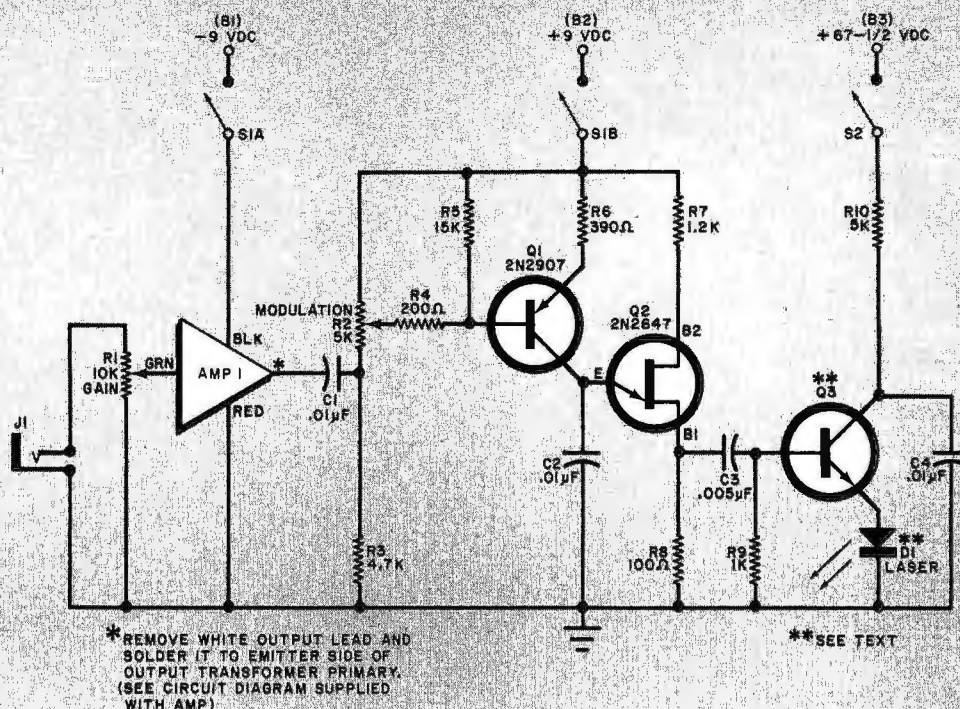


Fig. 1. A commercial modular audio amplifier modulates a UJT oscillator to drive the laser.

PARTS LIST (TRANSMITTER)

AMP1—Modular audio amplifier (Radio Shack 277-1240 or similar)
 B1, B2—9-V transistor radio battery
 B3—67½-V battery (Everready 457 or similar)
 C1, C2—0.01-μF capacitor
 C3—0.005-μF capacitor
 C4—0.01-μF, 100-V capacitor (disc or paper only)
 D1—Laser diode (see table at right)
 J1—Microphone jack
 Q1—2N2907 transistor
 Q2—2N2647 UJT
 Q3—Selected npn switching transistor (see text)
 R1—10,000-ohm potentiometer

R2—5000-ohm potentiometer
 R3—4700-ohm, ¼-W resistor
 R4—200-ohm, ¼-W resistor
 R5—15,000-ohm, ¼-W resistor
 R6—390-ohm, ¼-W resistor
 R7—1200-ohm, ¼-W resistor
 R8—100-ohm, ¼-W resistor
 R9—1000-ohm, ¼-W resistor
 R10—5000-ohm, ½-W resistor
 S1—Dpdt toggle switch
 S2—Spdt toggle switch
 Misc.—LMB B-H 643 enclosure, lens, battery retainers and clips, brass tubing, telescope, mounting hardware, 200-ohm dynamic microphone, epoxy, pc board, solder, etc.

SUITABLE LASERS

	RCA SG2001	RCA SG2002	RCA C30025	LDL LD22
Power output (W)*	1	2	0.5	6
Threshold current (A)	4	4	1.5	8
Peak current (A)	10	10	5	25

*Typical power output at peak forward current.
 Note: The prototype laser has been successfully operated with all three of the RCA lasers listed above.

Addresses: The manufacturers will provide current prices and specifications upon request. Write to: RCA, Electronic Components, Box 1140, New Holland Pike, Lancaster, PA 17604; Laser Diode Laboratories (LDL), 205 Forrest St., Metuchen, NJ 08840.

tion frequency. The center frequency is determined by the setting of R2.

The resulting PFM signal across R8 triggers a laser drive circuit comprised of relaxation oscillator C4, Q3, R10, and D1. Transistor Q3 is an npn switching transistor operated in a nonconventional avalanche mode. A charge is placed on C4 through R10 until the breakdown voltage of Q3 is reached. The capacitor then discharges through Q3 and the laser. The pulse is very fast (50 ns) and high in current (5 to 10 A) to fire the laser. The cycle then repeats. The large current surge does not mean that the battery has to supply 5 or 10 amperes. The surge comes from the charge stored on the capacitor.

Transistor Q3 oscillates independently of the modulator even when

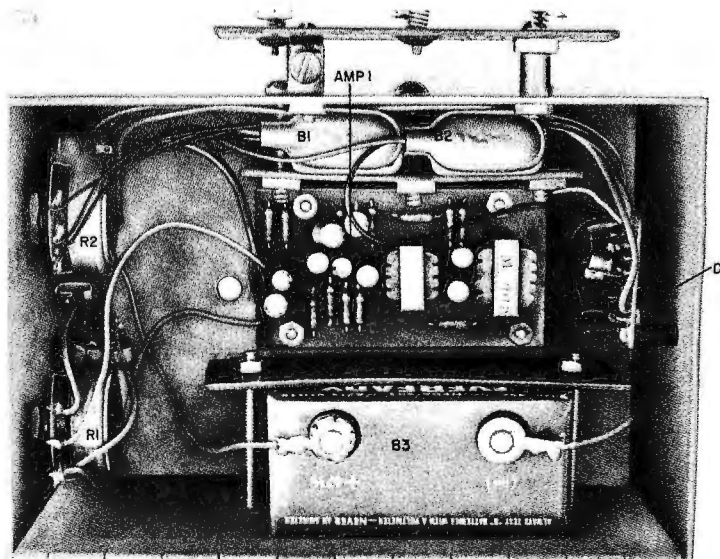


Photo shows layout of prototype transmitter. Mounting for boresighting telescope is at top.

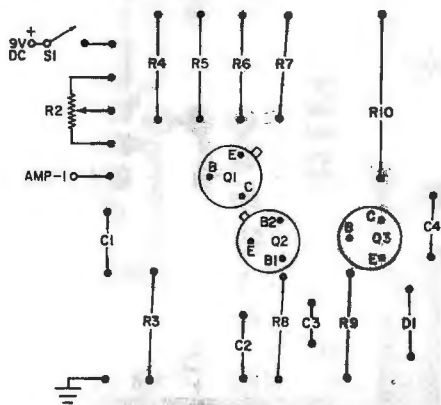


Fig. 2. Actual-size etching and drilling guide for transmitter is above, component layout at left.

the latter is in the relaxation mode. However, with an input, the oscillation varies with the signal. Potentiometer *R2* adjusts the carrier frequency to achieve the best modulation. A carrier of about 20 kHz gives the best results for the circuit used here. This is much higher than the 6 or 8 kHz required for acceptable voice transmission and insures good quality for both voice and music.

The transmitter is assembled on a printed circuit board as shown in Fig. 2. All components can be installed after the board is prepared, with the exception of *Q3* and the laser diode. Transistor *Q3* must be selected by using a test jig such as that shown in Fig. 3, which measures breakdown voltage. Ideally, a 15-MHz oscilloscope should be used to measure the current delivered by the transistor under test. This is done by measuring the pulse voltage across *R3* in the test circuit. Since this is a 1-ohm resistor, the voltage measured is equal to the current.

If a 15-MHz scope is not available, a lower-bandwidth scope, connected across *C1*, can be used to measure the transistor's breakdown voltage. The graph in Fig. 4 can be used to deter-

mine the peak current delivered by the transistor.

Not all transistors will oscillate in the test circuit. For best results, try common npn switching transistors such as 2N914, 2N2222, 2N3643, 2N4400, 2N5188, HEP50, etc. Select a transistor that gives a peak current between the laser's threshold and peak-allowable currents (as specified by the manufacturer). High currents give high output power. Install the transistor on the pc board and note its current for future reference.

Several lasers can be used, as listed in the table. Do not install the laser yet. Instead, connect an infrared LED (SSL-55C, TIL31, TIL27, etc.) in the circuit for preliminary testing. This permits you to get the circuit operating properly without the possibility of damaging the laser diode.

Receiver. In the receiver (Fig. 5), infrared radiation from the laser strikes PIN photodiode *D1* and generates a current which is amplified by *IC1*. Capacitive coupling between amplifier stages blocks dc signals from ambient sunlight and other light sources.

The output of *IC1* can be fed directly to an earphone for AM operation. For

PFM, however, a threshold discriminator is necessary. The monostable multivibrator composed of *Q1* and *Q2* forms the threshold circuit. When an amplified pulse from *IC1* exceeds the trigger threshold of the multivibrator (a few tenths of a volt), *Q2* delivers a pulse of constant width and amplitude. This can be picked up at the collector of *Q2*, but best results are obtained by adding an amplifier (*AMP1*) for loudspeaker operation.

The pc board for the receiver is shown in Fig. 6. Use care when installing the IC to avoid bridging the copper portions.

Receiver sensitivity can be improved somewhat by the addition of potentiometer *R7*, which can be adjusted to reduce the threshold of the multivibrator and permit detection of weak signals. (There is no provision for *R7* on the pc board. It can be added by removing a short section of foil from the negative line to *Q1* and *Q2* and soldering the potentiometer's leads across the gap.)

The photodiode used in the prototype was a high-quality EG & G device costing about \$15. This diode has a highly linear response and can be operated in broad daylight. Less expensive detectors (even ordinary silicon solar cells) can also be used; but light baffles, shields, or an infrared filter will be necessary for daylight operation.

Assembly. Check the pc boards for errors and then mount them in suitable enclosures. The enclosures noted in the parts lists were used in the prototype because the hinged lids permit rapid access to the batteries and pc boards.

Assemble the receiver first. Use a chassis punch or nibbling tool to cut a hole in one end of the cabinet for the lens. A 2" plastic lens was used in the prototype, but most any simple lens can be used as long as its focal length is 4 1/4" or less. The larger the lens, the better its light gathering power.

Use L brackets to mount the pc board in the enclosure with the photodiode at the exact center of the lens opening. For the lens given in the parts list, the diode should be exactly 4 1/4" from the inside cabinet wall in which the lens hole is cut.

Mount the threshold adjust pot (*R7*, if used), gain control (*R15*), and power switch (*S1*) on the end of the case opposite the lens opening. Use appropriate mounting hardware for the

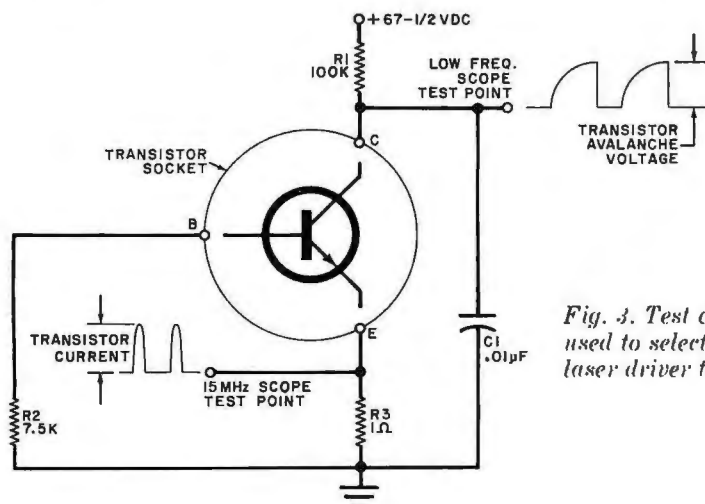


Fig. 3. Test circuit used to select laser driver transistor.

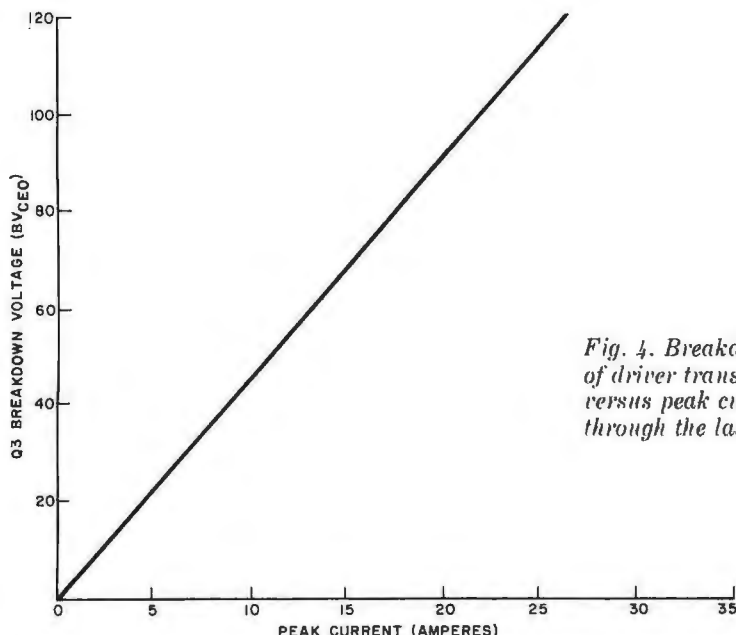


Fig. 4. Breakdown voltage of driver transistor versus peak current through the laser diode.

speaker, AMP1, and the two 9-volt batteries. Scraps of pc board 1" x 3" make good battery retainers. Use rubber grommets as standoffs for AMP1. Complete receiver assembly by wiring

the various components to one another. Then mount the lens using a flexible adhesive such as Dow Corning Silastic". The plastic lens mentioned in the parts list can be mounted

by bending its shoulders with a hot soldering iron.

There are two steps to the transmitter assembly. First, prepare appropriate mounting holes for the controls, hardware, and lens tube assembly. A 9/16" hole should be adequate for the lens tube. Then install all components and batteries except the laser pc board. Make the necessary connections to the board but don't mount it.

Install an infrared LED (note proper polarity) instead of the laser. Test the receiver by pointing it toward a line-powered incandescent lamp. If the receiver is properly aligned with respect to the lamp, a 120-Hz buzz should be heard from the speaker.

Now point the transmitter LED toward the receiver lens and turn on the power. Talk into the microphone or place it near a radio while adjusting R2. It should be possible to get good-quality audio from the receiver. If not, make sure the transmitter LED is properly aligned with respect to the receiver. Then try adjusting R7 in the

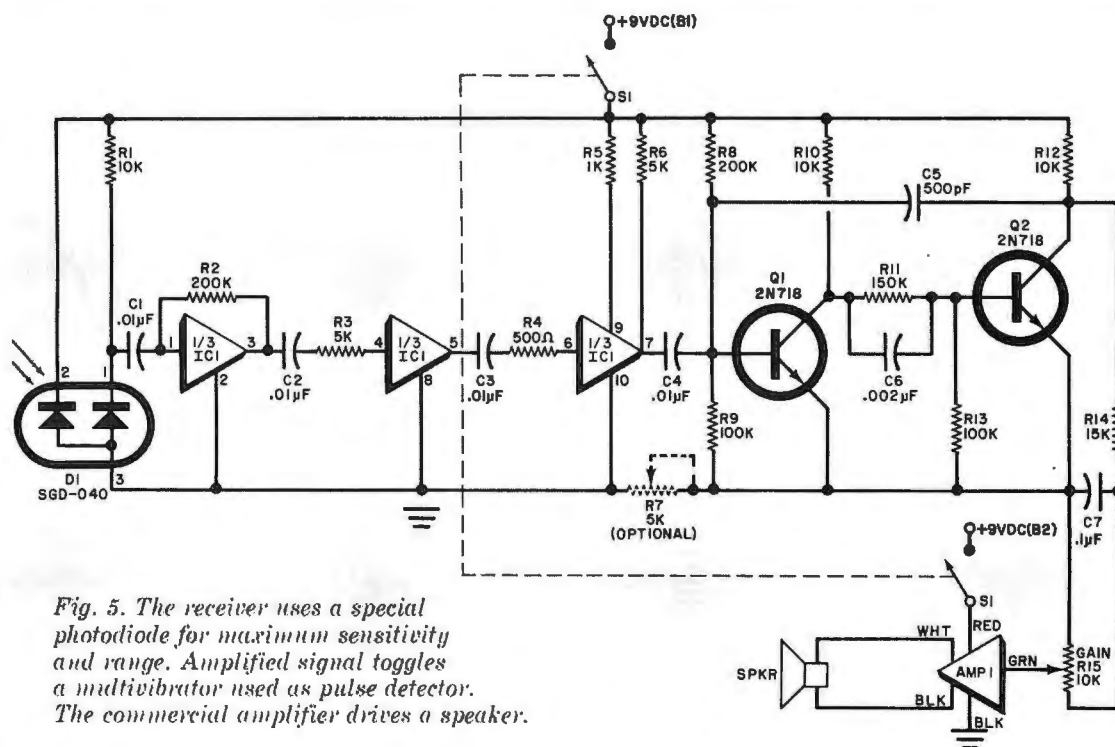


Fig. 5. The receiver uses a special photodiode for maximum sensitivity and range. Amplified signal toggles a multivibrator used as pulse detector. The commercial amplifier drives a speaker.

PARTS LIST (RECEIVER)

AMP1—Modular audio amplifier (Radio Shack 277-1240 or similar)
 B1, B2—9-V transistor radio battery
 C1 to C4—0.01- μ F capacitor
 C5—500-pF capacitor
 C6—0.002- μ F capacitor
 C7—0.1- μ F capacitor
 D1—SGD-040B PIN photodiode (EG&G; available from Cramer Electronics, 85 Wells Ave., Newton, MA

02159, for \$15 plus postage; see text)
 IC1—CA3035 amplifier array (RCA)
 Q1, Q2—2N718 npn switching transistor (or equivalent)
 R1, R10, R12—10,000-ohm, 1/4-W resistor
 R2, R8—200,000-ohm, 1/4-W resistor
 R5—1000-ohm, 1/4-W resistor
 R3, R6—5000-ohm, 1/4-W resistor
 R4—500-ohm, 1/4-W resistor
 R7—5000-ohm potentiometer (optional, see text)

R9, R13—100,000-ohm, 1/4-W resistor
 R11—150,000-ohm, 1/4-W resistor
 R14—15,000-ohm, 1/4-W resistor
 R15—10,000-ohm potentiometer
 S1—Dpst toggle switch
 Spkr—8-ohm miniature speaker
 Misc.—LMB B-H 643 enclosure, lens, battery retainers and clips, mounting hardware, cement, solder, pc board, etc.

receiver. If no signal is heard, check the transmitter wiring. Also, the LED may be bad, Q3 may not be oscillating, or one or more of the batteries may be weak.

Proper operation of the system is obvious since a slight misalignment of the transmitter with respect to the receiver will cause loud noise and oscillation from the receiver and then silence. This illustrates the PFM mode of operation. Unlike simple AM systems, a PFM light-beam communicator gives constant receiver amplitude at all ranges out to the threshold cut-off point.

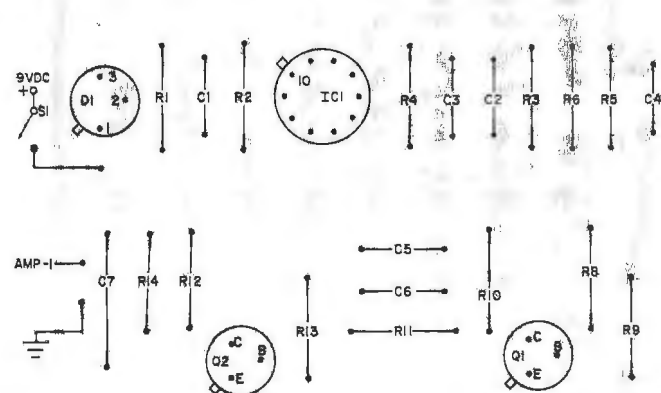
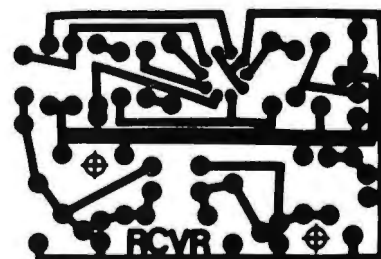


Fig. 6. Actual-size etching and drilling guide for receiver at right. Component layout is at left.



SAFETY CONSIDERATIONS

The GaAs laser used in this system has a peak optical power output of a few watts if operated at maximum current. That is a lot of light compared to the output of low-power helium-neon lasers; but the optical pulses are brief so that the average power is far less than that of most helium-neon devices.

According to the U.S. Air Force School of Aerospace Medicine, GaAs lasers emitting 10 watts per pulse are not capable of producing detectable eye damage. Three principal factors contribute to this safety margin: the absorption of the infrared in the eye's vitreous humor, imperfect focusing of the infrared, and the laser's low average power.

Nevertheless, a few basic precautions must be followed to insure utmost safety:

1. As with any source of bright light, do not look directly into the laser beam.
2. Avoid pointing the laser at shiny surfaces (mirrors, unpainted metal, etc.) because reflected light can be as potentially dangerous as direct light.
3. Do not point the laser in a direction in which bystanders might look into the beam.
4. Turn off the laser transmitter when it is not in use, to preserve its life and that of the battery.

Final Transmitter Assembly.

When the system is operating properly, remove the LED from the transmitter and install the laser. Mount the laser with its glass window on the back side of the pc board and secure it in place with a #8-32 nut. The plane of the laser junction should be parallel with the narrow side of the pc board. (See Fig. 7.) Next, carefully bend the laser's flying lead so that it goes into its mounting hole. Make sure the lead doesn't short against the laser mounting stud.

CAUTION: Do not connect a VOM to the laser diode. The small amount of

current delivered by the meter will destroy the laser chip.

With the laser in place, test the system again. If it works properly, a 1/2" length of brass tubing (available from hobby shops) is carefully soldered to the back of the pc board with the laser chip at the exact center. Cut a slot from the tube as shown in Fig. 7 to prevent possible shorts. If the tube is not soldered properly the first time, try again until it is centered and level. This tube becomes the laser lens receptacle.

Next use two 7/16" standoffs to mount the laser pc board in the cabinet. A telescoping lens tube made as shown in Fig. 7 is inserted in the tube receptacle. Use a simple lens with a diameter of 12 to 15 mm and a similar focal length. Use epoxy to secure the lens in place.

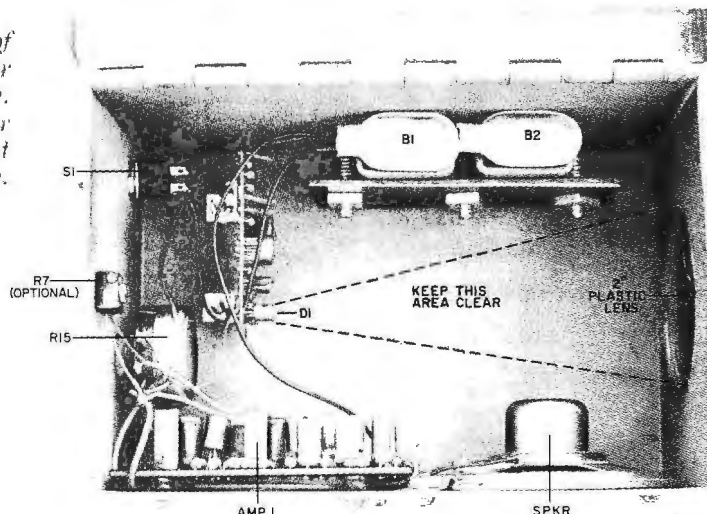
Optical Alignment. Both transmitter and receiver must be aligned with infrared light for best results. This is no problem with the receiver if the lens called for in the parts list is used since its infrared focal length is 4 1/4". For other lenses, add perhaps a quarter of an inch to the visible focal length.

Alignment of the transmitter is more difficult due to the small size of the laser source. An approximate alignment can be made by placing the lens a millimeter or so farther from the laser chip than the visible focal length

of the lens. An approximate alignment will give a broad beam suitable for communications up to about 1000 feet. For long ranges, the beam must be made nearly parallel by adjusting the lens for as small a beam spread as possible. This is easily done if an infrared image converter is available.

Surplus sniper scopes are ideal for this purpose, but they are expensive. Kodak makes infrared-sensitive phosphor screens which glow orange when struck by a beam from an IR laser or LED. These screens cost about \$25 (a lot less than electronic

Photo of receiver prototype. Leave a clear path for light to hit diode.



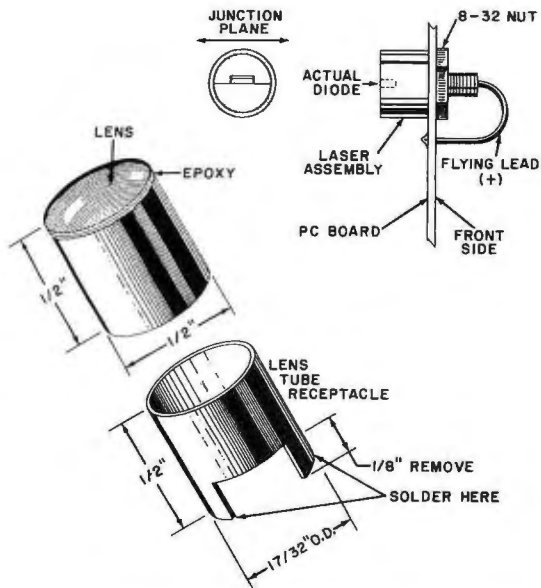


Fig. 7. Mounting details for laser and lens tube.

image systems). Write Special Product Sales, Kodak Apparatus Div., Eastman Kodak Co., Rochester, NY 14650 for details and prices.

Align the laser lens by pointing the beam at a white card (or the phosphor screen) at least 3 feet away and focus the lens for the smallest spot size. Use the infrared viewer to see the spot if the white card is used.

When the optimum focus point for the lens is found, use white glue to secure the lens in place and prevent need for realignment.

Telescope Alignment. Range tests of a few hundred feet are relatively straightforward, but long-range operation requires the addition of an alignment telescope for the transmitter. You can use any spotting or rifle telescope of 3X to 10X as long as it has a cross hair. For the sake of economy, in the prototype, an inexpensive 10X pocket telescope was obtained from

Radio Shack for about \$3 (Cat. No. 63-844). (Also available from other electronics outlets.) A cross hair was added by cementing two human hairs to a $\frac{3}{8}$ " washer which was then cemented to a shoulder inside the telescope eyepiece section.

The telescope must be boresighted with the laser. Make an adjustable mount similar to the one shown in Fig. 8. Use two sections of pc board for the mounting platform. Solder three nuts to the back of one board and use springs to permit adjustment.

Aligning the telescope is fairly easy if a phosphor screen or infrared viewer is available. The transmitter is mounted on a tripod with an appropriate nut and the laser is caused to illuminate a fixed spot at least 50 feet away. The telescope is then aligned until the crosshair falls on the target. Recheck the laser to make sure it still illuminates the target and alignment is complete. Perform the alignment at

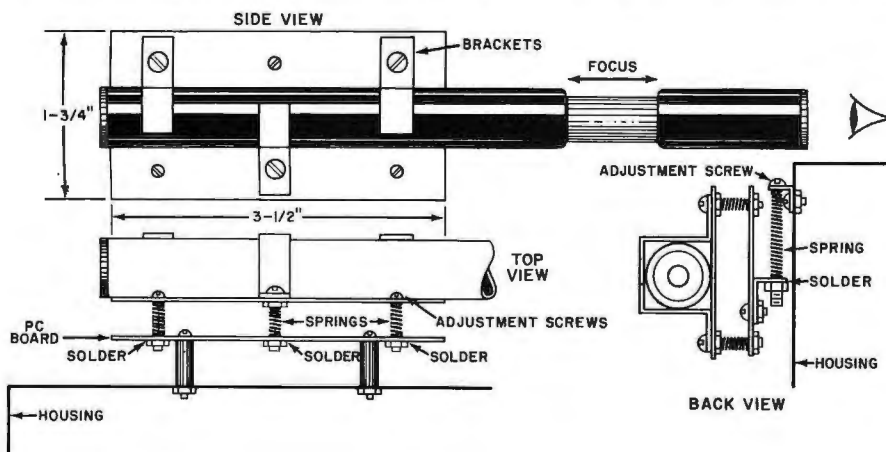


Fig. 8. Details for mounting the telescope which is used to boresight the transmitter.

night for fast results and use a flashlight to illuminate the target when the telescope is being used.

Range Testing. When the telescope is boresighted with the laser, the system is ready for long-range testing. Begin by mounting the laser on a tripod and pointing the telescope at a fence post, car, or other object at least 1000 feet away. Place the microphone near a radio to get a continuous audio signal. Proceed to the target site, and point the receiver toward the transmitter. It will be necessary to move the receiver about until the optimum detection angle and point are found. If no signal is received, the laser beam has probably crossed the telescope field of view at a point beyond the range of the initial alignment target. Therefore, proceed a few feet toward the telescope side of the laser until the signal is received. An infrared viewer is helpful in finding the brightest spot in the projected beam (which is only a few feet across at $\frac{1}{2}$ mile).

Once test techniques for a 1000' range have been perfected, longer ranges can be tried. These tests will be simplified by compensating for the laser-beam crossover problem by appropriately adjusting the horizontal telescope adjustment.

The prototype communicator has been used to achieve a range of 3380' (1.03 km). This could be increased to well over a mile by increasing the laser current, reducing the transmitter beam width, or increasing the receiver lens size. For example, the prototype uses a laser with a threshold current of 4.1 amperes. While the laser can be operated at a top peak of 10 A, transistor Q3 delivers only about 5 A. Therefore, the laser output is only a few hundred milliwatts, while more than a watt would be available at 10 A. With the full 10-A current, the optical-communication range equation shows that range would be slightly more than doubled.

Similarly, a diverging beam of light follows the inverse square law, so doubling the diameter of the receiver lens from 2 to 4 inches will double the range.

More Information. For further reading on laser communications, see: *Semiconductor Diode Lasers*, R.W. Campbell and F.M. Mims, Howard W. Sams & Co., 1972; and *Light Beam Communications*, F.M. Mims, Howard W. Sams & Co., 1975.

A LOW-COST AUDIO- FREQUENCY METER



Four ranges from 5 Hz to 50 kHz.

BY CHARLES GREEN

FOR experimenters who do a lot of work in the audio-frequency range, but can't afford a modern frequency meter, here's an easy-to-build, low-cost unit that may just fill the bill. The meter measures frequency (sine or square waves) from 5 Hz to 50 kHz in four switch-selectable ranges. Sensitivity is 0.2 volt rms over most of the range.

Circuit Operation. As shown in Fig. 1, the input signal at *J1* is amplified by *Q1*, a high-input-impedance FET. In *IC1*, a differential dc amplifier arranged in a Schmitt trigger configuration, the waveform is squared off. It is further amplified by *Q2*, another FET. Zener diode *D1* limits the output swing to 9.1 volts.

The waveform then passes to diode array *IC2*, whose circuit includes switch-selected capacitors (via *S2A*) and resistors (via *S2B*) which differentiate the square wave into a series of sharp fixed-amplitude pulses. The rectified dc from the diode array drives the meter, *M1*. The average indication on *M1* is proportional to the number of pulses per second from the differen-

tiator, the number of pulses being determined by the frequency of the input.

Construction. Since only low frequencies are involved, neither the layout nor wiring of the meter is critical. In the prototype, adhesive-backed copper strips and pads were used (Circuit-Stik, Quick-Circuits, Circuit-Zaps, etc.) These are available through many mail-order houses. A simpler way might be to use perforated board, with clips and sockets to mount the components.

The enclosure should be just large enough to mount the switches, meter, and input jacks on the front. Mount the circuit board on spacers on the bottom of the enclosure and the battery assembly of two sets of four AA cells in holders on the rear wall. Use press-on type to identify the components on the front panel. Carefully remove the front cover of the meter and, using a small piece of white paper with the letters Hz on it, cover the μA marking on the meter scale.

Calibration. To calibrate the meter,

you will need an audio-frequency generator (or other known frequency source) covering the range from 50 Hz to 50 kHz.

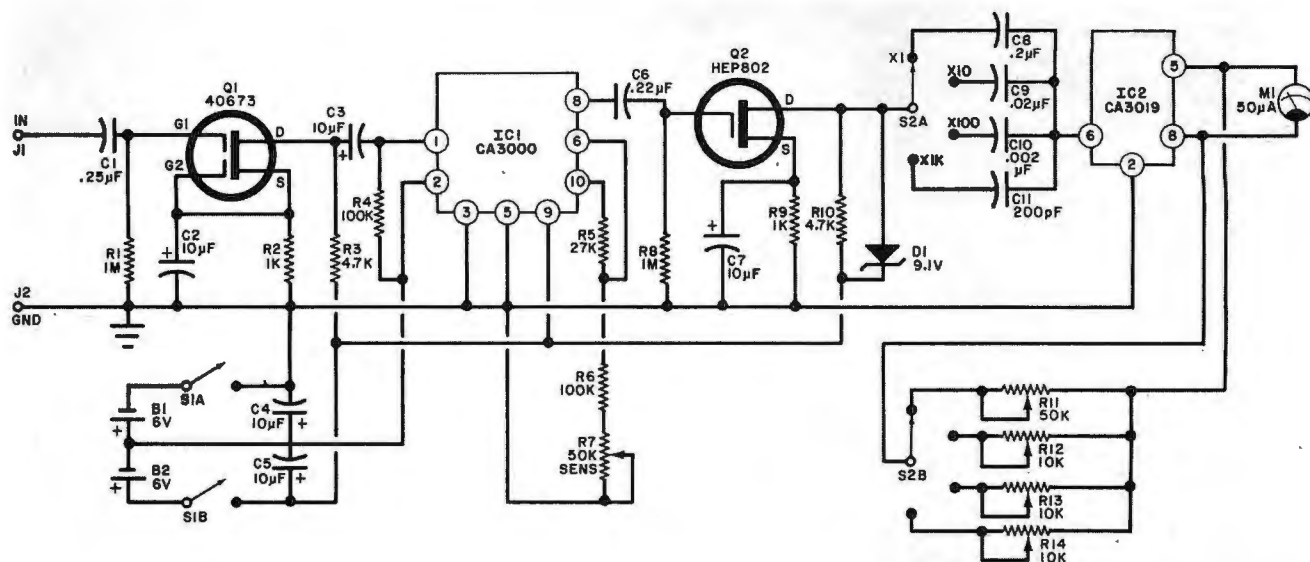
Before turning on the power to the meter, make sure that the needle indicates zero. If necessary, use the zero-adjust screw to set the needle on zero.

Set RANGE switch *S2* to X1000 and turn on the power. Connect the high output of the signal generator to *J1* and the ground to *J2*. Adjust the audio generator for an output of 20,000 Hz at 0.2 volt rms. You may have to adjust potentiometer *R14* to keep the meter from going off scale.

Adjust *R7* (in the *IC1* circuit) for maximum meter indication. Slightly reduce the audio generator output and readjust *R7* for maximum meter indication. Repeat the process until the best sensitivity has been attained (the lowest generator output voltage that will cause *M1* to indicate).

Set the audio generator to 50 Hz at about 1 volt rms and set the RANGE switch on X1. Adjust potentiometer *R11* to get a reading of 50 (full scale) on the meter.

Set the audio generator to 500 Hz



PARTS LIST

B1, B2—6-volt battery (4 AA cells in series)
 C1—0.25-μF, 100-V ceramic or paper capacitor
 C2 to C5, C7—10-μF, 6-V electrolytic capacitor
 C6—0.22-μF, 12-V ceramic or paper capacitor
 C8—0.2-μF, 10%, 12-V ceramic or paper capacitor
 C9—0.02-μF, 10%, 12-V ceramic or paper capacitor

C10—0.002-μF, 10%, 12-V ceramic or paper capacitor
 C11—200-pF, 10%, 12-V ceramic or paper capacitor
 D1—9.1-V, 1-W zener diode (HEP104 or similar)
 IC1—CA3000 dc amplifier (RCA)
 IC2—CA3019 diode array (RCA)
 J1, J2—Banana jack (one red, one black)
 M1—50-μA meter (Midland 23-200 or similar)
 Q1—40673 dual-gate FET (RCA)
 Q2—HEP802 FET
 R1, R8—1-megohm, ½-W, 10% resistor
 R2, R9—1000-ohm, ½-W, 10% resistor
 R3, R10—4700-ohm, ½-W, 10% resistor

R4, R6—100,000-ohm, ½-W, 10% resistor
 R5—27,000-ohm, ½-W, 10% resistor
 R7, R11—50,000-ohm pc potentiometer (Radio Shack 271-219 or similar)
 R12 to R14—10,000-ohm pc potentiometer (Radio Shack 271-218 or similar)
 S1—Dpdt switch (Calectro E2-105 or similar)
 S2—2-pole, 5-position nonshorting rotary switch (one position not used) (Calectro E2-163 or similar)
 Misc.—Aluminum cabinet (LMB 442 or similar), battery holders, mounting hardware, wire, solder, etc.

Fig. 1. High input impedance is provided by FET Q1. IC1 is Schmitt trigger and IC2 is a diode array.

and the RANGE switch to X10. Adjust R12 to get full scale reading of 500 on the meter.

Repeat these steps for the X100 and X1000 ranges, using 5000 and 50,000 Hz inputs and adjusting R13 and R14 respectively.

Disconnect the audio generator and install the metal cover on the frequency meter.

Operation. The one-megohm input resistance (and the high impedance of Q1) places minimum loading on any

circuit being tested. The basic sensitivity of 0.2 volt rms is good from about 30 Hz to 40,000 Hz, but the actual sensitivity depends on the particular FET used for Q1. From 5 Hz to about 30 Hz the sensitivity is approximately 0.4 volt rms. The maximum input voltage is determined primarily by the voltage rating of Q1 (which has no internal diode protection gate).

When measuring an unknown frequency, always use the highest range first and then switch down until the meter indicates on scale. If the voltage of the unknown signal is not higher than the basic sensitivity of the meter (at least 0.2 volt rms) an erroneous frequency indication may be observed. Always measure the voltage value of the unknown frequency before measuring its frequency. If necessary, use some form of voltage divider at the input to the frequency meter.

At periodic intervals, check the battery voltage and, if necessary, recalibrate the frequency meter to compensate for changes in characteristics due to component aging.

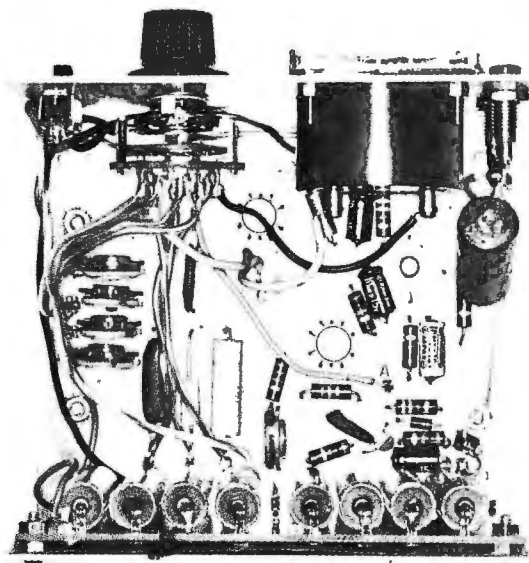


Photo shows the arrangement of the author's prototype.

A NEW NATIONAL TV NETWORK?

*Communication satellites may make a
national pay TV network a reality.*

IT IS possible that there will be a new, fourth television network in the United States. It will differ from the "Big Three" in several respects—signals will be carried by coaxial cable rather than the airwaves; programming will include current films, sports events, concerts and theatre; and viewers will pay a per-program fee in addition to a monthly service charge.

Regional "Pay TV" has gained some acceptance with more than 130,000 homes subscribing to its services. (This is not to be confused with "Cable TV," which duplicates standard TV broadcast fare.) Now three companies, including two regional Pay TV firms, have applied for FCC permis-

sion to form a *national* network using the cable format. The stimuli of this renewed interest in a Pay TV network are developments in satellite communications and increased public acceptance of the two representative Pay TV systems.

Under the proposed format, program material would be beamed to a domestic communications satellite (See drawing) from a central network studio (A or B). Member cable systems (1 through 8) would receive the program through an earth station connected to their cable plant. Home viewers subscribing to the service would have their choice of regular commercial programming or the spe-

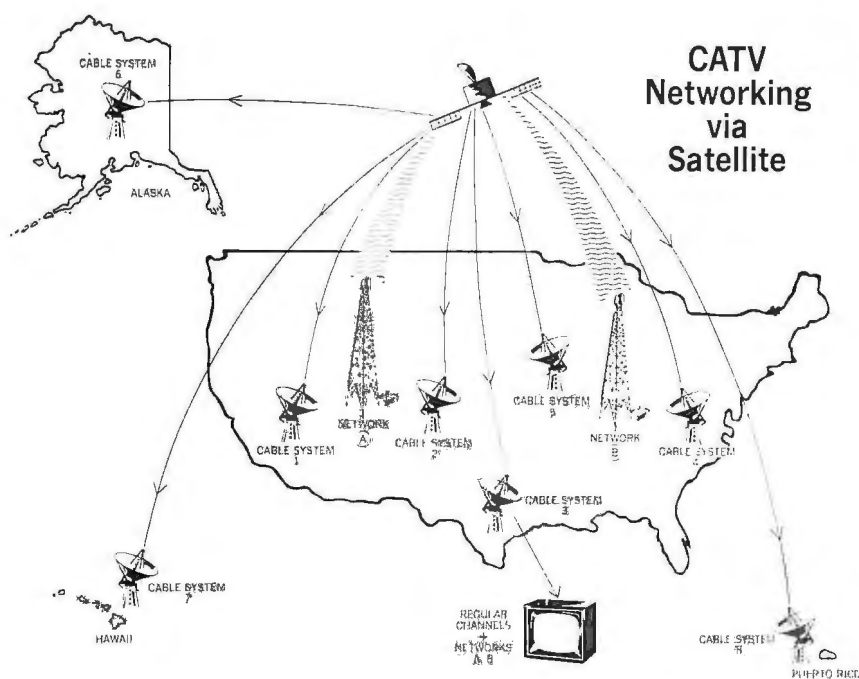
cial "pay" programs sent by the cable network.

The cost of the required earth stations has been steadily dropping because of advances in technology. At present such installations cost about \$100,000, but this is expected to drop 50% in ten years. An RCA communications satellite, part of the Global Communications system, would be employed.

Home Box Office, UA-Columbia Cablevision, and RCA Global Communications are actively pursuing the idea of such a "cable network." UA-Columbia says that 40% of the 10,000 subscribers to its Wayne, N.J., system have purchased the special events channel. In Brookhaven, N.Y., 4,000 of the 24,000 subscribers bought it in less than five months.

UA-Columbia hopes to build earth stations in 1976 for its cable systems at Fort Smith, Ark.; Laredo, Texas; Yuma, Ariz.; El Centro, Calif.; and Pasco and Kennewick, Wash. AT&T proposes to build an earth station at Orlando, Fla., to provide the Home Box Office features to several of its cable systems in central Florida, as well as to nearby systems operated by other cable companies.

Studies made by Knowledge Industry Publications, Inc. show that the establishment of a national cable TV network would require a capital investment of more than \$75 million, and that the network would operate at a loss for the first four years. Afterward, profits are expected to steadily grow, with a cumulative cash flow exceeding \$400 million in 10 years. This compares to estimates of \$4.2 billion in advertising revenues projected for broadcast TV networks by 1984. ♦



HAVE FUN WITH ELECTRONIC DICE

*Electronic game
of chance
uses TTL & LED's*

BY R. M. STITT

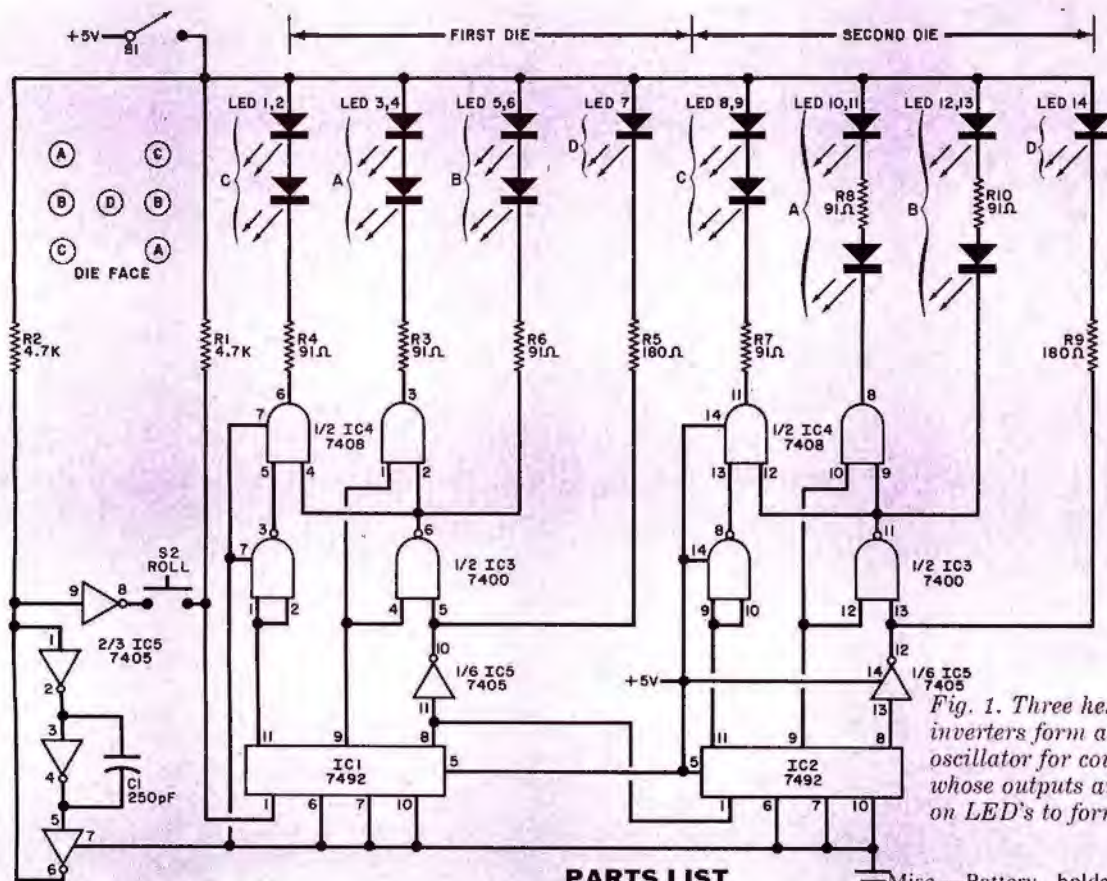


The rolling of dice is one of the oldest games known to man. In ancient times, dice were actually carved out of bones, with various characters on the six sides. Today, we have electronic dice. Though some of the character of the game may be lost

in the transition from rolling the bones to pushing a button, the chances of winning and losing are still the same (sometimes better, since there are no mechanical irregularities to modify probabilities). Also, electronic dice can be used in the dark and don't emit

rattling noises that can be disturbing to some people.

The electronic dice device described here is easily built and comes in a neat, simple package. It makes an ideal game for children and grownups whatever their ages.



PARTS LIST

B1—Four AA cells (see text)
C1—250-pF, 10-V disc capacitor
IC1, IC2—7492 divide-by-12 counter
IC3—7400 quad 2-input NAND gate
IC4—7408 quad 2-input AND gate
IC5—7405 hex inverter
LED1 to LED14—Red LED (matched, see text)

R1, R2—4700-ohm, 1/2-W, 5% resistor
R3, R4, R6 to R8, R10—91-ohm, 1/2-W, 5% resistor
R5, R9—180-ohm, 1/2-W, 5% resistor
S1—Spst switch
S2—Spst normally open pushbutton switch

Misc.—Battery holder, plastic case (Davis 200 or similar), mounting hardware, etc.

Note: The following are available from MITS, Inc., 6328 Linn, N.E., Albuquerque, NM 87108: pc board alone at \$5.00; complete kit of all parts, including board but not case, at \$28.

Fig. 1. Three hex inverters form a 1-MHz oscillator for counters whose outputs are displayed on LED's to form dice.

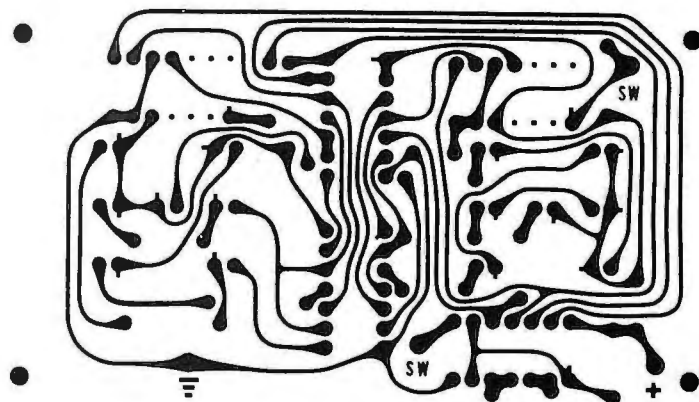
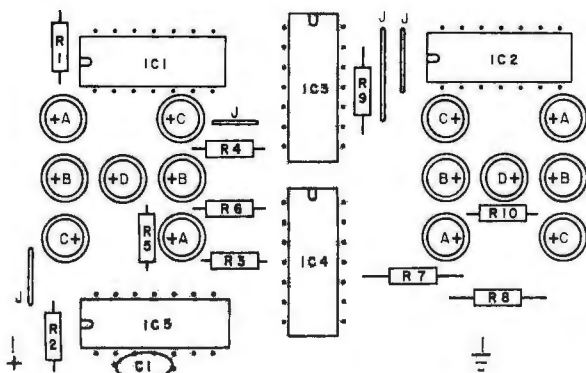


Fig. 2. Actual-size foil pattern is shown at right. Component installation at left.

Circuit Operation. As shown in Fig. 1, three of the six inverters in *IC5* are interconnected with *C1* and *R2* to form a clock oscillator running at about 1 MHz. A fourth inverter in *IC5* is used as a buffer to drive the first die circuit (*IC1*). This IC is a divide-by-12 counter consisting of a divide-by-2 (not used) and a divide-by-6 (used). The outputs of the counter are decoded by one inverter in *IC5*, two NAND gates in *IC3* and two AND gates in *IC4*. The decoded outputs then drive directly the six LED's which form the face of one die.

The output (carry) from the first die is used to drive the second die circuit formed by *IC2* and the remaining elements of the other IC's.

When the roll switch, *S2*, is operated, the clock oscillator is coupled to the first die, and its circuit runs through its states at a rate of 1 million times per second. The second die runs

through its states at about 166,000 times per second. When *S2* is released, the LED indication is truly random, with the same probability as an actual pair of theoretically perfect dice would have.

Construction. Neither the circuit layout nor lead dress is particularly critical, but an effort should be made to minimize the length of the lead between the 1-MHz oscillator and the first counter (*IC1*). If desired, a pc board can be made, using the etching and drilling guide shown in Fig. 2.

There are two ways to mount the LED's. The first is to mount them directly on the pc board in their designated places, making sure that their tops are at least 3/16" to 1/4" above the tops of the integrated circuits. Then the top cover of the enclosure must be drilled so that the seven LED's for each die protrude

through the holes. The pc board can then be mounted on the top cover using suitable mounting hardware. The LED's should be selected (by connecting them to a 5-volt dc source through a 180-ohm, 1/2-watt resistor) to make sure that they all glow with about the same brightness.

The pc board fits in the plastic case given in the parts list. When the top of this case has been drilled for the LED's, it is covered with a red anti-glare filter that obscures the unlit LED's. This makes the face of each die clear.

The batteries (in their holder) are secured to the bottom of the case and a piece of foam rubber is placed on top of the batteries so that the pc board and LED's make a tight fit when the case is closed. The foam rubber keeps things from moving about. Of course, with this approach, the pc board need not be attached to the cover. In the prototype, nickel-cadmium cells were used. Although their initial price is high, they can be recharged many times.

The second way of mounting the LED's involves drilling the top cover and attaching the LED's to it with epoxy. Then lengths of insulated wire can be used to interconnect the LED's and the pc board.

Operation. When the power switch is first turned on, the dice should illuminate in combination. This initial state is determined primarily by the mismatches in the thresholds of the IC's and will vary with the IC's. Therefore, this "start-up" state is not random and should not be used as a "throw" of the dice.

When the roll pushbutton is depressed, all 14 LED's should go on. Some will be brighter than others due to the differences in their duty cycles. When the button is released, the display will be a random roll. ♦

A ROLL-DOWN CIRCUIT

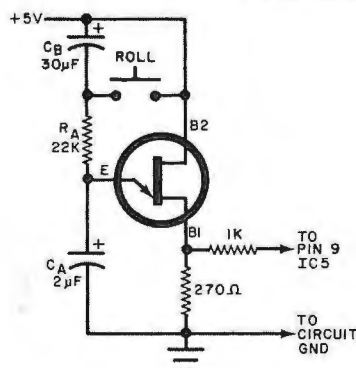
While testing the electronic dice, we experimented with finding a way to produce a "roll-down" similar to the effect obtained when regular dice are thrown. This can be done by using the circuit shown here to replace the three-inverter oscillator portion of Fig. 1.

The output of the UJT is coupled to pin 9 of *IC5*, while pin 8 of *IC5* is connected directly to the junction of *R1* and pin 1 of *IC1*. The *R1* of the original circuit is required because the 7405 (hex inverter) has an open collector on its output transistor. Note the new position of the roll pushbutton.

When the roll switch is pushed, the UJT forms a conventional oscillator with a frequency determined by *R_A* and *C_A*, whose values can be changed as desired. When the switch is released, the dc supply is removed from the timing circuit and *C_B* is included in the circuit. As the charge on *C_B* leaks off,

less and less voltage is applied to the timing circuit and the oscillator frequency drops. This causes the dice display to "slow down" and, as the voltage drops to almost zero, the dice stop rolling. Reclosing the roll switch will start the roll again. The value of *C_B* can be changed to vary the duration of the roll-down time.

—The Editors

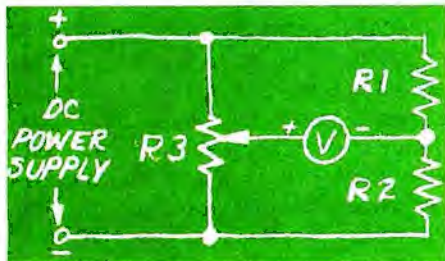


Precision Matching of RESISTORS

Home experimenter technique for matching resistors to better than 0.5%

BY JAMES DEMAS

PRECISION matching of resistor values is extremely important in such circuits as bridges and differential amplifiers. At first glance, you might think that an easy way to match values is to use expensive 1% or better precision resistors. A close look at the situation, however, will reveal a basic flaw in this plan. If you use 1% resistors, one resistor might be 1% higher and the other 1% lower than the nominal value required. Hence, the matched-pair tolerance would be 2%.



Ordinarily, when you need closely matched resistor pairs, the absolute resistance value is not as important as how close the values are to each other. Closely matched resistors whose absolute values are "in the ballpark" of those required will usually suffice for a given application.

While commercial manufacturers generally use expensive laboratory-type equipment, the home experimenter must find a more economical means for matching resistors. Fortunately, all he needs is a high-impedance multimeter, a 0-to-30-volt power supply, and a 10-turn potentiometer. The meter should have a 10-megohm or greater input impedance and a sensitive low-voltage range, preferably 0.6 volt or less full scale. Almost any value for the potentiometer's resistance between a few hundred and about 50,000 ohms will do for this test circuit.

Resistance-Ratio Method. The Wheatstone bridge that you must set up with the meter, power supply, potentiometer, and resistors to be matched is shown in the schematic diagram. With this setup, you can easily obtain resistance ratios that will permit you to match resistors to better than 0.5%.

The resistors to be matched in the diagram are R_1 and R_2 . These will form one voltage-divider leg of the bridge, while the potentiometer (R_3) will form the other leg. When using this circuit, with R_1 and R_2 in place, adjust R_3 for a null, indicated by the meter reading as close as possible to zero on the most sensitive range. This balances the bridge.

Interchange R_1 and R_2 . If the values of R_1 and R_2 are identical, transposing the two resistors will not affect the meter reading. However, any difference in the resistances will unbalance the bridge and cause the meter to read some positive or negative voltage above or below the null point by an amount proportional to the ratio of the two resistor values.

The resistances of R_1 and R_2 are related by the formula

$$\frac{R_2}{R_1} = \frac{1 + \frac{\Delta E^*}{E}}{1 - \frac{\Delta E^*}{E}}$$

* $\Delta E = E_2 - E_1$

where R_1 and R_2 are the values of the resistors to be matched, E is the power supply voltage, E_2 is the meter reading after transposing the resistors, and E_1 is the initial meter reading after nulling. The formula applies only if the power supply and meter are connected as shown. Also, E_2 and

E_1 have polarity signs that must be carried into the calculations.

A sample calculation of how to use the formula is instructive. Assume two 175,000-ohm resistors are compared using an 18.5-volt supply potential. The initial null is at -1.0 mV (E_1) and the final voltage (E_2) is -1.96 V. This yields

$$\frac{\Delta E}{E} = \frac{-1.96 \text{ V} - (-0.001 \text{ V})}{18.5 \text{ V}} = -0.1059$$

$$\therefore \frac{R_2}{R_1} = \frac{1 + (-0.1059)}{1 - (-0.1059)} = 0.8086$$

This means that the value of R_2 is lower than that of R_1 by $1 - 0.8086$, or about 19.1%.

For matching resistor values greater than 5000 ohms, use an 18- or a 27-volt supply potential. For resistors of less than 5000 ohms, use a 9-volt supply potential. Resistances of less than 1000-ohms should not be matched by this procedure because of their excessive power dissipation.

Another point to keep in mind is that, when the values of R_1 and R_2 exceed about 50,000 ohms, the first equation will be in error, owing to the meter's inherent loading effect on the circuit. This results in a ΔE measurement that will be too small. To correct for the error, replace the ΔE entry in the formula with

$$\Delta E \left(\frac{R_m + 0.5R_1}{R_m} \right)$$

Where R_m is the input impedance of the meter. Finally, because of noise pickup and the magnitude of the correction term, resistances greater than

10 megohms cannot be reliably matched.

With the resistance-ratio method, you can obtain matching accuracies of almost 0.05%. If you use a very sensitive meter—say a DMM with a 10-mV full-scale range—you will in all likelihood be able to match resistors to better than 0.01%.

Matching the Resistors. There's an obvious—but usually impractical—procedure for matching resistors: select one resistor from a batch having the same nominal value and proceed to measure ratios until you hit on a close match. A more practical procedure would be to trim one resistor to make it equal to the other.

The initial trimming is of two types. In series trimming, the lower resistance is increased by adding in series with it another resistor of the proper value. In parallel trimming, the larger resistance is decreased by connecting a resistor of the proper value in parallel. Series trimming is preferred where possible. When the lower-value resistor is a standard or reference that cannot be modified, however, you have no alternative but to employ parallel trimming.

In series trimming, if R_2 is greater in value than R_1 (you can always change your reference to make R_2 the smaller resistance), the necessary series resistance for R_1 , designated R_s , can be calculated by using the formula

$$R_s = R_1 \left(\frac{R_2}{R_1} - 1 \right)$$

The absolute value of R_1 may not be known, requiring that you use the nominal value for computation. The closest commercially available value for R_s can be used. These two error sources, however, usually prevent the trimmed pair from being perfectly matched. But the matching will still be much better than if you just took two precision resistors of the same nominal value and used them.

With parallel trimming of the larger-value resistor, trimming resistor R_p 's value can be computed by

$$R_p = \frac{R_2}{\frac{R_2}{R_1} - 1}$$

Again, R_2/R_1 is greater than 1, and the nominal value of R_2 is used in the cal-

culation. This procedure works well if R_2/R_1 is not too close to 1.000. As the ratio approaches unity, R_p becomes prohibitively large. Hence, with parallel trimming, use an R_p that is slightly lower in value than that calculated from the equation. This makes R_2 a little lower in value than R_1 . Then series trim as discussed above for any final adjustment of the ratio.

If the match is still inadequate, further trimming will make it approach the ideal. With series trimming, if R_s is too low, add another resistor of lower value in series with R_1 and R_s to correct the value. If R_s is too large, the combination of R_s and R_1 is greater than R_2 . Several solutions are possible. Series trim smaller resistance R_2 . Alternatively, connect a suitable resistance in parallel with R_s —NOT the series combination of R_s and R_1 —to reduce it to the correct value.

The required parallel trimming resistor, R_p , for R_s is calculated by

$$R_p = \frac{R_s \left(1 - \frac{R_1}{R_2} \right)}{\frac{R_1 + R_s}{R_2} - 1}$$

where R_1/R_2 is just the inverse of the original ratio determined for the resistor pair, and $(R_1 + R_s)/R_2$ is the ratio determined after the first trim.

The most economical type of resistors to use for matching are 10% composition types. Using 10% composition resistors and the matching procedure outlined above, you can be sure of better than 1% matching for less than the cost of two 5% resistors. Absolute accuracy will be sacrificed, however. But if you buy your resistors all at one time and from the same place, they will usually be from the same batch. Resistors in a given batch are usually closely matched.

Matching composition resistors to better than 0.5% is possible, but such resistors have poor inherent long-term stability, especially for values exceeding 1 megohm. Stability can be improved by operating the resistors well below their rated power and by burning them in before matching. Once matched, treat the resistors as you would semiconductor devices. Don't overheat them and use a low-power soldering iron and heat sinks on the leads.

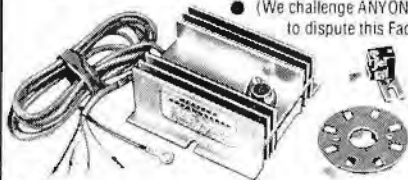
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Product Test Reports

ABOUT THIS MONTH'S HI-FI REPORTS

The three, very different products in this month's reports have two things in common: they are all innovative and they deliver outstandingly fine performance.

Many people think a preamplifier should do nothing but amplify and possibly alter the frequency response of a signal. Phase Linear's very different philosophy is exemplified by its Model 4000 preamplifier. In addition to all of the usual preamplifier features, it has a unique autocorrelator circuit that removes most of the hiss, hum, and rumble from a signal without the least audible effect on its frequency response. It also has a dynamic expander that restores much of the dynamic range removed from every recorded or broadcast program.

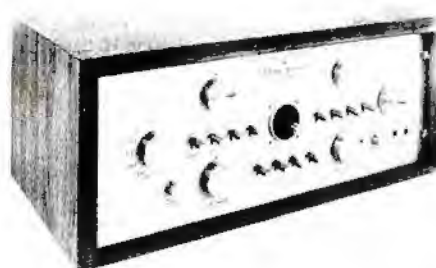
JVC's new deluxe cassette deck, Model 1669, combines a very smooth, solenoid-operated, remote-controlled tape transport with a refined ferrite head that extends its useful frequency response to just short of 20 kHz. The JVC1669 has its own ANRS noise reduction system, which is similar to the Dolby system in its effect.

Pioneer's headphones deliver the performance you would expect from the better electrostatics at a fraction of their price, and in a nearly "feather-weight" package.

—Julian D. Hirsch

PHASE LINEAR MODEL 4000 STEREO PREAMPLIFIER

Superb preamp features unique signal processing system.



Unique noise reduction and dynamic range-expanding circuitry are among

the many features of the Phase Linear Model 4000 preamplifier. The preamp has inputs for two phono cartridges and two high-level program sources and a tape playback input for one of the two tape decks it can control. The other tape recorder's playback can be monitored during recording, and it is possible to copy from it to the first deck while listening to another program source through the preamp.

The preamplifier measures 19"W × 8 3/4"D × 7"H (48 × 23 × 18 cm) and weighs 18 pounds (8.2 kg). It retails for \$599.

General Description. The separate bass and treble controls for each channel have selectable turnover frequencies of 40 or 150 Hz for the bass and 2000 or 8000 Hz for the treble. (A separate switch is provided for bypassing the tone control circuits.) Each control is an 11-position switch. The volume control, which cannot reduce the output to zero, is augmented by a 20-dB attenuator switch to provide an adequate control range.

Channel balance is by means of a "joystick" control located in the center of the front panel. Although this is basically a stereo preamp, it has built into it an SQ decoding matrix with Phase Linear's own front-back logic system that can be used to decode SQ discs or FM broadcasts or to synthesize rear-channel "ambience" outputs from stereo programs.

Input selection and tone and volume settings are made with rotary controls. All other switching functions are available via lever switches. Lever switches also control the special signal-processing circuits and an "active equalizer" that provides a slight boost at very low and very high frequencies where most speaker systems fall off appreciably in their responses.

Perhaps the most unique feature of the preamp is its "autocorrelator" noise reduction system that operates on any input source. Unlike the Dolby system, the autocorrelator does not require specially processed program material. In a sense, it is a dynamic low-pass filter whose action is controlled by the levels and frequency distribution of the program material. There is, however, an important difference.

Signals in the 200- to 2000-Hz band are sensed to determine the presence of discrete frequency components, as opposed to random noise. Any discrete frequencies detected cause "windows" to open up on the preamp's 2000- to 20,000-Hz response range at harmonics of the control signals. (The control signals are assumed to be musical fundamentals.) In this manner, the normal harmonic structure of the program is not affected; yet, the portions of the 2000- to 20,000-Hz spectrum not required to pass the harmonics are closed off, excluding noise components not related to the signal.

A small control knob on the front panel permits continuous operational threshold adjustments to be made for the autocorrelator. Adjustment of the control is not critical. As it is turned counterclockwise, the hiss suddenly drops. Only after considerable additional rotation do the highs in the program drop out. Within its operating range, the system reduces hiss by about 10 dB, with no effect on the frequency content of the output signal.

The autocorrelator switch also turns on a low-frequency dynamic filter that removes rumble and hum from only the phono signals. Its threshold adjustment is via a screwdriver-operated control that is accessible through a hole in the front panel. The filter cuts the response at 20 Hz and below by some 15 dB without any loss of low-frequency program material.

The second unique feature of the preamp is its "Peak Unlimiter and Downward Expander." Turned on by a separate lever switch, it is a sophisti-

cated volume-expansion system that provides several different expansion characteristics according to the instantaneous program level, with different time constants in each operating area. A small knob on the control panel is used to set the threshold for the filter system.

When the filter system is operating, a red LED flashes on signal peaks. The total expansion is 7 or 8 dB, sufficient to restore much of the dynamics of a program normally suppressed by recording and broadcast compressors or limiters. The filter is not detectable in action, nor does it add any unnatural qualities to the signal.

The preamp's various inputs and outputs are located on the rear apron. In addition to the four channel outputs, there is a second pair of front-channel outputs. A third set of outputs is on the front panel—two stereo phone jacks for the front and rear channels. Since these come after the signal-processing circuits, they can be used to supply a noise-reduced signal to another tape deck or amplifier.

Two screwdriver controls next to the PHONO 1 inputs compensate for any effect the cartridge's inductance might have on the preamp's equalization so that a true RIAA-equalized response can be achieved. Recommended settings for most phono cartridges are given in the instruction manual.

There are six accessory ac outlets on the rear apron. Three are switched via a heavy-duty relay to control up to 25 amperes of current, which might be required if the preamp were to be used to control power to two high-power amplifiers like the Phase Linear Model 700's.

Laboratory Measurements. In addition to their conventional turn-over points near the frequency extremes, the tone controls have a limited range of about ± 8 dB. Their effects are quite subtle, even when used to the fullest extent; but they make it possible to equalize the response of a good speaker system and make it even better.

Although its function might seem to be much like that of a loudness control, the active equalizer is totally different. At the low end, it begins to boost the response below 70 Hz to about +6 dB at 20 Hz. At the high end, the boost begins at 10,000 Hz and is only 3.5 dB at 20,000 Hz. With most

speaker systems, it can be left on at all times, producing no obvious coloration but definitely enhancing the total sound quality.

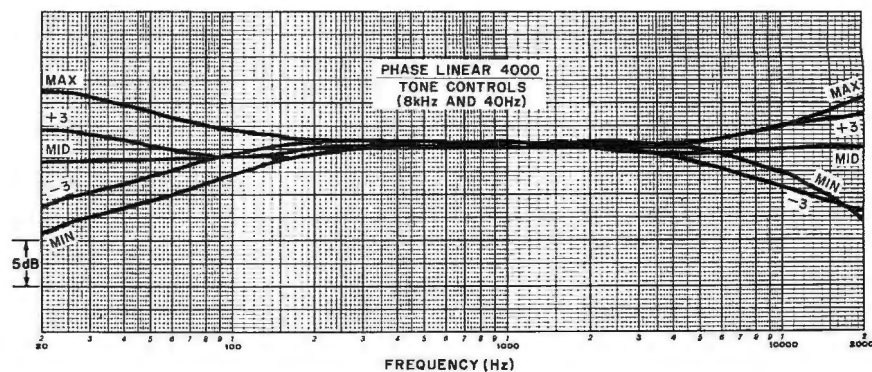
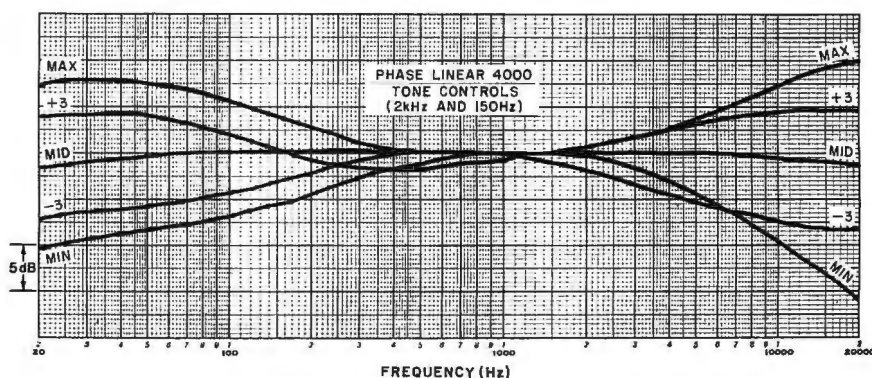
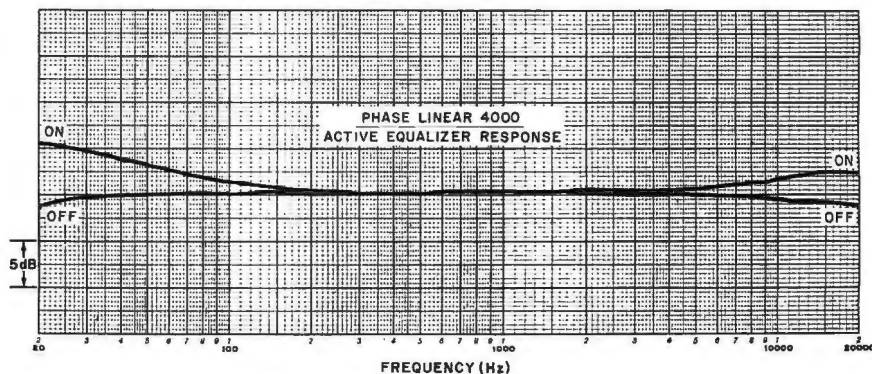
The RIAA equalization was accurate to within ± 0.5 dB from 20 to 20,000 Hz. With proper adjustment of the cartridge compensation controls, the flat response was maintained over the full frequency range. (Most preamps suffer a loss of several decibels beyond 10,000 Hz due to interaction with the phono cartridge.)

To produce a 1-volt reference output, the high-level inputs required 0.175-volt and the phono inputs 1.8-mV signals. The phono inputs overloaded at 62 mV. The unweighted noise in the outputs was -68 dB on the phono inputs, referred to 1 volt. Referred to the rated 8-volt output, each would be improved by 18 dB. (If the associated power amplifier has level controls, they should be set to

require at least several volts from the preamplifier at rated output to gain the maximum S/N advantage.)

The THD at 1000 Hz was less than 0.03% up to a 2-volt output, increasing slowly to 0.1% between 6 and 7 volts and to 0.17% at the rated 8 volts. The IM distortion was less than 0.05% up to 1 volt, 0.25% at 5 volts, and 0.6% at 8 volts.

The dynamic nature of the peak limiter and autocorrelator system prevented us from making measurement of them. They and the SQ decoder were evaluated subjectively by extended listening tests. The autocorrelator proved to be by far the most effective noise reducer that does not require preprocessed signals that we have used. In A-B comparisons, it appeared to be about as effective as the Dolby B system in hiss reduction. Since it can be used with the Dolby or any other noise-reduction system, the



combination of the two actually reduces hiss to complete inaudibility even under very high-level listening conditions.

The peak limiter/downward expander contributed almost as much noise reduction as the autocorrelator. During low-level passages, switching in the expander dropped the level noticeably, with a corresponding noise reduction. On program peaks, switching it in gives a level increase of about 3 dB that is clearly audible. Over most of the intervening range of levels, there is no audible effect. At no time did we hear any "breathing" or other side effects from the expansion process.

The reduction in low-frequency noise accompanying the use of the

autocorrelator adds immeasurably to the sense of realism in the sound. Regardless of the quality of the turntable, most records have considerable low-frequency noise, and the dead silence that replaces it must be heard to be believed.

As an SQ decoder, the Model 4000 appeared to be about as good as the various "partial-logic" systems offered in many receivers. It is substantially better in its front-rear directionality than a simple matrix, but it cannot compare to the latest "variable-blend wave-matching" SQ logic systems.

User Comment. By using the full signal processing facilities of the preamp, it is possible to make a fantastic improvement in program realism.

Used with high-power amplifiers of comparable quality and good speaker systems, the result is an overall realism—even with older stereo and mono discs—that one would believe to be impossible if it could not be repeatedly demonstrated.

We consider the Phase Linear Model 4000 to be one of the most outstanding electronic developments to appear on the hi-fi scene in recent memory. It is unequalled in its ability to provide full-fidelity music reproduction, free from unwanted noises of all types and with a restored dynamic range that some of us occasionally forget is lacking in our recorded and broadcasted programs.

CIRCLE NO. 65 ON READER SERVICE CARD

JVC AMERICA MODEL CD-1669 CASSETTE DECK

Smooth transport operation and automatic noise reduction.



A solenoid-controlled, two-motor transport and JVC America's own automatic

noise reduction system (ANRS) are standard features in the company's Model CD-1669 deluxe cassette deck. Light-touch pushbutton controls operate the solenoids, while a logic system makes it possible to manipulate the controls in any manner without the possibility of tape damage or the necessity of stopping tape motion.

The deck measures 16 $\frac{1}{8}$ "W \times 12 $\frac{1}{16}$ "D \times 5 $\frac{5}{8}$ "H (42.2 \times 30.1 \times 14.3 cm) and weighs 18 $\frac{3}{4}$ pounds (8.5 kg). It retails for \$499.95.

General Description. Separate toggle switches are provided for selecting the optimum bias and equalization for NORMAL, low-noise/high-output (SH), and chromium-dioxide (CHROME) tape formulations. Illuminated legends near the switches indicate when the deck is in the RECORD status, the circuits are set for CHROME tape, and the ANRS is

switched on. The ANRS can be activated manually by operating a toggle switch. It can also be activated automatically by a piece of conducting foil attached to the rear edge of the cassette.

Two large illuminated meters provide monitoring facilities for the recording and playback levels. They are located electrically ahead of the playback level controls. A PEAK light between the meters flashes if momentary peaks exceed the maximum undistorted recording level.

The cassette cover, with cassette, pops up at a touch of the EJECT button. The tape index counter is internally illuminated by a lamp that flashes when the tape is in motion. A three-position MEMORY MODE switch can be set to stop the tape during rewind when the counter returns to a zero reading. It can also be set to automatically return the tape to PLAY at that point. In any mode, the transport shuts down when the tape stops for any reason.

A switch is provided for transferring the recording inputs between the LINE and MIC/DIN sources. Two slide-type controls with detented settings permit the recording gain and playback level to be set as desired.

There are six transport control buttons. Three are for REWIND, PLAY, and FAST FORWARD. A long STOP button sits in front of these three buttons, while the RECORD button is located some distance away. The RECORD and PLAY buttons must be depressed simul-

taneously to make a recording. A novel feature of this deck is its ability to transfer from the PLAY to the RECORD mode at any time while the tape is playing by pressing both the RECORD and PLAY buttons. Finally, the PAUSE button, when depressed, instantly stops tape motion without interrupting the recording mode.

On the rear apron are the LINE inputs and outputs, a DIN connector, and a socket for the remote-control accessory supplied with the deck. The accessory duplicates all the transport controls, except PAUSE, on a small box that measures 5" \times 2" \times 1 $\frac{1}{2}$ " (12.7 \times 5.1 \times 3.8 cm). The box is equipped with a 16' (4.9-m) cable.

An insert on the front edge of the deck's walnut base contains the headphone jack and two standard phone jacks for the MIC inputs. The recess is covered by a sliding clear plastic door when access to it is not required.

Laboratory Measurements. The equalization switch on the deck changes the playback response to the 70- μ s characteristic for CrO₂ tapes. This produced a playback frequency response within ± 2 dB from 40 to 10,000 Hz, the tape limits, with the 70- μ s Teac 116SP test tape. Problems with older 120- μ s tapes prevented us from measuring the playback response with ferric-oxide tapes; but listening to previously recorded tapes convinced us that the equalization was accurate for both cases.

In the recording mode, a 77-mV LINE or a 0.3-mV mic input yielded a 0-dB meter indication. The corresponding playback was 0.34 volt. The mic inputs overloaded at 35 mV. The record/playback performance was tested with two types of tape: TDK SD using both NORMAL and SH bias and equalization, and TDK KROM-O₂ chromium-dioxide tapes.

At a 0-dB recording level, the 1000-Hz playback THD was about 1.9%. This was essentially all random hiss, since we could see no harmonic components in the output of our distortion analyzer. The reference 3% THD was reached at recording inputs of +5.5 dB (TDK SD/NORMAL), +5 dB (TDK SD/SH), and +4 dB (CrO₂).

The unweighted S/N was about 49 dB. It improved to about 55 dB with IEC A weighting and to about 60 dB when ANRS was used. The difference between the tapes never exceeded 1 dB in these measurements. The noise level increased by only 3 dB, an unusually low figure, through the mic inputs at maximum gain.

The overall record/playback frequency response at a -20-dB recording level was ± 2 dB from 26 to 16,000 Hz with all the tapes used. (The low-frequency response reached 23 Hz at the -2-dB point when using CrO₂ tape.) There were slight differences in the high-frequency responses of the tapes, however, with TDK SD/SH giving the flattest overall response, TDK SD/NORMAL having about 0.5 dB greater output between 10,000 and 15,000 Hz, and the CrO₂ output sloping slightly downward beyond 13,000 Hz. The frequency response, measured at a 0-dB level, revealed the early and pronounced drop in high-frequency response that one finds with all cassette recorders and most open-reel machines due to tape saturation. As would be expected from the improved high-frequency properties of chrome tape, the 0-dB high-

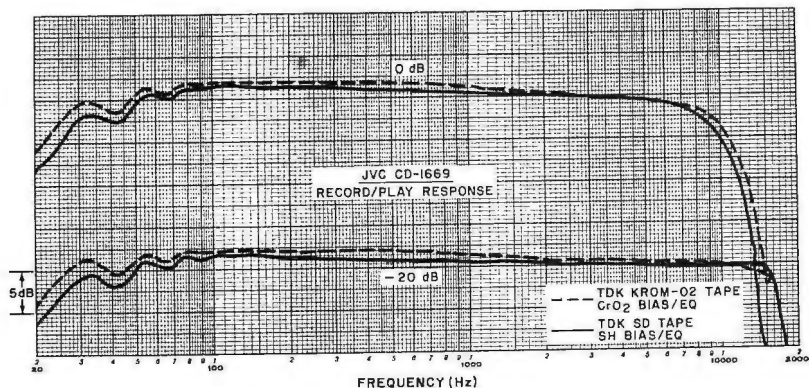
frequency output with CrO₂ tape was somewhat better than it was with ferric-oxide tape.

The unweighted wow and flutter measured 0.05% and 0.19%. A combined record/playback measurement yielded slightly lower numbers of 0.03% and 0.17%. In its fast speeds, the transport handled a C-60 cassette in about 75 seconds. The recorder's meters responded to a 0.3-second tone burst—a standard test for the ballistic response of a VU meter—with an overshoot of about 10%. A 200 nanoweber/meter Dolby-level tape indicated between +3 and +4 dB on the meters. (The +3-dB point corresponds to a CAL mark for the ANRS, which is claimed to be compatible with the somewhat similar Dolby system.)

The PEAK light flashed at +5 dB, the approximate input that produces 3% distortion on playback. The tracking of the ANRS, the change in overall record/playback frequency response when the ANRS is used, was very good at -30- and -40-dB levels, with typical differences of 1 dB or less below 12,000 Hz. At -40 dB, the ANRS introduced a gradual rolloff in response beginning at about 1000 Hz. It reached 2.5 dB at 13,000 Hz.

User Comment. The electrical and mechanical performance of the deck was fully up to the standards of a top-quality cassette recorder. Programs taped from records and FM broadcasts have a fidelity that makes it almost impossible to tell the recording from the original. Although other decks can do this, few can match the operating ease and versatility of the JVC deck.

The logic-and-solenoid control of the transport puts one in mind of the finest open-reel recorders. It is literally impossible to do anything wrong when operating the controls. The controls themselves have a light but posi-



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CIRCLE NO. 19 ON READER SERVICE CARD

tive feel. The MEMORY MODE rewind is a great convenience, both as a means of returning to the beginning of a selection and as an effortless way to repeat any given selection.

This recorder has more recording "headroom" than most cassette decks. One can record with the meters regularly reaching the 0-dB mark or even going into the red area without serious risk of overload distortion. Unlike most recorders, this deck produced a useful volume level with 200-ohm headphones as well as with the usual 8- to 16-ohm "standard" phones to which other recorders are restricted.

The automatic switching of the ANRS with a suitably prepared cassette is an excellent idea, and it

worked to perfection. The noise-reduction system is said to be compatible with other such cassette tape systems, presumably referring to the Dolby system. Although the two systems are not entirely identical in their characteristics, it appears that they are sufficiently alike to permit a Dolby-encoded tape to be played through the JVC deck with perfectly acceptable results, and vice versa. When we tried changing tapes and decks, both systems seemed to afford about the same amount of noise reduction. Neither had a significant effect on overall frequency response.

When we switched tapes, the differences in response were usually no greater than one would expect for two machines without noise-reduction

systems. One exception to this was the playing of prerecorded Dolby-encoded tapes in the Advent CR/70 series, which sounded a trifle dull in their highest registers through the JVC deck. Even so, it was not the type of change that would have been detected without previous familiarity with the sound of these tapes or by a comparison to playback through a Dolby machine.

By and large, we feel that the deck can do just about everything that any other two-head cassette machine can. In many respects, it is superior to most others. This performance, plus superior operating "feel," excellent construction, and versatile operating features, easily justify the price.

CIRCLE NO. 66 ON READER SERVICE CARD

PIONEER MODEL SE-700 HI/FI HEADPHONES

New "high-polymer" material provides light weight and uncolored performance.



**HIRSCH-
HOUCK**

Hi-fi headphones have traditionally been either electromagnetic or electrostatic in design. The electromagnetic phones resemble miniature loudspeakers. They can be very efficient and are capable of delivering a high acoustical output with very low distortion, but their frequency response is as irregular as that of a dynamic loudspeaker. On the other hand, electrostatic phones can have a smooth response over a wide frequency range, but their acoustical output is limited and they require dc polarizing and high signal voltages for proper operation.

Recently, a new type of headphone that combines the advantages of both types of phones with few of their disadvantages has been developed. It uses a specially processed plastic material, known as a "high polymer" (HP), that has piezoelectric properties.

When an electric field is applied across the thickness of a sheet of this material, the length or width changes. One of the first headphones to use the HP material is the Model SE-700 stereophones from U.S. Pioneer Electronics Corp.

The 13-ounce (370-g) headphones have earcups that are flat, with perforated back surfaces, and surrounded by soft foam ear pads. The phones are fitted with a 3-m (about 10') long straight—not coiled—cord that is terminated in a three-circuit plug for stereo operation. Although the phones are not completely transparent to outside sounds, they do not appreciably attenuate room noises.

The retail price of the Model SE-400 headphones is \$79.95.

General Information. The Pioneer phones use a bimorph element that consists of a 7-micron (0.3-mil) film of polyvinyl fluoride sandwiched between two metal electrodes. The whole is formed into a curved surface and is clamped at the edges. When an audio signal is applied across the electrodes, the element flexes and produces an acoustical output. The HP elements have most of the performance attributes of electrostatic drivers and some unique advantages of their own.

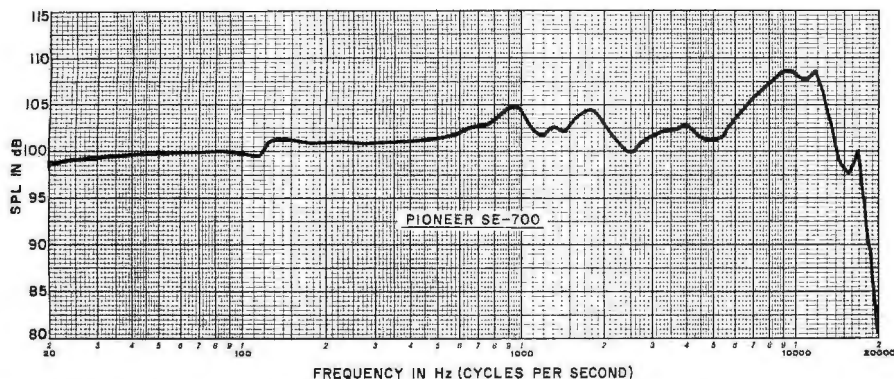
An HP element does not require the high-level signal voltages of an electrostatic element. It, therefore, does not need a step-up transformer. Addi-

tionally, there is no need for a polarizing voltage.

The Model SE-700 phones are rated to generate a 100-dB sound-pressure level (SPL) with only 3 volts applied to their elements. The elements themselves are capacitive in nature, with a value of about 0.1 μ F. They can withstand high voltages (more than 30 volts rms) without sustaining damage. As is the case with an electrostatic element, the entire surface of an HP element is driven uniformly and is free of the majority of the spurious resonances common to dynamic drivers. Unlike electrostatic (and electret) phones, whose operation depends on surface effects and can be affected by humidity, the polarization of HP elements is within the plastic material itself and is permanent.

The phones can be driven from any power-amplifier speaker or headphone output capable of developing several volts. Their high impedance, however, makes them unsuitable for use with tape decks or other components designed to drive only low-impedance phones.

Laboratory Measurements. We tested the phones on a Koss-type acoustic coupler (artificial ear), driving them from a power amplifier at a constant 3-volt output. The resulting response curve was one of the smoothest we have ever obtained for a headphone. The output varied by only ± 3 dB over a frequency range of 20 Hz



to 7500 Hz. There was a rise in output in the 10,000- to 12,000-Hz range that roughly coincided with the diaphragm resonance of our microphone.

We did not attempt to apply a microphone correction to the curve because the other limitations of the headphone coupler measurements would not justify it. In any event, the overall response of 20 to 17,000 Hz, ± 5 dB places the Model SE-700 phones in contention for top honors with respect to range and the smoothness of performance within that range.

The acoustic output over most of the range measured approximately 100 dB SPL, as rated by Pioneer. At 1000 Hz and an SPL of 106 dB, we measured 1% distortion in the acoustical output. The impedance of the phones was greater than 50,000 ohms at frequencies below 150 Hz. It decreased smoothly to about 400 ohms at 20,000 Hz.

User Comment. All the measurements we made on the phones indicated that they should compare to the

best electrostatic phones in overall quality and freedom from coloration. Having made that comparison, our ears agree with the indications given by the laboratory instruments we used in the bench tests. Overall, this is as smooth and uncolored a headphone as we have heard, bested slightly in transparency only by some of the better ES phones. In addition, it is one of the most comfortable to wear and its light weight and absence of a "closed-in" feeling imparted by most phones with tightly sealed earcups makes it almost easy to forget you are wearing the phones.

Further, these phones can play *loud*, without distortion. We proved this, since no amplifier we had on hand, including a couple of brutes rated at 200 watts/channel, could overload them to the point of audible distortion.

Considering all the positive attributes of the SE-700, we feel they are a notable bargain at the price.

CIRCLE NO. 67 ON READER SERVICE CARD

COURIER "CRUISER" MOBILE AM CB TRANSCEIVER

Automatic delta tuning brings in off-frequency signals.



FULL 23-channel AM operation is provided by the Courier "Cruiser" mobile CB transceiver through a crystal-controlled synthesizer scheme. The transceiver is designed to be operated from 13.8-volt dc, positive- or negative-ground electrical systems. It has a special *automatic* delta-tune system that brings in a slightly off-frequency signal on the nose.

Among the more or less standard features are an adjustable squelch, a noise blanker/anl system that can be switched in and out as needed, zener-diode regulation, line filter, reverse-polarity protection, PA operation, external-speaker jacks, and a local/distance (LOC/DX) switch. The indicators include an ON THE AIR light and a meter that indicates both rela-

tive signal strength and relative output power, depending on the mode of operation.

The transceiver measures a compact 9"D x 6"W x 2"H (22.9 x 15.4 x 5.1 cm). It comes with mobile mounting bracket and hardware and a detachable push-to-talk microphone with attached coiled cord. The transceiver retails for \$219.95. An optional accessory power supply, Model PS20A, for using the rig as a base station is available for \$34.95.

The Receiver. A dual-gate MOSFET r-f amplifier, protected by shunt diodes at the input, serves as the receiver's front end. This plus double conversion (to a 10.635- to 10.595-MHz first i-f and a 455-kHz second i-f) provided a measured 0.35- μ V

sensitivity for 10 dB (S + N)/N modulated 30% by a 1000-Hz tone. The primary-image and i-f signal rejection measured an excellent 70 dB. Needless to say, the receiver's sensitivity is better than is usual for CB rigs.

Signal strengths of 100 μ V (40 dB above 1 μ V) or more in or near the CB range tended to introduce spurious signals. Otherwise, the rejection of other spurious signals measured 50 dB.

Mechanical and ceramic filters provide the selectivity at the 455-kHz i-f. This scheme provided good voice intelligibility, with an overall audio response of 375 to 2400 Hz at the -6-dB points. The adjacent-channel selectivity at the i-f itself was 60 dB. However, due to desensitization by an adjacent signal in practice, the 60-dB figure can be derated to 50 to 55 dB. Even so, this is still better than the standard minimum.

Applied to the r-f amplifier, mixer, and first i-f stages, the agc maintained the audio output to within 12 dB with an r-f input signal variation of 80 dB at 1 to 10,000 μ V. Some 6 dB of this change occurred with the first 20 dB r-f change at 1 to 10 μ V, which is somewhat better than par for this end of the range.

The S meter was quite conservative in its indication. It required a 3000- μ V input signal to register an S9. Signals of 100 μ V registered only S5. The squelch threshold range was 0.25 to 500 μ V.

The audio section of the receiver consists of a series gate (that is switched on or off simultaneously with the r-f noise blanker) and two amplifier stages that are followed by the customary push-pull (class-B) power stage. This setup was capable of developing somewhat more output than usual, measuring 4.5 watts at 6% distortion with 1000-Hz signals into an 8-ohm load.

Frequency Synthesizer. Six crystals in the 37.600- to 37.850-MHz range produce the first i-f and four crystals in the 10.180- to 10.140-MHz range create the second i-f for receiving in the conventional frequency synthesis system.

The automatic delta tune (ADT) system is like the automatic frequency control (afc) schemes used in FM receivers. It operates at the 455-kHz i-f and consists of a limiter, ceramic discriminator, dc amplifiers, and a variable-capacitance diode to correct the frequency of the 10.160-MHz crystals in the direction that maintains an exact 455-kHz i-f signal. Its range is about ± 1300 Hz.

The Transmitter. On transmit, one of four crystal frequencies in the 10.635- to 10.595-MHz range is mixed

with one of the signals in the 37.6-MHz range at the synthesizer to produce the transmitter carrier. The carrier goes through a spurious-response filter and on to two r-f driver and the power amplifier stages. The output of the power amplifier is a triple-pi network that matches to a nominal 50-ohm load. Included here are two TVI traps, one of which is fixed at 81 MHz to attenuate the third harmonic, while the other is adjustable around 54 MHz for reducing the second harmonic. Harmonic radiation can therefore be well below FCC requirements.

The driver and power amplifier are conventionally modulated by the receiver's output section. (A speech amplifier is switched in automatically.) Automatic modulation control, or amc, is provided, using a compression system. Electronic switching is used for transmit/receive transfer.

The carrier power measured 4 watts. With a 1000-Hz test tone, compression started at about 90% modulation, with 5% distortion. The distortion rose to 10% with 6 dB of compression. However, time constants of the amc are such that during dynamic operation with voice, peaks can go to a full 100% modulation with a well filled r-f envelope for a good signal punch, while holding adjacent-channel splatter down to better than 55 dB.

The transceiver draws 1.1 to 1.6 amperes on transmit, while on receive, the drain is 350 mA.

User Comment. From an opera-

tional point of view, where difficulties might crop up with a strong local signal, pulling out the squelch control knob conveniently engages the LOC position of the LOC/DX switch. This reduces the receiver's gain by about 20 dB for coping with the situation. With the knob pushed in, the receiver operates at maximum sensitivity.

Although a delta-tune facility is not a real necessity on AM, the ADT in this rig eliminates the need for manipulating a variable control. The user simply pushes a button to place the ADT into operation for automatic frequency correction, indicated by a mid-scale pointer swing of a separate meter. When the ADT is disengaged, off-frequency signals cause the meter's pointer to swing to one side of center-scale.

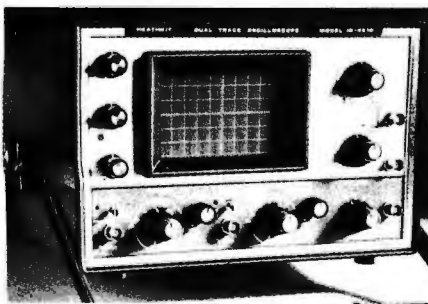
The two meter movements are very small edgewise units, which can make reading them quite difficult in some installations. The knob for the channel selector is also quite small and requires quite a bit of finger pressure to rotate it. The PA, NB (noise blanker), and ADT systems are very easy to switch in and out as desired via a trio of pushbuttons on the front panel.

From the point of view of performance, the Cruiser stacks up well against larger base-station rigs with its good sensitivity and selectivity, fine audio quality, highly effective noise silencing, and a fully modulated signal that can be maintained without adverse splatter.

CIRCLE NO. 68 ON READER SERVICE CARD

HEATHKIT MODEL IO-4510 DUAL-TRACE TRIGGERED-SWEEP OSCILLOSCOPE

Digitally controlled time base gives stable sweep trigger to 15-MHz bandwidth scope.



THE oscilloscope is perhaps the most useful of all electronic test instruments. It lets you see what a waveform looks like as well as measure the waveform's amplitude and period (assuming it has been properly calibrated)—all without the need for other instruments.

The evolution of the oscilloscope over the past few years has been rapid, due to the development of new and better components. While older capacitively coupled (ac) scopes were often limited to a bandwidth of little more than the audio range, the new generation of direct-coupled (dc) scopes features vertical amplifiers that can respond to inputs ranging from dc to many megahertz. Many of the new scopes have true triggered-sweep systems that provide maximum trace stability. Some even have independent vertical sections that provide dual-trace operation.

The constant improvement in oscilloscopes has resulted in some excellent instruments for the service and

experimenter benches. An excellent example of an up-to-the-minute service instrument is the Heathkit Model IO-4510 triggered-sweep, dual-trace oscilloscope that sells for \$549.95 in kit form. (This scope is also available assembled as the Model SO-4510 for \$750.) The published specifications are impressive, such as a dc to 15-MHz vertical bandwidth and 45-MHz triggering bandwidth.

The Model IO-4510 does not have the bulky "box" look so long associated with oscilloscopes. Instead, it is housed in a low-profile case that measures 21½"D × 13"W × 7"H (54.6 × 33 × 17.8 cm). The cabinet has a large adjustable carrying handle that doubles as a tilt stand.

General Information. The triggered sweep switch has 20 positions, spanning a range of 100 ns/cm to 0.2

s/cm. A separate control permits continuous adjustments on any given range of the switch. A 5× magnifier permits close examination of the displayed waveform at any point in the sweep.

Unlike some triggered-sweep scopes, the Heath instrument does not have the usual touchy sweep trigger stability adjustments and controls. A novel, digitally controlled time base provides rock-steady automatic triggering. Instead of the trace disappearing from the CRT screen when the trigger signal is absent, this new approach produces a constant base line to indicate that the system is working and that all controls are properly set. As soon as the channel input probe is connected to a signal source, the base line disappears and the signal's waveform is displayed.

Another nice touch is the location of the delay line. It is wired between the signal that triggers the sweep and the vertical amplifiers. This enables you to see at least 20 ns of the waveform before the trigger point. Hence, with this setup you can see *all* of the waveform.

In the auto-trigger mode, the trigger is initiated at zero crossing, although a couple of controls are provided to allow the time base to be triggered at any desired positive or negative point on the input wave form. It is this automatic sweep triggering that makes the Heath scope easier to use than conventional triggered-sweep instruments.

The scope employs a rectangular 10 × 6-cm post-deflection-acceleration CRT that produces a bright, sharp trace display. The engraved graticule on the CRT screen has a brightness control that makes it easy to set the graticule's visibility.

Assembly and Performance. The kit went together in about 35 hours of assembly time. Almost all of the electronic components that make up the scope mount on printed circuit boards, of which there are separate assemblies for each function in the instrument. The boards interconnect with each other and mount in the mainframe by way of heavy-duty plug connectors and factory-prepared wiring harnesses.

After assembling and checking out the scope according to the step-by-step instructions given in the manual that accompanied the instrument, we performed a few tests with the aid of our laboratory-grade 1-Hz to 1-MHz

square-wave generator and a standard r-f signal generator/frequency counter.

The scope's rise time measured considerably better than the 24-ns figure specified by Heath. The tunnel-diode output from our square-wave generator, with its extremely fast rise time, produced a clean wavefront, with a complete absence of ringing and other visible distortion products. The control of each of the two traces was complete. There was no interaction between the two channels, other than a slight dimming of the beam intensity when we switched in both traces. We merely turned up the scope's intensity control to compensate for the loss of brightness.

We used our r-f generator and frequency counter to run some bandwidth tests. The scope responded to 30 MHz before the amplitude of the displayed waveform became too low to be of much use in tests. With the scope's vertical gain control turned up to maximum, there was still a waveform displayed (admittedly, very low in amplitude) to about 65 MHz of input signal. We ran this test for the purpose of determining at what point the scope's triggered sweep system would become unstable and lose sync. To our surprise, the instrument remained in sync at 65 MHz, which is well beyond the 45-MHz figure stated in the published specs. Even switching between positive- and negative-transition triggering did not upset the synchronization.

The vertical amplifiers responded to signals down to 1 mV in amplitude. This, plus the results of our bandwidth and stability tests, was most impressive for an oscilloscope in its price range.

Comment. It is a fundamental engineering maxim that the test equipment you use must be at least one order of magnitude better than the device or equipment being tested. In this era of ultra-fast digital electronic equipment and broadband audio gear, this places heavy demands on an oscilloscope. Equally important, a scope bought now should be usable even with the next generation of developments in electronics.

The Heathkit Model IO-4510 oscilloscope will easily handle most jobs in modern electronics. It will undoubtedly not be obsolete for a long time to come.

CIRCLE NO. 5 ON READER SERVICE CARD



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The latest generation of integrated circuits reduces total harmonic distortion to 0.1%, typically .03%, and gives you a signal-to-noise ratio of 74dB below 10mV. That's quiet!

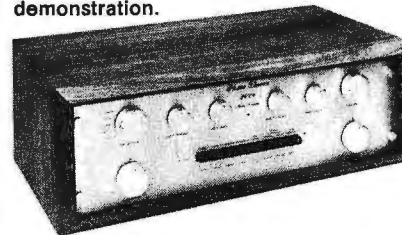
A highly advanced integrated circuit phono preamplifier creates the sonic excellence you have come to expect from Phase Linear.

A variable ambience injection circuit gives you more of the music—allows for the recovery of music lost with most preamplifiers.

Other features:

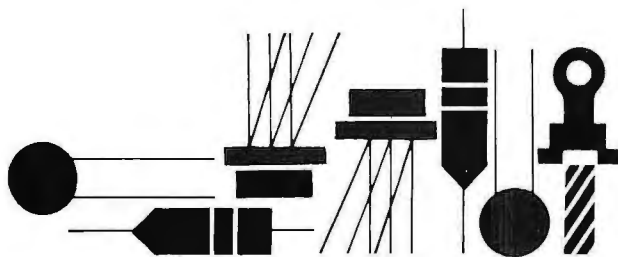
Individual detented bass and treble controls with a professional feel in each channel. Turnover points at 50Hz, 150Hz, 2kHz, and 5kHz, where up to 12dB of boost or cut may be applied... *a switchable low frequency active equalizer* for up to 6dB boost below 50Hz for a flatter bass response... *two complete tape circuits* for easy control and tape-to-tape dubbing... *a comfortable size* that complements other Phase Linear products: 5½" x 19" x 6"... and an *outstanding value at \$299.00.*

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Solid State

By Lou Garner

MANY USES FOR FLASHER/OSCILLATOR

WHILE most solid-state devices, except for highly specialized memories and custom IC's, are suitable for use in a variety of projects, semiconductor manufacturers occasionally introduce new units so versatile that they have as many potential applications as the proverbial mongrel dog has fleas. The ubiquitous 741 op amp is one example; the popular 555 timer and the CA3062 photo detector and power amplifier are others.

The latest member of this relatively exclusive club of "super-versatile" devices is the LM3909 LED flasher/oscillator, recently introduced by the National Semiconductor Corporation (2900 Semiconductor Drive, Santa Clara, CA 95051).

Comprising one pnp double collector and three npn transistors, a zener diode and nine resistors on a monolithic chip, as illustrated schematically in Fig. 1A, the LM3909 is packaged in an 8-lead plastic mini-DIP. Lead terminal connections are identified in Fig. 1B. With a maximum power dissipation rating of 500 mW, the device is specified for an operational temperature range of -25°C to $+70^{\circ}\text{C}$. Its max-

Typical 1.5V Flasher

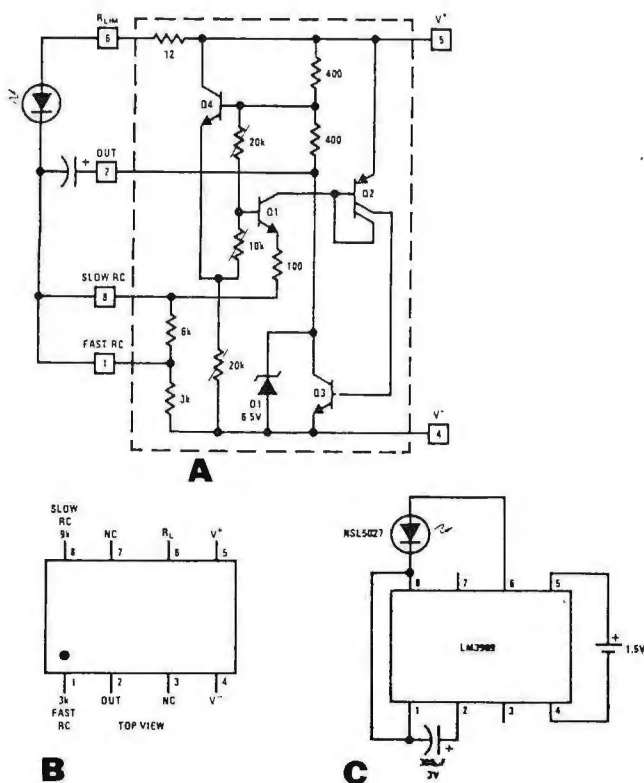


Fig. 1. Internal schematic of the LM 3909 (A), lead connections (B), basic flasher circuit (C).

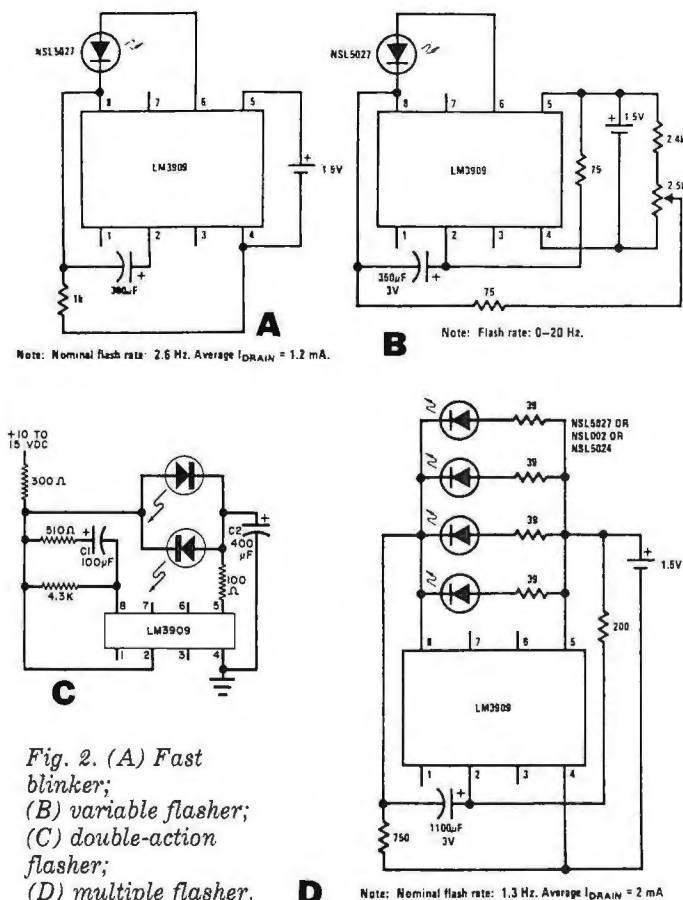
imum supply voltage rating, established by the internal zener, is 6.4 volts. Although the device will operate on voltages as low as 1.0 volt, with a power drain of only a few hundred microwatts, it is capable of delivering current pulses of as much as 200 mA, thus providing sufficient drive for a load such as an 8-ohm PM loudspeaker.

Unique among pulse-generating IC's, the LM3909 can deliver an output pulse with an amplitude higher than the dc source voltage. Thus it can drive LED's when powered by a dc supply of as little as 1 volt, even though 1.6 volts is required, normally, to energize the diode. This action is achieved by discharging the external timing capacitor through the LED in series with the source voltage, boosting the voltage applied to the diode. In practice, this capability, coupled with the LM3909's extremely high efficiency, makes it feasible to assemble a LED flasher circuit that will operate for more than a year, 24 hours a day, on a size D flashlight cell. In some cases, in fact, a cell's operating life in a flasher circuit may actually exceed its nominal shelf life!

With internal timing and LED current limiting resistors, the LM3909 requires only three external components for operation as a flasher—a LED, a timing capacitor, and a dc power source, as shown in Fig. 1C. Generally, the timing capacitor will be an electrolytic type, with a 3-volt rating suitable for LED flashers operating on dc supplies of 6 volts maximum. With the values specified on the diagram, the circuit's nominal flashing rate is 1 Hz, but its actual rate will depend on the capacitor's *true* value, taking tolerances into account. (Most small electrolytics have a rather broad capacitance tolerance range, typically from -20% to $+100\%$.) The circuit's average current drain ranges from a little over 0.6 mA with a new cell to less than 0.3 mA as the battery nears the end of its useful life. If an alkaline cell is used, it should have a useful life of over two and a half years, assuming that the flasher operates continuously.

With its extremely long battery life, the basic LED flasher circuit is ideal for use in boat mooring floats and rural lane markers, as well as in sales and advertising displays. It also makes a good night location marker for emergency equipment and controls, such as fire extinguishers and hoses, fire axes, special lighting gear, first-aid cabinets, fuse boxes, switches, locks, and control valves. Other potential applications include toy trucks and cars, children's vehicles, model trains, R/C model planes and boats, games, advertising novelties, and dress accessories and jewelry.

Other LED flasher circuits for the LM3909 are shown in Fig. 2. All of these use readily available components and can be breadboarded for experimental tests, or assembled on perforated or pc board. Except where noted, the resistors are rated for $\frac{1}{4}$ or $\frac{1}{2}$ watt; the capacitors are electrolytics; and the LED's are conventional devices.



The fast blinker circuit in Fig. 2A has a nominal flashing rate of 2.6 Hz and an average current drain of 1.2 mA. It is useful in conjunction with the basic slow-speed flasher to provide additional identification. In an apartment, office, or home, for example, the standard 1-Hz flasher could be used as a marker/locator for fire fighting and emergency lighting equipment, while the fast blinker might be used to identify controls, switches and locks. With the higher flashing rate, battery life is correspondingly shorter, but it still can be several months to over a year.

A variable flasher circuit is shown in Fig. 2B. With a flashing rate of 0 to 20 Hz, depending on the adjustment of a 2500-ohm potentiometer, this circuit can be used for experimental tests and in games, toys, and advertising displays. It should be of value, too, in psychological experiments and response time tests. If the rate control is calibrated, the design could be used for a simple photographic darkroom timer.

Designed to flash two LED's alternately, the double-action flasher circuit in Fig. 2C requires a somewhat higher source voltage and operates at (approximately) a 2.5-Hz rate. Capacitor C2 determines the flashing speed. In operation, one LED is energized as C2 charges, the second as C2 discharges. This circuit can be used with individual LED's or with dual-element devices, such as the MV5491. If a red/green flasher is desired, the green LED's anode should be connected towards pin 5, since a higher voltage pulse is available in this direction.

Four LED's are flashed simultaneously by the multiple flasher circuit in Fig. 2D. With an average current drain of only 2.0 mA and a nominal flashing rate of 1.3 Hz, this circuit can be used where a special identification pattern is needed, such as a bar, square or arrow. It should be useful, too, in toys and models. With a model plane, for example, the four LED's could be located on the nose, tail and two

wing tips. Other applications include advertising displays and games.

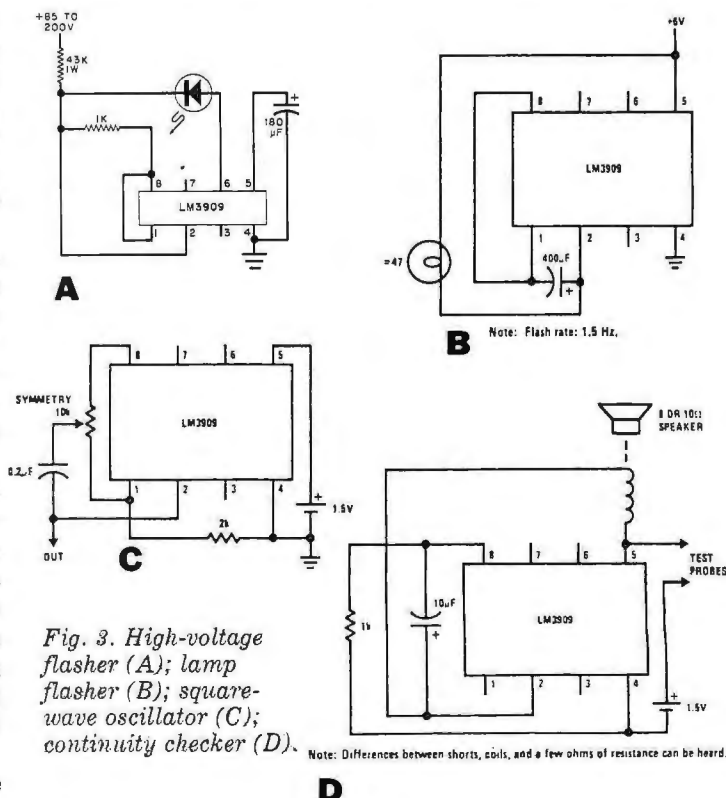
Although the LM3909 is designed specifically for use as a low-voltage LED flashing device, its versatility is such that it can be used in a variety of other circuits. Some additional applications are illustrated in Fig. 3.

The high-voltage flasher circuit in Fig. 3A can be used as an alternative to a neon warning lamp for dc power supplies. It is particularly valuable for remote indicator applications because the IC limits the maximum voltage on the LED to less than 7 volts above ground. In operation, the timing capacitor is charged through the 43,000-ohm series resistor, pin 2, and the IC's internal resistors, then discharged periodically through the LED when pin 2 is shunted to ground internally. With the component values specified, the nominal flashing rate is 1.7 Hz and the circuit will work satisfactorily with a dc source voltage of 85 to 200 volts.

Interestingly, the surprising LM3909 may be used to flash incandescent bulbs as well as LED's. A basic incandescent lamp flasher is shown in Fig. 3B. Here, a type #47 bulb is used in conjunction with a 6-volt dc power source, such as four series-connected flashlight cells. The circuit's nominal flashing rate with a 400-µF timing capacitor is 1.5 Hz.

One of a number of possible nonflasher applications for the LM3909 is illustrated in Fig. 3C, a 1-kHz square-wave oscillator. This circuit can be used in test equipment designs and as a clock source for digital timers, calculators, or control circuits. In operation, the circuit delivers a positive-going pulse with a peak-to-peak amplitude of slightly more than 1 volt. A 10,000-ohm potentiometer serves as the output signal's symmetry control.

A useful "buzz box" continuity and coil checker circuit is



given in Fig. 3D. Here, the LM3909 is used as an audio-frequency oscillator to drive a small PM loudspeaker. With practice, an operator can distinguish the differences be-

tween shorts, coils, and a few ohms of resistance by the quality of the sound obtained from the loudspeaker. This design could be assembled conveniently in a small plastic case or metal box for use as either a portable or bench test instrument.

Would you believe a flashlight that identifies itself in the dark? Such an intelligent device can be assembled using the LM3909. The basic circuit and light assembly is illustrated in Figs. 4A and 4B. A conventional two-cell flashlight may be used as the base for project construction, with the LM3909, 200- μ F timing capacitor, and LED installed in a translucent plastic cap attached to the back end of the case. Only one insulated contact strip in addition to the case connection is needed for flasher power since circuit current is drawn through the relatively low resistance (generally less than 2 ohms) of the flashlight bulb. The LED flasher operates continuously, of course, but the battery life is essentially unchanged due to the circuit's low current drain. If a single-cell flashlight is used, pins 1 and 8 of the LM3909 should be shorted together.

An emergency lantern/flasher application for the LM3909 is given in Fig. 4C. The IC drives an external transistor which, in turn, supplies current to a heavy-duty PR13 incandescent lamp bulb. With the component values indicated on the diagram, the nominal flashing rate is 1.5 Hz. Separate switches permit the user to select either flasher or lantern type operation. Operating power is supplied by a conventional 6-volt lantern battery. If desired, the flashing feature may be added to a standard 6-volt lantern, for, as a general rule, there is adequate free space within the typical lantern's case for circuit components.

The applications discussed above and illustrated in Figs. 1, 2, 3, and 4 are but a sampling of the many ways in which the versatile LM3909 can be used in practical circuits. Space permitting, I'll present additional circuits in future columns. One further hint—sometimes a flasher circuit will fail to operate due to a LED defect that is not apparent because it reduces the device's light output by only 10% or so. These LED's can be identified by a substantial increase in their current conduction between 0.9 and 1.2 volts. If you assemble an LM3909 LED flasher circuit, then, and it doesn't work, *check the LED*—you may have to get the LED out!

Reader's Circuit. One of our friends north of the border, Martin Jansen (991 Fleet Ave., Winnipeg, Manitoba, Canada R3M 1K5), submitted the interesting electronic "coin flipper" circuit illustrated in Fig. 5. Featuring a pair of popular IC's, the design may be used for assembling an executive decision maker (YES/NO) or as the basis for an electronic version of such games as "put and take" or "heads and tails." Standard, readily available components are used throughout, and the circuit can be assembled quite easily in

a small pocket-sized plastic or metal case for convenient use at appropriate times.

In operation, a pulse generator, IC1, serves to drive a JK flip-flop, IC2, when control switch S2 is closed. The flip-flop, in turn, alternately energizes a pair of light-emitting diodes, LED1 and LED2. The pulse rate, determined by timing capacitor C1, is faster than the eye can follow, so that it is impossible to tell which LED is on at any given moment. When S2 is opened, one or the other of the two LED's will remain lit, the other dark, the selection essentially a random choice depending on the precise instant that S2 is released. One of the LED's is used to represent YES, HEADS, PUT or a similar word, while the other represents the corresponding opposite expression, such as NO, TAILS, or TAKE. Thus, the instrument provides the user a random choice of two alternative decisions.

Except for trimmer potentiometer R3, all the resistors are $\frac{1}{4}$ or $\frac{1}{2}$ watt, while C1 is a small low-voltage ceramic or tubular paper capacitor. Almost any standard LED's may be used for the output indicators, LED1 and LED2, with R4's and R5's values chosen to limit their "on" current within specified maximum ratings.

Martin writes that he assembled his original model on a piece of Veroboard, mounting the assembly in an empty metal spice box, which he painted with model paints. However, with neither layout nor lead dress critical, the circuit might be wired on perf board, on a suitable pc board, or even point-to-point, if sockets are provided for the IC's.

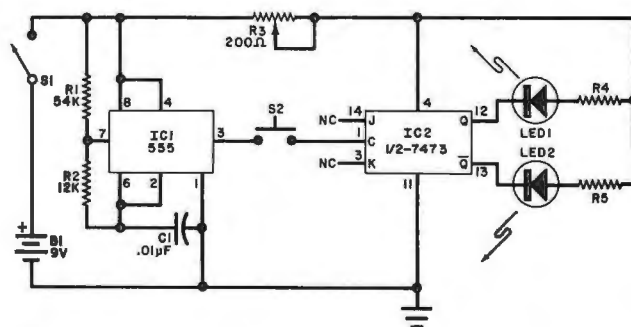


Fig. 5. Reader's electronic coin-flipper circuit.

When the wiring is completed and checked for errors, the circuit should be switched "on" and R3 adjusted to set IC2's voltage (between pins 4 and 11) to 5.0 volts. Afterwards, the completed unit may be used as is or mounted in an appropriate metal or plastic case, as preferred.

Device/Product News. RCA's Solid State Division (Box 3200, Somerville, NJ 08876) has announced a number of new power transistors which should spark the creative juices of imaginative experimenters and hobbyists. In-

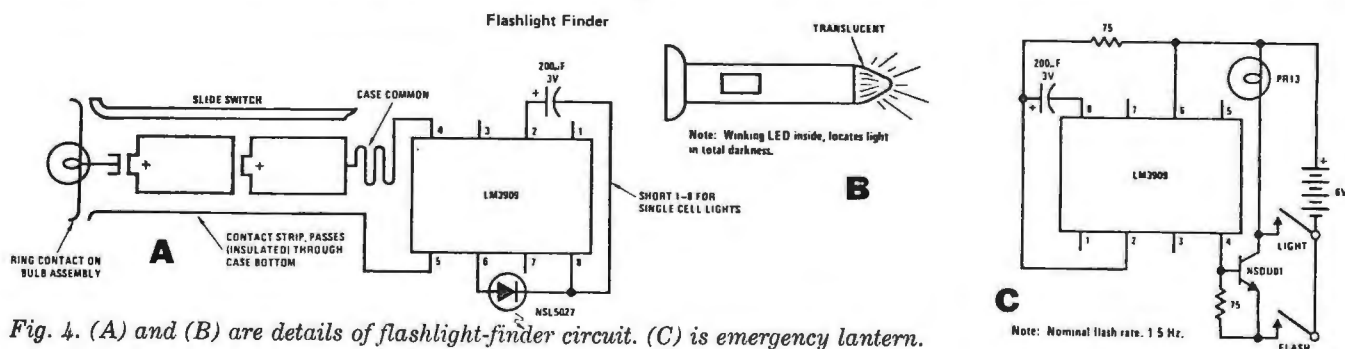


Fig. 4. (A) and (B) are details of flashlight-finder circuit. (C) is emergency lantern.

cluded are five new high-voltage silicon npn devices, types 2N6510-2N6514, designed primarily for use in electronic ignition systems. These have voltage ratings from 200 to 350 volts, depending on type, maximum collector currents of 7 amperes, device dissipations of 120 watts, and a dc beta range of 10 to 50. All five types are supplied in hermetic steel TO-3 packages. In addition to the high-voltage devices, three new 10-ampere pnp Darlington transistors, types RCA8203, RCA8203A, and RCA8203B, have been added to RCA's growing family of Darlington units. These new transistors are monolithic silicon pnp complements of npn types 2N6386, 2N6387, and 2N6388, and have voltage ratings from -40 to -80 volts, 60 watts device dissipation, and gains of 1000 at 5 amperes. Suitable for operation directly from an IC without a predriver, and designed for low- and medium-frequency applications in audio amplifiers, power switching circuits, hammer drivers, and series and shunt regulators, they are supplied in the TO-220AB straight lead version of the VERSAWATT plastic package.

From high power to high frequency—the Amperex Electronic Corporation (Solid State and Active Devices Division, Slatersville, RI 02876) has developed ten new small-signal uhf transistors with gain-bandwidth products from 2 GHz to 6 GHz at collector currents between 100 μ A and 150 mA. The new transistors offer low intermodulation distortion and low cross-modulation distortion for wide-band and similar sophisticated linear applications. Noise figures are as low as 1.9 dB at 500 MHz.

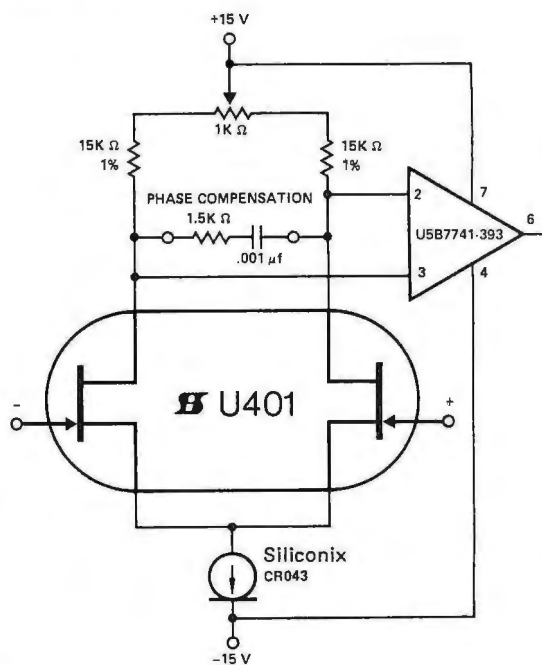


Fig. 6. Dual FET combined with op amp.

Siliconix has a suggestion for those of you who may need tightly spec'd FET input op amps... simply team one of its dual FETs with a standard bipolar op amp. One suggested circuit is illustrated in Fig. 6. Here, a U401 dual FET, in conjunction with a CR043 current regulator diode, is used as an input driver for a U5B7741-393 op amp. Matched 1% drain load resistors are used while a 1-K pot serves as a null adjustment. Phase compensation is provided by a 1.5-K resistor in series with a 0.001- μ F capacitor. According to Siliconix, this combination offers an input current rating of 15 pA maximum, 1 pA typical, an offset (without nulling) of 6 mV maximum, a drift of only 12 mV/ $^{\circ}$ C, a CMRR of 90 dB, and a slew rate of 0.5 V/ms. ♦

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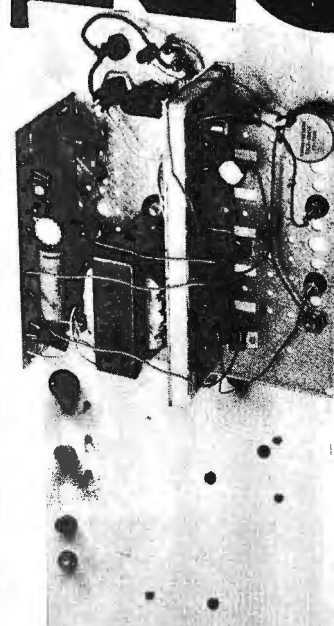
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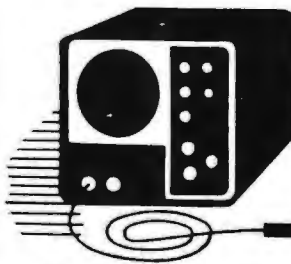
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Test Equipment Scene

By Leslie Solomon

TESTING CB MODULATION AND CAPACITORS

READERS frequently ask us how they can accomplish some testing chore that would normally be easy if they had the proper equipment—but the latter is too expensive for occasional use. There are usually ways to get around such problems. Here are two examples.

Checking CB Modulation. The typical CB'er is interested in knowing just how well modulated his transmitter is. Possibly he has had complaints about poor audio quality from his listeners on the other end. Obviously, the closer a transmitter is to having 100% modulation, the better the received signal. With less than 100% modulation, the audio "volume" is reduced. Modulation over 100% produces interfering "splatter," which can make transmission almost unintelligible, and is also illegal.

The transmitter can be checked easily with a modulation monitor, but this is an expensive instrument that is usually found only in professional r-f service shops.

To do your own modulation checking, you can build up the circuit shown in Fig. 1. You will need an oscilloscope on which you can gain access to the four electrostatic deflection plates of the CRT. Or, you can build a suitable power supply for almost any type of electrostatic CRT that you have on

hand. There is no need for the vertical and horizontal deflection circuits—just access to the deflection plate connectors.

The tuned input circuit is preset for the 27-MHz CB band and a short antenna is added. The rest of the circuit consists of a capacitor (C1) that couples the r-f signal to the upper vertical deflection plate of the CRT. The other plate is grounded. A simple diode detector and filter circuit couples the demodulated audio signal to the left horizontal deflection plate, with the right plate grounded.

To use the modulation monitor, apply power to the CRT circuit and allow it to warm up until a spot is displayed on the CRT. The modulation monitor does not need a power supply. Then turn on the CB rig and orient the monitor's antenna until the CRT spot changes to a vertical line when the CB transmitter is energized. Adjust the monitor tuning capacitor and antenna so that the vertical line is longer than half of the CRT screen.

With the CB microphone shielded so that it does not pick up any signals, a hum in the transmitter will show up as a broadening of the vertical line.

Speaking into the microphone at a normal level and with the normal mouth-to-microphone distance should cause the thin vertical line to change into a trapezoid. The trap-

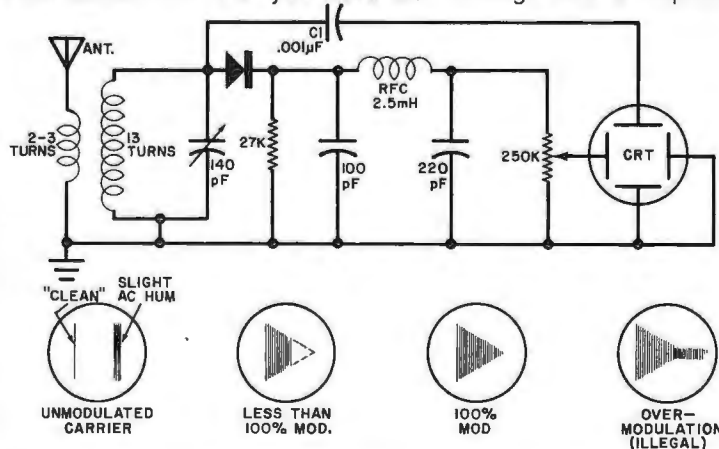


Fig. 1. Circuit for checking modulation. Waveforms show scope results.

ezoid will change to a triangle at the 100% modulation point. (See the four traces in Fig. 1.) When the shape is a trapezoid, the transmission is legal because it is modulated less than 100%. You can adjust the potentiometer to change the width of the trace.

If the triangle develops a "tail," as in the right-hand trace, the modulation is over 100% and is illegal. This tail is what causes the splatter that is so annoying on the band. Any rig that produces this effect should be checked before it is put back on the air. However, remember that FCC rules require that any adjustments on the frequency-sensitive portion of the transmitter must be made by a licensed Radio Technician.

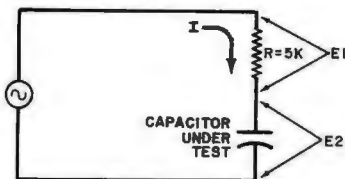


Fig. 2. Capacitor test circuit.

Capacitor Testing. There are several different types of capacitor testers available—some of them very expensive—but the simplest approach uses just an ordinary filament transformer, a fixed resistor, and an ac voltmeter. The basic circuit is shown in Fig. 2.

Connect the resistor and the capacitor to be tested in series across an ac source of known frequency. Although almost any audio frequency will do, the 60-Hz commercial line can be used. It is stable and convenient, but use the transformer to isolate the circuit for safety's sake.

First calculate the current flowing through the circuit. To do this, measure the voltage across the resistor, calling it E_1 . The current is then $I = E_1/R$. For example, if the resistor is 5000 ohms and the voltage drop is 7.5 V, the current is 0.0015 A.

To determine the capacitor value, first measure the voltage drop across the capacitor, calling it E_2 . Then the capacitance is $C = I/(2\pi fE_2)$. Thus, in the example, if E_2 is 5 V, $C = 0.0015/(6.28 \times 60 \times 5) = 0.7 \mu\text{F}$.

This approach is limited in accuracy since many capacitors may leak and produce erroneous meter indications. Also, the procedure cannot be used to check electrolytic capacitors.

If you are checking a number of capacitors, it might be handy to add a scale to the meter calibrated to read capacitance rather than voltage. ♦

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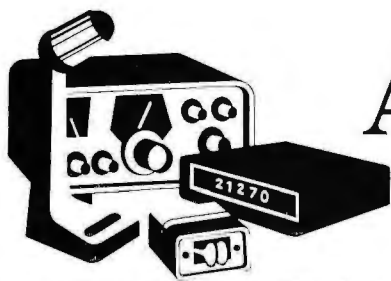
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Amateur Radio

By Herbert S. Brier, W9EGQ

USING THE OSCAR SATELLITES

UNTIL recently, working "real" DX on the vhf bands with low-power equipment was limited to a few hardy souls using sophisticated stations and techniques. All this has changed. Amateurs need no longer rely on the moon, fickle sunspots, etc., to propagate their signals—OSCAR can do the job reliably!

The Orbital Satellite Carrying Amateur Radio program officially started in 1961, when OSCAR 1 was assembled. OSCAR hitched a ride on a U.S. Air Force satellite booster and entered into a 300-mile (483-km) high polar orbit on December 12, 1961. Over 570 amateurs in 44 states and 28 countries reported hearing the cheery CW "Hi" from the satellite's 140-mW, 2-meter beacon.

OSCAR 2, another simple beacon, was launched in 1963, paving the way for OSCAR 3, an orbiting repeater. "Three" received signals near 144.1 MHz and retransmitted them near 145.9 MHz. During its 230 active orbits, hundreds of amateurs worked each other through OSCAR from state to state, country to country, and continent to continent.

The booster carrying OSCAR 4, launched December 1965, malfunctioned, and the satellite went into a highly elliptical orbit, which decayed after a few passes. However, before OSCAR 4's fiery reentry, the first satellite contact between the USSR and the USA was accomplished. OSCAR 5, built by Australian amateurs, followed in 1970. It transmitted continuous beacon signals on 145 MHz and 29.5-MHz beacon signals that could be turned on and off from the ground.

OSCAR 6 and OSCAR 7. OSCAR 6 was launched on October 15, 1972, and is still going strong! It receives signals between 145.9 and 146 MHz and repeats them between 29.45 and 29.55 MHz, with a power output of about 1.3 watts.

OSCAR 7, entering orbit November 15, 1974, contains all the features of the previous OSCAR's in one package. Constructed by Australian, Canadian, German and American amateurs, it contains two complete repeaters. Repeater "A" receives between 145.85 and 145.95 MHz and transmits between 29.4 and 29.5 MHz with an output of 2 watts PEP. On alternate days, OSCAR 7's repeater "B" receives between 432.125 and 432.175 MHz and retransmits between 145.975 and 145.925 MHz with a maximum power of 14 watts PEP. (Note: as the 432-MHz frequencies increase, the 145-MHz frequencies decrease.)

Besides functioning as repeaters, both OSCAR's transmit beacon signals and send telemetry information about their internal operation. They can also be programmed from the ground to send important messages to listeners. The OSCAR 6 beacon operates on 29.45 MHz. In contrast,

OSCAR 7 sends three beacon signals. On "A" days they are found at 29.502 MHz (CW and RTTY) and 432.1 MHz (RTTY), while on "B" days the beacon is active on 145.972 MHz (CW or RTTY).

OSCAR'S are powered by nickel/cadmium batteries, which are recharged through solar cells distributed over their outer surfaces. OSCAR 7 has a larger and more efficient charging system than OSCAR 6 has, so it can run continuously. OSCAR 6, on the other hand, must be shut down periodically to allow its batteries to recharge completely.

Using the Satellites. Probably the best way to start using the OSCAR satellites is to listen to them. You'll need a sensitive receiver capable of receiving 10-meter and/or 2-meter CW and SSB signals, and a fairly good receiving antenna. The best "starter" antennas are circularly polarized to minimize fading. Consult the Radio Amateurs Handbook (ARRL), Specialized Communications Techniques (ARRL), or the VHF Handbook (Radio Publishing) for plans of antennas and other OSCAR accessories.

The OSCAR's cross the United States each evening from south to north between approximately 7 and 11 p.m., local standard time. From north to south they make passes between 7 and 11 a.m. On the present OSCAR 7 schedule, Mode A (2- and 10-meter) operates Monday, Thursday, and Saturday evenings; Mode B (2-meter), on Sunday, Wednesday, and Friday evenings. Tuesday evenings and each morning (except weekends) are reserved for tests, class-room demonstrations and special schedules.

Start listening on the appropriate frequency (29.45, 29.502, or 145.972 MHz) shortly before 7 p.m., until the beacon signal is heard. Carefully note the acquisition time. The satellite will be in the same position at about the same time two days later. In addition, you will probably be able to hear the next pass about 115 minutes later, when OSCAR will have progressed 28.73 degrees to the west. If the second pass is louder than the first, listen again another 115 minutes later. On alternate days, each pass occurs about an hour earlier (or later) than the day before. After a few days you'll become familiar with the pattern.

For precise information, copy W1AW on Sunday afternoons. At 2000 GMT, all OSCAR north-to-south



Stuart Cowan, W2LX, Rye, N.Y., and his home-constructed, 40-watt, 146-MHz transmitter. He has worked a dozen countries in three continents using the OSCAR satellites. Antennas include a 14-element Yagi, a beam, and a center-fed wire doublet.



Holding a personal 3-continent "QSO" are (left to right) Phil Haller, W9HPG, ARRL Central Div. Director; Arnim Rudder, 9Y4AR, Trinidad; and S. Mittelsdorf, DL3UT, W. Germany. At Hamfesters picnic in Chicago.

equatorial crossing times for the following week are transmitted on CW. Frequencies are 3.58, 7.08, 14.08 and 21.08 MHz. The bulletins are repeated on RTTY at 2100 GMT on 3.625, 7.095, 14.095 and 21.095 MHz. Included are overpass times on each orbit for major cities like Detroit, Denver, New York, Houston, and San Francisco. This same information is available in printed form from AMSAT, Box 27, Washington D.C., 20044 (include a SASE).

You can identify the beacons by their strings of 5-digit numbers, with "Hi Hi" every 90 seconds, on CW (20 wpm) or RTTY. OSCAR 7's 10-meter beacon is somewhat stronger than the one aboard OSCAR 6. As soon as you can hear the beacon, tune into the appropriate passband for signals coming through the down-link. Most will be on CW, and the rest probably on SSB.

The satellite moves quickly, so you must continually compensate for resulting Doppler frequency shift. A usable pass will last anywhere from less than a minute to about 20 minutes. At first, signals will seem to pop in and out before they can be tuned in, and then the pass will be over. After a little practice, however, you'll get the "hang" of OSCAR operation. When the satellite is directly overhead, you should be able to hear stations within a 2500-mile (4025-km) circle centered on your QTH.

Transmitting. To avoid "hogging" the satellite's translator, your effective radiated power (erp) shouldn't exceed 100 watts. This can be achieved with 10 watts into a beam with a 10-dB gain, or 100 watts into a nondirectional antenna.

Many amateurs have old 146-MHz AM/CW transmitters stashed away, and many dealers have similar units on their used-equipment shelves. These can be resurrected and keyed for OSCAR work. Another source of 146- and 432-MHz transmitters is the 150- and 450-MHz commercial FM

gear available from surplus dealers. They can usually be retuned for the adjacent amateur band and modified for CW operation without much trouble. Commercially manufactured vhf SSB gear is being introduced; hf-to-vhf "transverters" can also be used. Amateur literature contains plenty of suggestions for the homebrewer. A good "junk box" will provide most of the parts needed to get on 2 meters or 70 cm.

When you are ready for two-way OSCAR work, tune your receiver to the OSCAR downlink passband. Send a short string of slow dots on the input passband and tune in your own signal. For OSCAR 7, choose 10-meter frequencies between 29.400 and 29.445 MHz for CW, RTTY, and SSTV; 29.445-29.455 MHz "potluck"; and 29.455 to 29.495 MHz for SSB. Do not operate above 29.495 MHz, or you'll cause interference with the beacon signal. After tuning in your own signal and noting how you sound to other operators, you're ready to make contacts.

Meetings and Literature. The 1975 ARRL Technical Symposium will be held Sept. 12, 1975 and the ARRL National Convention, Sept. 13 & 14, in Reston, Va. They will be sponsored by the Northern Virginia Amateur Radio Council and the Foundation for Amateur Radio. For details, write: Registration Chairman, P.O. Box 682, McLean, VA 22101.

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LISTEN IN TO APOLLO/SOYUZ TEST PROJECT

BY RICHARD S. FLAGG

AT 1220 GMT on July 15, 1975 (as of this writing), a Soyuz manned spacecraft will be launched from the Soviet Cosmodrome at Tyuratam. Seven and a half hours later, a manned Apollo spacecraft will be launched from Cape Canaveral, Florida. The combined operation will be called the Apollo-Soyuz Test Project (ASTP).

It is hoped that the Soyuz and the Apollo will rendezvous and dock at 1615 GMT, July 17. After some experiments, the two spacecraft will separate at 2254 GMT, July 19. The Soyuz is scheduled to return to earth at 1050 GMT, July 21, while the Apollo will stay in space until July 24.

The Soyuz will be injected into an 88.7-minute period orbit inclined at 51.5° to the equator. Approximately 78 minutes after launch, Soyuz will cross the equator at 41.6° proceeding northwest. The next north-bound equator cross will occur 88.7 minutes later at 32.54° west longitude. Each succeeding equatorial crossing will then occur 22.54° farther west along the equator at 88.7-minute intervals. These crossings can be plotted on a world map to find out where Soyuz is for reception purposes.

Soviet tracking ships will be stationed near Sable Island (Nova Scotia) and in the Gulf of Honduras. The "circle of coverage" for these ships is 1600 km (almost 1000 miles) centered on the ship. If a 1600-km circle, centered on the listener's location, overlaps the ship coverage, then communications can be monitored when the spacecraft is in the overlap area.

The easiest frequency to hear will be the 121.75-MHz transmissions using a 70-kHz voice-modulated FM transmission with 4 watts output. The Soyuz antenna is linearly polarized. The Apollo will use the same frequency, method of modulation, and power, but its antenna will be right-hand polarized. There will be several ground stations scattered about the U.S.A. (also many abroad) to maintain contact with the spacecraft. Downlink

voice communications to these stations will be on 296.8 MHz from Soyuz and 2287.5 MHz from the unified S-band system aboard the Apollo. Frequencies that will be used are shown in the table.

Experience during previous Soyuz flights has shown that a dipole antenna is sufficient to receive the 121.75-MHz signals if the receiver has a 3- or 4-dB noise figure. To ensure good voice signals, an antenna having about 10 dB of gain is suggested. A low-noise antenna preamplifier will also help.

SPACECRAFT FREQUENCIES

20.008 MHz (A)*	Soyuz. PDM, CW
121.75 MHz*	Soyuz, Salyut-4. 70-kHz voice FM
259.7 MHz*	ASTP. Intership AM voice
296.8 MHz*	ASTP. downlink AM voice to US ground stations from Salyut
922.75 MHz*	Soviet earth satellites. Beacon and telemetry
2287.5 MHz*	Apollo unified S-band center frequency

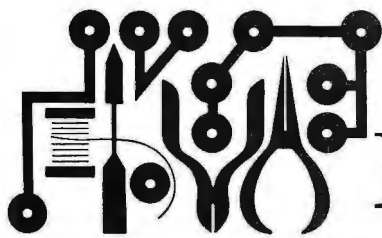
Notes:

(A) Intermittent use during flight.

* Will be used during ASTP flight

Legality of Monitoring. Listeners should be aware of Section 605 of the Communications Act of 1934 ("Unauthorized Publication of Communications") which states that it is unlawful to divulge the contents of any interstate or foreign communications which have been received, with the exception of communications broadcast or transmitted by amateurs or others for the use of the general public, or relating to ships in distress.

According to this rule, there appears to be no legal problem involved with the monitoring of spacecraft transmissions as long as the contents are not divulged to someone not present when the signals were received.



Hobby Scene

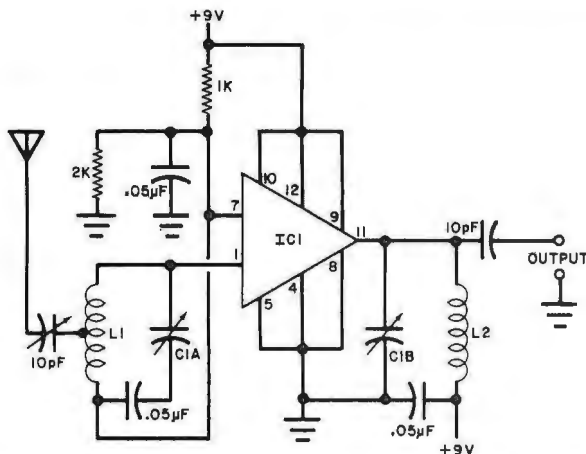
FM PREAMPLIFIER

Q. How about a schematic for an FM signal booster?

—Jeff Gold, Van Nuys, CA.

A. The circuit shown will provide about 24 dB gain across the FM broadcast band. It's fairly immune to cross-modulation, as it can handle interfering signals up to about 15 millivolts with 10% cross-modulation at maximum gain. IC1 is an RCA CA3005 amplifier, and allows connection of an

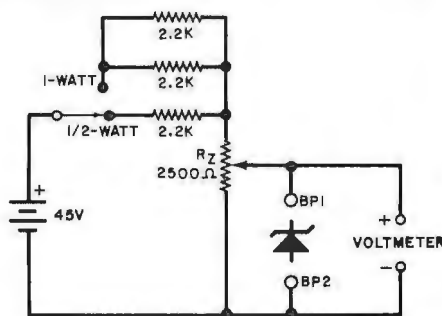
agc line. Reverse agc can be applied by varying the voltage at pin 12 from 9 volts (maximum gain) to 3 volts (full cutoff). Dynamic agc range is about 60 dB. L1 is made by winding four turns of #22 wire, center tapped, on a 1/4-inch OD coil form with an "E" material slug. L2 is the same as L1, but has no center tap. C1 (A and B) is a two-gang FM tuning capacitor (approx. 2.9-30 pF). Peak C1 and the 10-pF trimmer for maximum signal.



ZENER DIODE TESTER

Q. I bought a batch of zener diodes, but they are unmarked except for polarity. I want to find out the breakdown voltage of each of them, which is supposedly between 5 and 15 volts. Is there a circuit that will do this?—Joseph Gargiulo, Brooklyn N.Y.

A. The circuit shown here will be useful for testing zener diodes. Care must be taken lest the current rating be exceeded. Assuming the diodes are half-watt models, maximum current for a 5-volt zener will be 100 mA, and 25 mA for 20-volt zeners. For one-watt diodes, maximum current is 50 mA (20-volt zeners) and 200 mA (5-volt devices). With the switch in the half-watt position, current is limited to 20 mA. In the one-watt position, it is 40 mA. Most half- and one-watt diodes will zener at 20 mA, so set the switch to the half-watt position. Using an electronic volt-



meter, set the 2500-ohm potentiometer so that the voltmeter indicates 0 volts, then install the test diode between binding posts as shown. Slowly turn the potentiometer and note the increase in the voltmeter reading. If the zener is OK, you will reach a point where any further rotation of the pot will produce no increase in the voltage. This is the zener voltage. For some higher-powered zeners, it might be necessary to set the switch to one watt, if a run in the half-watt setting indicates no zenering action.

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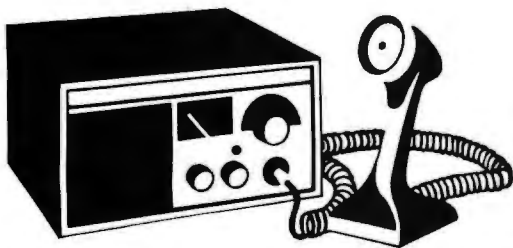
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CIRCLE NO. 24 ON READER SERVICE CARD



CB Scene

By Len Buckwalter

FUNDAMENTAL BLOCKING

MOST next-door neighbors will take a lot of guff. For instance, I've played my hi-fi at 102 dB after midnight, and none of my neighbors has ever complained. (I can still lean over the back fence and borrow a cup of sugar.) However, there is nothing that enrages a neighbor like interfering with his TV reception. A few microvolts of CB signal in the wrong place will cause the local populace to raise a furor that will make you want to move to Broken Jaw, Wyoming.

One of the trickier causes of TVI is not the fault of the CB'er or his rig. It is called fundamental blocking.

When a CB transceiver is located very close to a TV set, or if their antennas are not many feet apart, a 27-MHz carrier can be strong enough to "side-step" the TV's tuned circuits. It is possible for a powerful 27-MHz fundamental to impress a voltage somewhere in the TV chassis and be rectified into video or audio interference. The result: jellied Johnny Carson.

A clue to distinguishing fundamental blocking from second-harmonic interference is the distribution of the problem over the TV band. Second harmonic tends to produce a herringbone design on channel 2. Fundamental blocking can tear the picture (or sound) on any, or every, channel. The effect varies from station to station because of differences in TV signal strength.

The greatest victim of fundamental blocking is probably your own TV set because it is so near. Since this brand of interference is cured at the TV set, not at the CB transceiver, you can usually add the required filtering to your set and restore the family peace. But try to cure a neighbor's set and you'll need the diplomatic credentials of a Talleyrand. The dilemma is that, if you take it upon yourself to install a filter on a neighbor's TV, you'll probably be blamed for every trouble that

befalls the set for the next decade — from falling knobs to fly specks on the CRT. No one has yet figured out how to explain, convincingly, that hanging a passive filter on a TV's antenna terminals can't cause a breakdown somewhere else in the receiver.

An ironic twist to all of this is that the FCC is on the side of the CB'er when it comes to fundamental blocking. Literature put out by the Commission states that most TVI is caused by deficiencies in TV receiver design. A mass-produced set simply doesn't have sufficient shielding and rejection of signals beyond its tuning bandwidth. But try explaining that to your neighbors.

One solution is to tell the suffering viewer that some TV manufacturers offer high-pass filters to cure the problem. (Generally, it's a Drake TV-300-HP.) The policy varies in the industry, but some manufacturers will supply the component at no charge to a set owner upon request. (Sometimes you can get assistance in this matter by inquiring at a local FCC field office.) If the filter is provided, but installation is not, it is wise to have the TV owner get a service technician to make the connections. They may involve removing the back of the set to get at the input to the tuner (sometimes necessary in bad cases of TVI) and the owner may not like the idea of your poking around in there.



Fig. 1. High-pass filter.

Helping out. However, if your neighbor welcomes any technical help you want to volunteer, there are ways to deal with fundamental blocking. The easiest is to purchase a high-pass filter that is made for connecting to the external antenna input terminals (Fig. 1). Try this location before attempting to put the filter inside the set.

Another device you can try is an easily home-brewed wave trap which removes the CB signal at the TV antenna terminals. When tuned to resonance, the trap is a short circuit to the CB signal but won't affect TV signals. A

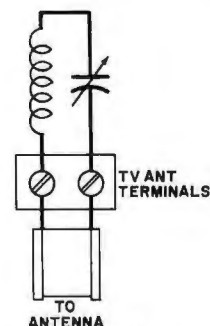


Fig. 2. Series-tuned wave trap.

schematic of the trap is shown in Fig. 2. The coil is made by closely winding 22 turns of 20-gauge enamelled wire on a 1/4-in. form (a pencil will do). Strip the enamel clean at both ends. The tuning capacitor is a common trimmer rated at 3-30 pF. Mount both the coil and capacitor on a small perforated board about 2 inches (5.1 cm) square. Attach a few inches of twinlead to the board and wire the trap as shown. The free ends of the twinlead connect to the TV terminals along with the regular TV antenna lead.

Now turn on the CB set and watch the interference on the TV screen. With a plastic tuning tool, adjust the capacitor until it hits resonance on 27 MHz and clears the TV picture. The capacitance of your hand can effect the tuning so do it by trial and error — tune, take your hand away, tune again, etc.

There's a chance that you won't be able to null out the CB signal. Although the values given here should work, distributed capacitance and/or inductance in your circuit can nudge the resonance point out of the 27-MHz band, beyond range of the tuning capacitor. This is cured by adjusting the coil. Try spreading the coil turns to reduce inductance and raise the trap's frequency.

Once in a while, the coil will have insufficient inductance and require a few additional turns. It is easier,

though, to try reducing the capacitance first. A good way to determine whether the trap is on frequency is to monitor it with a grid-dip meter. As you change the circuit parameters, the meter should null when the frequency hits 27-MHz resonance. As this is done, leave the tuning capacitor screw at its midrange. If you don't have a grid-dip meter, use the TV screen as the measuring instrument. When the trap is on frequency, interference should drop out. Then touch up the capacitor adjustment once more.

Which Is Better? As to whether the high-pass filter or the trap is better for reducing fundamental blocking, I'll have to duck the question. TVI is a cantankerous problem that usually succumbs only to trial-and-error treatment. The high-pass filter has the advantage of attenuating interference below 50 MHz and thus prevents blocking from police, fire, and other services in the low vhf band from 30 to 50 MHz or transmitters active in the h-f region. The trap, on the other hand, is inexpensive to make and can be centered right on the offending 27-MHz CB signal.

If nothing works, and your neighbor threatens to tear down your antenna, that is a possible solution. Moving a CB antenna 10 or 20 feet farther from a TV antenna can take some of the punch out of fundamental blocking. ♦

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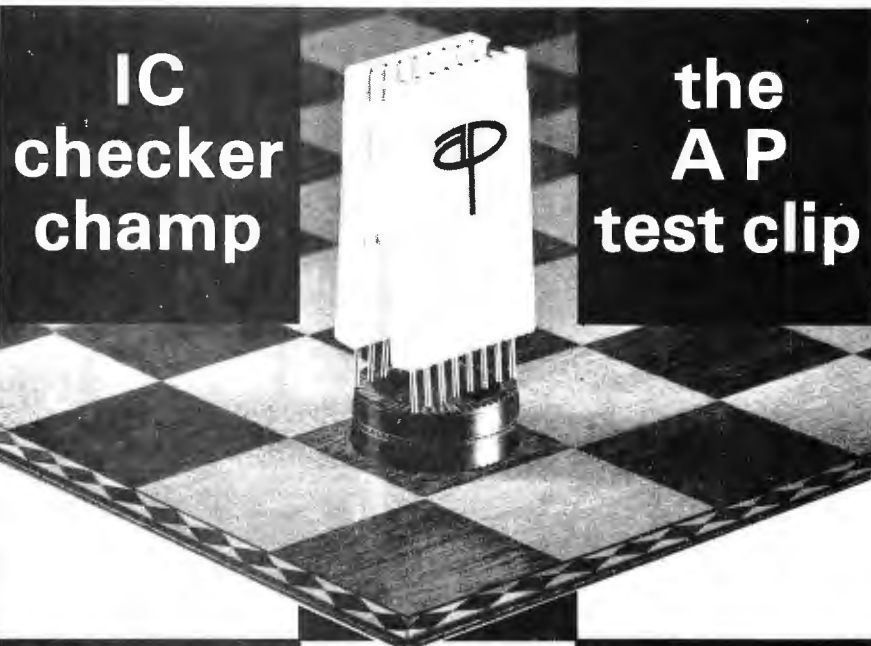
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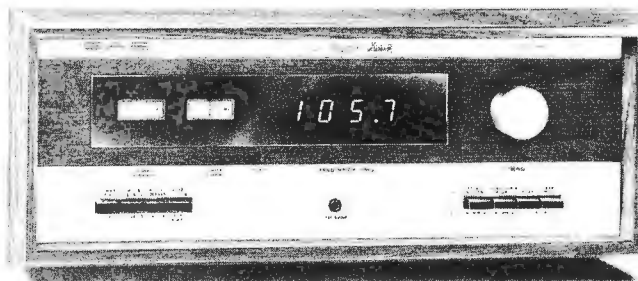
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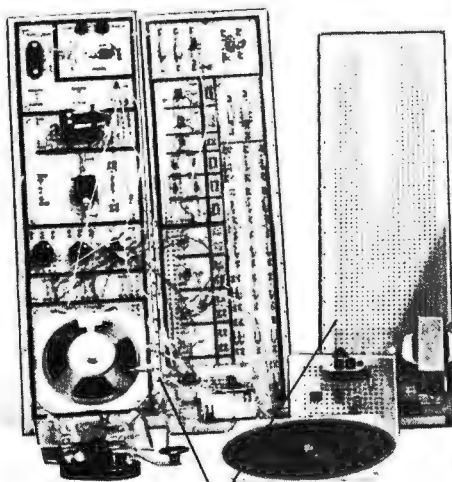
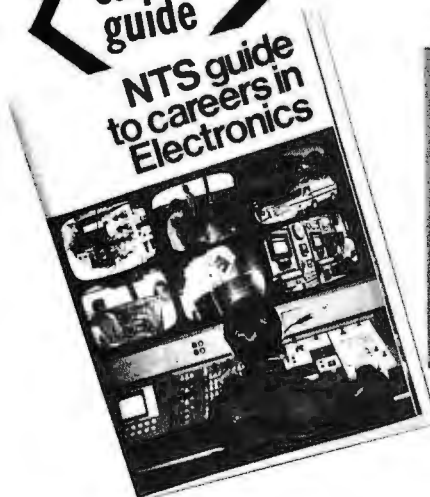
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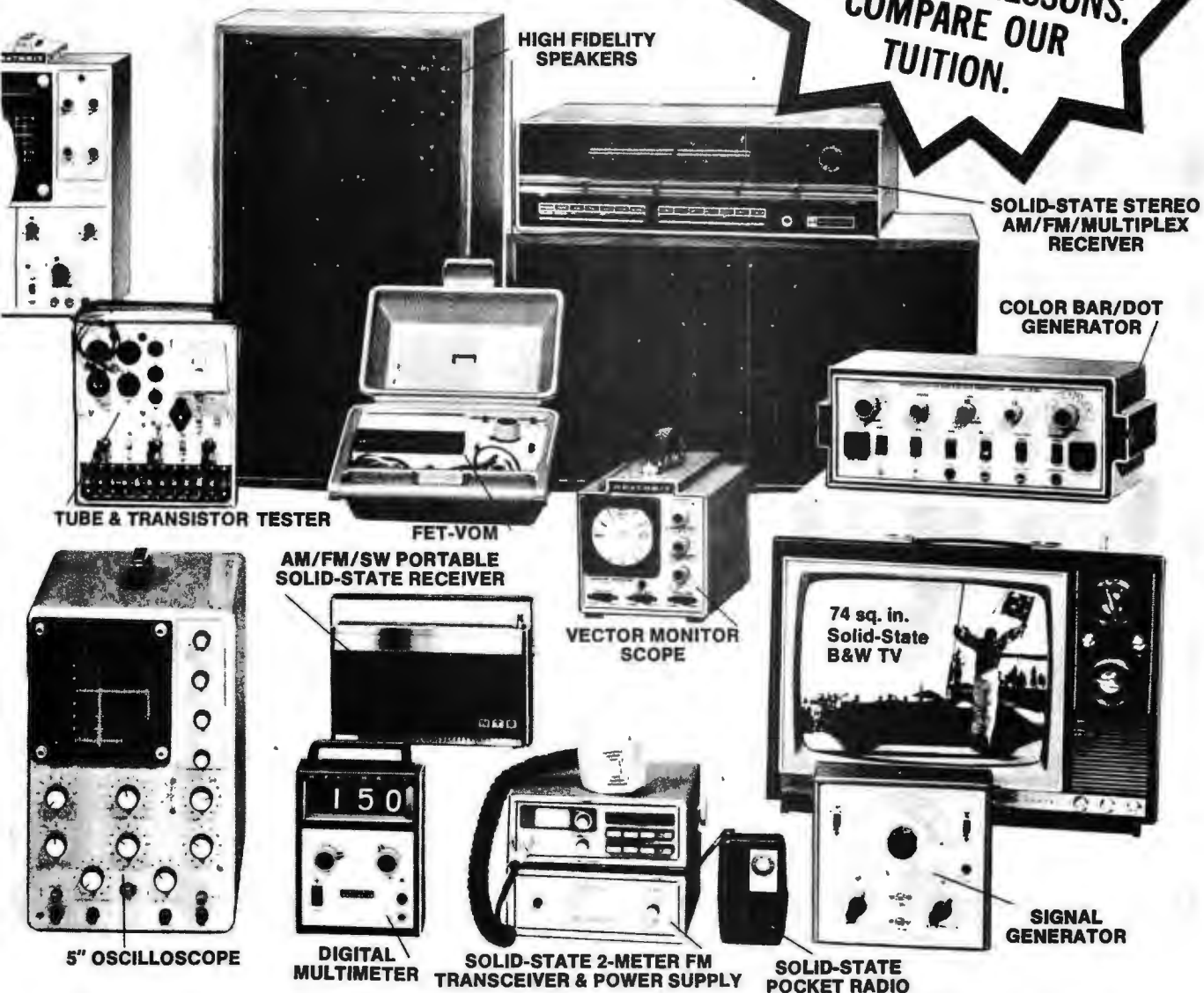
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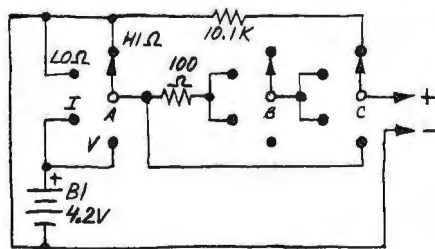
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Tips & Techniques

CALIBRATOR FOR VOM's

If you are unsure of the accuracy of your VOM, here's a simple calibrator with which you can check performance on the voltage, current, and resistance scales. Mercury cells, which keep a fairly constant output voltage across their terminals, and precision (1%) resistors are used. The voltage standard consists of B1, a 4.2-V mercury



battery (VS-133 or equivalent). A standard current source of 42 mA is derived from a mercury cell/precision resistor series combination. This same resistor (100 ohms) is used as a *LOW OHMS* standard, while a 10.1-kilohm precision resistor provides a *HIGH OHMS* calibration point. Resistors should be capable of dissipating at least 1/4W. Switch S1 is a 3P4T model (Calectro E2-166 or equivalent).

—Donald Walton

FELT TIPS AND TECHNIQUES

Fine-tip permanent markers (such as the "Sharpie" by Sanford Corp.) have many applications in experimenting. They can write on glass, so the fading type numbers on tube envelopes can be rewritten. The markings are waterproof, so hand perspiration won't obliterate them. Acetone or nail polish remover will erase the characters. Another application is in drawing lines on prototype pc boards instead of using inconvenient layout tape. The markings are also resistant to pc board etchant as well as layout tape. If you're imaginative, no doubt you can think of other useful applications.

—Garry Barnett

ORDINARY TYPING ERASER SAFELY CLEANS PC BOARDS

The raw copper conductor patterns on non-plated printed circuit boards have a habit of oxidizing rather quickly. The oxide often serves as a barrier that prevents solder from flowing properly around the pads to which leads are to be soldered. To avoid this problem, you could use steel wool as the oxide removing agent. However, the

safer approach and simpler tool to use is an ordinary typing eraser. The abrasive in the eraser is likely to remove a great deal less of the copper than does steel wool. And the eraser comes with its own built-in brush that can be used to sweep away the residue after erasing is completed.

—Steve Sekel

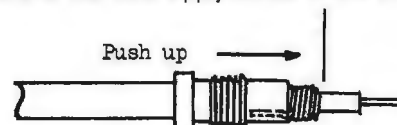
MAGNETIC HOLDER FOR SOLDERING PENCILS

A soldering pencil is ideally suited for pc work, but it can be hard to keep in place on a workbench. The pencil tends to roll because of its round shape. To keep it stationary, a magnetic latch (sold in hardware stores) can be used. The latch will hold it securely in place, yet it doesn't slow down soldering time.

—Thomas Fox

SOLDERING BNC CONNECTORS

Here's an easy and neat way to solder BNC connectors. Instead of fanning out the cable braid, wind 12 turns of No. 18 or 20 wire over a 3/8-in. (9.5-mm) length of braid, starting about 1/4 in. (19.1-mm) from one end of the wire. Apply solder to this coil.

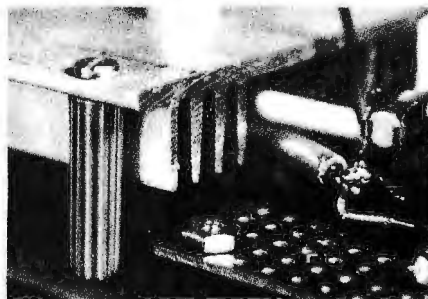


Bend the 3/4-in. (19.1-mm) lead down alongside the cable jacket. Finally, slide the male section of the BNC over the 3/4-in. (19.1-mm) lead (with which it should make a good, tight contact) until it lines up with the top of the coil. Proceed with the rest of the standard technique.

—Raul Lopez

PLASTIC SCREW ANCHORS MAKE INSULATED HEAT-SINK MOUNTS

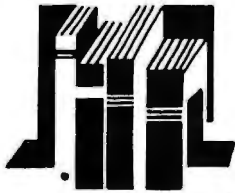
In some circuits, mounting the heat sinks for SCR's and power transistors presents a problem because the cathode or collector must be isolated from the chassis to which the heat sink is to be secured. Obviously, a



good nonconducting anchor must be found, and almost made to order are the plastic screw anchors sold in any hardware or houseware store. These anchors provide sturdy support for the heat sink while maintaining electrical isolation from the chassis. Anchors designed for 9/32-in. (7.14-mm) holes work well with No. 4 through No. 6 hardware. They can be cut to length as required.

—David Kraeuter

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LEARNING ABOUT SYNTHESIZERS

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The introductory manual contains a brief history of electronic music, a discussion of how a synthesizer works, and lists of synthesizer manufacturers and of some groups using synthesizers. Tips are given on selecting a synthesizer, and a list of reading sources and music trade magazines is given. A glossary of electronic music terms will be valuable to those not acquainted with this field.

Published by Music Studios, South Village Square, Amherst, MA 01002. 23 pages (8½" × 11"). \$5.00 soft cover.

ELECTRONIC DATABOOK—A GUIDE FOR DESIGNERS (2nd Edition)

by Rudolf Graf

Designers active in many fields will find some useful information in this volume. Data covering frequency allocations, modes of communication, representative communications systems, passive components and circuits, active components and amplifier configurations, mathematical relationships, formulas, and symbols, and physical configurations of components are included. Many monographs, tables, and curves are reproduced.

Published by Van Nostrand Reinhold Co., 450 W. 33rd St., New York, NY 10001. 312 pages (8½" × 11"). \$10.95

PRACTICAL DIGITAL ELECTRONICS—AN INTRODUCTION

by Juris Blukis and Mark Baker

In a world where computers and data communications are becoming ever more important, a knowledge of digital logic and circuits is desirable. This two-volume set, prepared by the Hewlett-Packard Company will provide an introduction to this field. Suitable for secondary schools and higher levels, the text and laboratory workbook aim at giving the student a working knowledge sufficient to prepare for troubleshooting or maintaining digital electronic equipment, including calculators, computers, digital instruments, and data communications equipment. The set is recent enough to treat CMOS and LSI, while providing a simple explanation of binary logic.

Published by Hewlett-Packard Co., 1501 Page Mill Road, Palo Alto, CA. 94304. 8½" × 11". Text and Workbook \$8.00 each.

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Published by the American Radio Relay League, 225 Main St. Newington, CT 06111. 208 pages. \$3.00 soft cover.

FM ATLAS AND STATION DIRECTORY (3rd Edition)

by Bruce Elving

This updated book presents frequency, program, and geographical information about the 4000 FM broadcast stations located in North America. Data are given on program format, output power, antenna height, stereo capability, antenna polariza-

tion, operating frequency and call letters. The introductory pages discuss trends in FM broadcasting, four-channel FM, illegal FM stations, translators and boosters, FM DXing, Dolby circuitry, and the status of AM-FM all-channel radio legislation. Also listed are network affiliations, and SCA activities. The book contains outline maps showing station distribution, and an FCC chart for computing station coverage. Available from FM Atlas, Box 24, Adolph, MN 55701. 96 pages. \$2.50 soft cover.

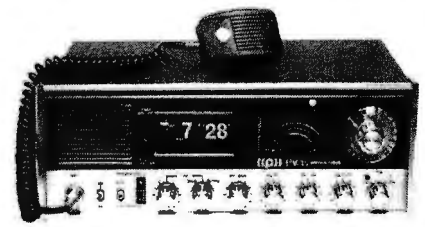
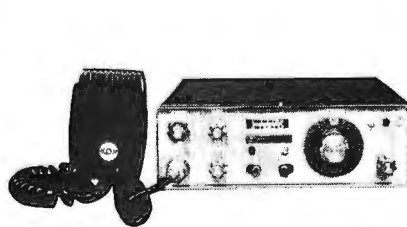
TTL COOKBOOK

by Don Lancaster

This book explains what transistor-transistor logic (TTL) is, how it works, and how to use it. TTL basics are given in Chapter One, and a catalog of TTL devices, including electrical and physical specifications, forms Chapter Two. Logic is covered in Chapter Three, such as one- and two-input systems, tri-state logic, and data-selector logic. Gate and timing circuits are covered in Chapter Four. Succeeding chapters discuss clocked logic, flip-flops, counters, shift registers, noise generators, and rate multipliers. A number of practical applications, including digital counters and test instruments, are described and illustrated.

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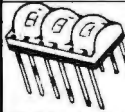


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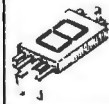
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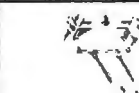
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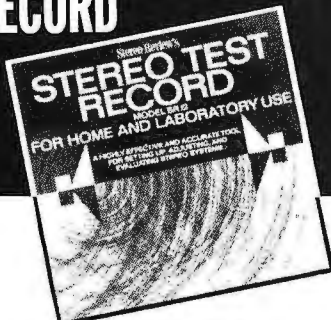
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P-1

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RESISTORS: 1/2, 1/4 watt— 5, 10%

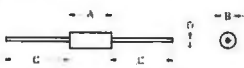
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- Permanent color codes which are immune to scrubbing with all commercially used flux solvents.

All Resistors from TABLE I 4c

All Resistors from TABLE II 6c

PLEASE ORDER IN MULTIPLES OF 5 ONLY.



Resistance: A B C D E
 10 250 0 015 0 140 0 015 1 500 0 015 0 015 0 015
 1 2 3 4 5 6 7 8 9 0

TABLE I: STANDARD 10% VALUES AND CATALOG NUMBERS

Resistance	Catalog Number	Resistance	Catalog Number	Resistance	Catalog Number	Resistance	Catalog Number
1/2 Watt	1/4 Watt	1/2 Watt	1/4 Watt	1/2 Watt	1/4 Watt	1/2 Watt	1/4 Watt
100	11 10207	12 10220	10K	11 10407	12 10420	1.0K	11 10607
120	11 12207	12 12220	12K	11 12407	12 12420	1.2K	11 12607
150	11 15207	12 15220	15K	11 15407	12 15420	1.5K	11 15607
180	11 18207	12 18220	18K	11 18407	12 18420	1.8K	11 18607
220	11 22207	12 22220	22K	11 22407	12 22420	2.2K	11 22607
2.7	11 27007	12 27020	270	11 27207	12 27220	27K	11 27407
3.3	11 33007	12 33020	330	11 33207	12 33220	33K	11 33407
3.9	11 39007	12 39020	390	11 39207	12 39220	39K	11 39407
4.7	11 47007	12 47020	470	11 47207	12 47220	47K	11 47407
5.6	11 56007	12 56020	560	11 56207	12 56220	56K	11 56407
6.8	11 68007	12 68020	680	11 68207	12 68220	68K	11 68407
8.2	11 82007	12 82020	820	11 82207	12 82220	82K	11 82407
10	11 10107	12 10120	1000	11 10307	12 10320	100K	11 10507
12	11 12107	12 12120	1200	11 12307	12 12320	120K	11 12507
15	11 15107	12 15120	1500	11 15307	12 15320	150K	11 15507
18	11 18107	12 18120	1800	11 18307	12 18320	180K	11 18507
22	11 22107	12 22120	2200	11 22307	12 22320	220K	11 22507
27	11 27107	12 27120	2700	11 27307	12 27320	270K	11 27507
33	11 33107	12 33120	3300	11 33307	12 33320	330K	11 33507
39	11 39107	12 39120	3900	11 39307	12 39320	390K	11 39507
47	11 47107	12 47120	4700	11 47307	12 47320	470K	11 47507
56	11 56107	12 56120	5600	11 56307	12 56320	560K	11 56507
68	11 68107	12 68120	6800	11 68307	12 68320	680K	11 68507
82	11 82107	12 82120	8200	11 82307	12 82320	820K	11 82507

TABLE II: STANDARD 5% VALUES AND CATALOG NUMBERS

Resistance	Catalog Number	Resistance	Catalog Number	Resistance	Catalog Number	Resistance	Catalog Number
1/2 Watt	1/4 Watt	1/2 Watt	1/4 Watt	1/2 Watt	1/4 Watt	1/2 Watt	1/4 Watt
100	13 10207	14 10220	10K	13 10407	14 10420	1.0K	13 10607
110	13 11207	14 11220	11K	13 11407	14 11420	1.1K	13 11607
120	13 12207	14 12220	12K	13 12407	14 12420	1.2K	13 12607
130	13 13207	14 13220	13K	13 13407	14 13420	1.3K	13 13607
150	13 15207	14 15220	15K	13 15407	14 15420	1.5K	13 15607
160	13 16207	14 16220	16K	13 16407	14 16420	1.6K	13 16607
180	13 18207	14 18220	18K	13 18407	14 18420	1.8K	13 18607
200	13 20207	14 20220	20K	13 20407	14 20420	2.0K	13 20607
220	13 22207	14 22220	22K	13 22407	14 22420	2.2K	13 22607
240	13 24207	14 24220	24K	13 24407	14 24420	2.4K	13 24607
270	13 27207	14 27220	27K	13 27407	14 27420	2.7K	13 27607
300	13 30207	14 30220	30K	13 30407	14 30420	3.0K	13 30607
330	13 33207	14 33220	33K	13 33407	14 33420	3.3K	13 33607
360	13 36207	14 36220	36K	13 36407	14 36420	3.6K	13 36607
390	13 39207	14 39220	39K	13 39407	14 39420	3.9K	13 39607
430	13 43207	14 43220	43K	13 43407	14 43420	4.3K	13 43607
470	13 47207	14 47220	47K	13 47407	14 47420	4.7K	13 47607
510	13 51207	14 51220	51K	13 51407	14 51420	5.1K	13 51607
560	13 56207	14 56220	56K	13 56407	14 56420	5.6K	13 56607
620	13 62207	14 62220	62K	13 62407	14 62420	6.2K	13 62607
680	13 68207	14 68220	68K	13 68407	14 68420	6.8K	13 68607
750	13 75207	14 75220	75K	13 75407	14 75420	7.5K	13 75607
820	13 82207	14 82220	82K	13 82407	14 82420	8.2K	13 82607
910	13 91207	14 91220	91K	13 91407	14 91420	9.1K	13 91607
1000	13 10307	14 10320	1000K	13 10507	14 10520	10K	13 10707
1100	13 11307	14 11320	1100K	13 11507	14 11520	11K	13 11707
1200	13 12307	14 12320	1200K	13 12507	14 12520	12K	13 12707
1300	13 13307	14 13320	1300K	13 13507	14 13520	13K	13 13707
1500	13 15307	14 15320	1500K	13 15507	14 15520	15K	13 15707
1600	13 16307	14 16320	1600K	13 16507	14 16520	16K	13 16707
1800	13 18307	14 18320	1800K	13 18507	14 18520	18K	13 18707
2000	13 20307	14 20320	2000K	13 20507	14 20520	20K	13 20707
2200	13 22307	14 22320	2200K	13 22507	14 22520	22K	13 22707
2400	13 24307	14 24320	2400K	13 24507	14 24520	24K	13 24707
2700	13 27307	14 27320	2700K	13 27507	14 27520	27K	13 27707
3000	13 30307	14 30320	3000K	13 30507	14 30520	30K	13 30707
3300	13 33307	14 33320	3300K	13 33507	14 33520	33K	13 33707
3600	13 36307	14 36320	3600K	13 36507	14 36520	36K	13 36707
3900	13 39307	14 39320	3900K	13 39507	14 39520	39K	13 39707
4300	13 43307	14 43320	4300K	13 43507	14 43520	43K	13 43707
4700	13 47307	14 47320	4700K	13 47507	14 47520	47K	13 47707
5100	13 51307	14 51320	5100K	13 51507	14 51520	51K	13 51707
5600	13 56307	14 56320	5600K	13 56507	14 56520	56K	13 56707
6200	13 62307	14 62320	6200K	13 62507	14 62520	62K	13 62707
6800	13 68307	14 68320	6800K	13 68507	14 68520	68K	13 68707
7500	13 75307	14 75320	7500K	13 75507	14 75520	75K	13 75707
8200	13 82307	14 82320	8200K	13 82507	14 82520	82K	13 82707
9100	13 91307	14 91320	9100K	13 91507	14 91520	91K	13 91707

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15 02310	2 Each of 167 Standard 5%, 1/2 Watt Resistors	21.50
15 03310	5 Each of 107 Standard 5%, 1/2 Watt Resistors	48.50
15 10310	10 Each of 167 Standard 5%, 1/2 Watt Resistors	99.00
15 01410	1 Each of 84 Standard 10%, 1/2 Watt Resistors	3.60
15 02410	2 Each of 84 Standard 10%, 1/2 Watt Resistors	6.75
15 05410	5 Each of 84 Standard 10%, 1/2 Watt Resistors	15.30
15 10410	10 Each of 84 Standard 10%, 1/2 Watt Resistors	29.70
15 01110	1 Each of 167 Standard 5%, 1/2 Watt Resistors	11.50
15 02110	2 Each of 167 Standard 5%, 1/2 Watt Resistors	21.50
15 05110	5 Each of 167 Standard 5%, 1/2 Watt Resistors	48.50
15 10110	10 Each of 167 Standard 5%, 1/2 Watt Resistors	99.00
15 01210	1 Each of 84 Standard 10%, 1/2 Watt Resistors	3.60
15 02210	2 Each of 84 Standard 10%, 1/2 Watt Resistors	6.75
15 05210	5 Each of 84 Standard 10%, 1/2 Watt Resistors	15.30
15 10210	10 Each of 84 Standard 10%, 1/2 Watt Resistors	29.70
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15 02715	2 Each of 15 Type 50A Ceramic Disc Capacitors	3.25
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15 10715	10 Each of 15 Type 50A Ceramic Disc Capacitors	13.50
15 01707	1 Each of 7 Type 70A Ceramic Disc Capacitors	0.90
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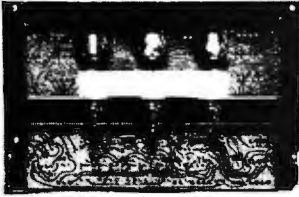
5HK Sprague type 5HK ceramic disc capacitors offer high capacity in a minimum space. All type 5HK capacitors have a tolerance of ±20%. Voltage ratings are 100VDC for values up to and including 0.01µF, and 500VDC for 0.015µF and higher.

Catalog Number	Capacitance	Unit Price
72 10369	1000 pF	0.7
72 15369	1500 pF	0.7
72 20369	2000 pF	0.7
72 22369	2200 pF	0.7
72 33369	3300 pF	0.7
72 47369	4700 pF	0.7
72 56369	5600 pF	0.7
72 68369	6800 pF	0.7
72 10400	0.010 µF	0.7
72 15400	0.015 µF	0.7
72 20400	0.020 µF	0.7
72 33400	0.030 µF	0.7
72 47400	0.040 µF	0.7
72 56400	0.050 µF	1.7
72 10500	0.1 µF	3.2

5GA Sprague type 5GA ceramic disc capacitors have low self-inductance of silvered flat-plate design for high by-pass efficiency. All type 5GA capacitors have a tolerance of ±20%, and 1000VDC ratings.

Catalog Number	Capacitance	Unit Price
71 10069	100 pF	0.7
71 15069	150 pF	0.7
71 10169	101 pF	0.7
71 12169	121 pF	0.7
71 15169	151 pF	0.7
71 20169	201 pF	0.7
71 25169	251 pF	0.7
71 27169	271 pF	0.7
71 30169	301 pF	0.7
71 33169	331 pF	0.7
71 36169	361 pF	0.7
71 39169	391 pF	0.7
71 43169	431 pF	0.7
71 47169	471 pF	0.7
71 51169	511 pF	0.7
71 56169	561 pF	0.7
71 68169	681 pF	0.7
71 75169	751 pF	0.7
71 82169	821 pF	0.7
71 10269	100 µF	0.7
71 12269	120 µF	0.7
71 15269	150 µF	0.7
71 18269	180 µF	0.7
71 20269	200 µF	0.7
71 22269	220 µF	0.7
71 25269	250 µF	0.7
71 27269	270 µF	0.7
71 30269	300 µF	0.7
71 33269	330 µF	0.7
71 36269	360 µF	0.7
71 39269	390 µF	0.7
71 43269	430 µF	0.7
71 47269	470 µF	0.7
71 50269	500 µF	0.7

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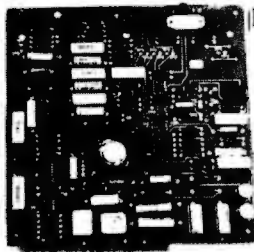
models. They all operate on input pulses, display the count, and close a set of contacts when the predetermined number is reached. Useful for many types of industrial counting, darkroom timing etc. All units have 3 BURROUGHS NIXIE tubes, type B5092A, which currently sell for \$17.25 ea. We supply operating instructions and some application data.

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2SA473	85	2SB407	2.10	2SC497	1.60	2SC930	65	2SD45	2.00
2SA495	65	2SB415	1.05	2SC515	80	2SC945	65	2SD64	75
2SA497	55	2SB461	1.25	2SC535	95	2SC1010	80	2SD65	75
2SA505	65	2SB463	1.65	2SC536	65	2SC1012	80	2SD68	70
2SA562	70	2SB471	1.75	2SC537	70	2SC1013	1.50	2SD72	1.00
2SA607	2.25	2SB474	1.75	2SC563	2.50	2SC1014	1.50	2SD88	1.50
2SA613	1.00	2SB481	2.10	2SC564	70	2SC1018	1.50	2SD120	85
2SA643	85	2SB492	1.25	2SC568	70	2SC1030	3.25	2SD130	1.50
2SA647	2.75	2SB495	95	2SC582	85	2SC1051	2.50	2SD141	2.25
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2SA679	2.25	2SB606	2.00	2SC605	1.00	2SC1079	3.95	2SD170	2.00
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2SB22	65	2SC143	3.50	2SC687	2.50	2SC1213	75	2SD292	85
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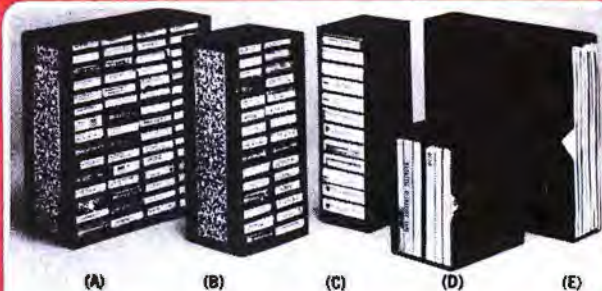
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100 pf/500V	7c	5.5c	4.5c	3.6c	8 pin Solder	27c	21c				
220 pf/500V	7c	5.5c	4.5c	3.6c	14 pin Solder	29c	23c				
470 pf/500V	7c	5.5c	4.5c	3.6c	16 pin Solder	32c	25c				
.001/500V	7c	5.5c	4.5c	3.6c	18 pin Solder	34c	26c				
.0022/500V	7c	5.5c	4.5c	3.6c	24 pin Solder	54c	42c				
.0047/500V	7c	5.5c	4.5c	3.6c							
.01/500V	10c	7.5c	6.3c	5.0c	6 pin W.W.	38c	30c				
.01/25V	5c	3.5c	3.0c	2.4c	14 pin W.W.	50c	39c				
.022/25V	6c	4.0c	3.5c	2.7c	16 pin W.W.	54c	42c				
.047/25V	9c	6.0c	5.3c	4.2c	18 pin W.W.	58c	46c				
.1/25V	12c	9.0c	7.5c	6.0c	24 pin W.W.	99c	80c				

1/2 & 1/4 WATT CARBON COMP. RESISTORS

5 each of the 85 standard 10% values (2.2-22M) 1/2 W Resistors (425 pcs.) Sorted by value \$12/set 2-4 are \$11/set 5-9 are \$10/set.
5 each of the 70 standard 10% values (10-5.6M) 1/4 W Resistors (350 pcs.) Sorted by value \$12/set 2-4 are \$11/set 5-9 are \$10/set.

SILICON TRANSISTORS

1-8 10-99 100					1-8 10-99 100				
2N918 . . . 10-106	21c	18.5c	16.5c	2N3645 . . . 10-105	20c	17.5c	16.0c		
2N930 . . . 10-106	21c	18.5c	16.5c	2N3646 . . . 10-106	22c	19.0c	17.5c		
2N932 . . . 10-106	21c	18.5c	16.5c	2N3904 . . . 10-92	22c	19.0c	17.5c		
2N934 . . . 10-106	21c	18.5c	16.5c	2N3906 . . . 10-92	22c	19.0c	17.5c		
2N936 . . . 10-106	21c	18.5c	16.5c	2N4124 . . . 10-92	22c	19.0c	17.5c		
2N938 . . . 10-98	18c	16.0c	14.5c	2N4126 . . . 10-92	22c	19.0c	17.5c		
2N391A . . . 98	22c	19.0c	17.5c	2N4401 . . . 10-92	22c	19.0c	17.5c		
2N392 . . . 98	22c	19.0c	17.5c	2N4402 . . . 10-92	22c	19.0c	17.5c		
2N393 . . . 98	22c	19.0c	17.5c	2N5087 . . . 10-92	22c	19.0c	17.5c		
2N394 . . . 98	22c	19.0c	17.5c	2N5089 . . . 10-92	22c	19.0c	17.5c		
2N563 . . . 10-106	20c	17.5c	17.5c	2N5129 . . . 10-92	19c	17.0c	15.0c		
2N564 . . . 10-106	20c	17.5c	17.5c	2N5130 . . . 10-92	19c	17.0c	15.0c		
2N538 . . . 10-105	20c	17.5c	18.0c	2N5134 . . . 10-106	19c	17.0c	15.0c		
2N368A . . . 10-105	20c	17.5c	18.0c	2N5137 . . . 10-106	19c	17.0c	15.0c		
2N540 . . . 10-106	20c	17.5c	18.0c	2N5138 . . . 10-106	19c	17.0c	15.0c		
2N541 . . . 10-106	20c	17.5c	18.0c	2N5139 . . . 10-106	19c	17.0c	15.0c		
2N542 . . . 10-105	20c	17.5c	18.0c	2N3955 . . . 10-92	3.10	29.9c	85.0c		

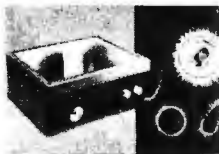
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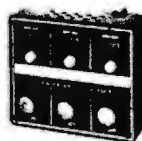
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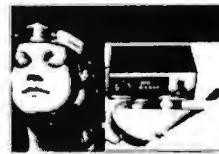
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